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ZHCS522H –JANUARY 2006–REVISED OCTOBER 2017

# **LM3100** 同步 **1MHz 1.5A** 降压稳压器

**Technical [Documents](http://www.ti.com.cn/product/cn/LM3100?dcmp=dsproject&hqs=td&#doctype2)** 

# <span id="page-0-0"></span>**1** 特性

- <sup>1</sup> 输入电压范围:4.5V 至 36V
- 1.5A 输出电流
- 0.8V,±1.5% 基准
- 集成 40V 双 N 通道同步开关
- 组件数量少,解决方案尺寸小
- 无需环路补偿
- 超快瞬态响应
- 可在使用陶瓷电容和其他低 ESR 电容器时保持稳 定
- 可编程开关频率高达 1MHz
- 启动时最大占空比受限
- 谷值电流限值
- 精密内部基准,可调节输出电压低至 0.8V
- 热关断
- <span id="page-0-2"></span>• 耐热增强型带散热片薄型小外形尺寸封装 (HTSSOP)-20 封装

# <span id="page-0-1"></span>**2** 应用

- 5VDC、12VDC、24VDC、12VAC 和 24VAC 系统
- 嵌入式系统
- 工业控制
- 汽车远程信息处理和车身电子装置
- 负载点稳压器
- 存储系统
- 宽带基础设施
- 直接对 2/3/4 节锂电池系统进行降压转换

# **3** 说明

Tools & **[Software](http://www.ti.com.cn/product/cn/LM3100?dcmp=dsproject&hqs=sw&#desKit)** 

LM3100 同步整流降压转换器 采用了 可实现高效经济 的降压稳压器所需的全部功能, 能够为负载提供 1.5A 电流和低至 0.8V 的电压。双 40V N 通道同步 MOSFET 开关使用的外部组件较少,从而降低了复杂 性,最大程度减少了布板空间。LM3100 专为与陶瓷及 其他极低的 ESR 输出电容器出色配合而设计。恒定导 通时间 (COT) 调节机制无需环路补偿, 从而实现快速 负载瞬态响应,并简化电路实现。与其他大多数 COT 稳压器不同,此款稳压器采用独特的设计,无需依赖 ESR 输出电容器也可实现稳定性。由于输入电压和导 通时间之间的反比关系,线路和负载变化时,运行频率 几乎保持恒定。通过外部编程,运行频率可高达 1MHz。保护功能 采用了 Vcc 欠压锁定、热关断和栅 极驱动欠压锁定。此器件采用热增强型 HTSSOP-20 封装

器件信息

-------		
器件型号	封装	封装尺寸(标称值)
LM3100	HTSSOP (20)	6.50mm x 4.40mm

(1) 如需了解所有可用封装,请参阅数据表末尾的可订购产品附 录。

图 **1.** 典型应用





# 目录





# <span id="page-1-0"></span>**4** 修订历史记录





• 已删除 从标题中删除了 Simple Switcher.. [1](#page-0-2)





# <span id="page-2-0"></span>**5 Pin Configuration and Functions**



#### **Pin Functions**



# <span id="page-3-0"></span>**6 Specifications**

# <span id="page-3-1"></span>**6.1 Absolute Maximum Ratings**

over operating free-air temperature range (unless otherwise noted)<sup>(1)(2)</sup>



(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office/ Distributors for availability and specifications.

# <span id="page-3-2"></span>**6.2 ESD Ratings**



(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.<br>(2) The human body model is a 100-pF capacitor discharged through a 1.5-k $\Omega$  resistor into each pin.

The human body model is a 100-pF capacitor discharged through a 1.5-kΩ resistor into each pin.

# <span id="page-3-3"></span>**6.3 Recommended Operating Conditions**

over operating free-air temperature range (unless otherwise noted)



### <span id="page-3-4"></span>**6.4 Thermal Information**



(1) For more information about traditional and new thermal metrics, see the *[Semiconductor](http://www.ti.com/cn/lit/pdf/spra953) and IC Package Thermal Metrics* application report.

#### <span id="page-4-0"></span>**6.5 Electrical Characteristics**

at T<sub>J</sub> = 25°C, and V<sub>IN</sub> = 18 V, V<sub>OUT</sub> = 3.3 V (unless otherwise noted).<sup>(1)</sup>



 $V_{\text{CC}}$  provides self bias for the internal gate drive and control circuits. Device thermal limitations limit external loading.

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# <span id="page-5-0"></span>**6.6 Typical Characteristics**

All curves taken at V<sub>IN</sub> = 18 V with configuration in typical application circuit for V<sub>OUT</sub> = 3.3 V shown in this datasheet. T<sub>A</sub> = 25°C, unless otherwise specified.





### **Typical Characteristics (continued)**

All curves taken at V<sub>IN</sub> = 18 V with configuration in typical application circuit for V<sub>OUT</sub> = 3.3 V shown in this datasheet. T<sub>A</sub> = 25°C, unless otherwise specified.



# **Typical Characteristics (continued)**

All curves taken at V<sub>IN</sub> = 18 V with configuration in typical application circuit for V<sub>OUT</sub> = 3.3 V shown in this datasheet. T<sub>A</sub> = 25°C, unless otherwise specified.





# <span id="page-8-0"></span>**7 Detailed Description**

# <span id="page-8-1"></span>**7.1 Overview**

The LM3100 Step Down Switching Regulator features all functions needed to implement a cost effective, efficient buck power converter capable of supplying 1.5 A to a load. This voltage regulator contains Dual 40-V N-Channel buck synchronous switches and is available in a thermally enhanced HTSSOP-20 package. The Constant ON-Time (COT) regulation scheme requires no loop compensation, results in fast load transient response, and simplifies circuit implementation. It will work correctly even with an all ceramic output capacitor network and does not rely on the output capacitor's ESR for stability. The operating frequency remains constant with line and load variations due to the inverse relationship between the input voltage and the on-time. The valley current limit detection circuit, internally set at 1.9 A, inhibits the high-side switch until the inductor current level subsides. Please refer to the functional block diagram with a typical application circuit.

The LM3100 can be applied in numerous applications and can operate efficiently from inputs as high as 36 V. Protection features include: Thermal shutdown, V<sub>CC</sub> under-voltage lockout, gate drive under-voltage lockout.



# <span id="page-8-2"></span>**7.2 Functional Block Diagram**

### <span id="page-8-3"></span>**7.3 Feature Description**

### <span id="page-8-4"></span>**7.3.1 Hysteretic Control Circuit Overview**

The LM3100 buck DC-DC regulator employs a control scheme in which the high-side switch on-time varies inversely with the line voltage  $(V_{\text{IN}})$ . Control is based on a comparator and the one-shot on-timer, with the output voltage feedback (FB) compared with an internal reference of 0.8 V. If the FB level is below the reference the buck switch is turned on for a fixed time determined by the input voltage and a programming resistor  $(R_{ON})$ . Following the on-time, the switch remains off for a minimum of 260 ns. If FB is below the reference at that time the switch turns on again for another on-time period. The switching will continue until regulation is achieved.

The regulator will operate in discontinuous conduction mode at light load currents, and continuous conduction mode with heavy load current. In discontinuous conduction mode (DCM), current through the output inductor starts at zero and ramps up to a peak during the on-time, then ramps back to zero before the end of the off-time. The next on-time period starts when the voltage at FB falls below the internal reference. Until then the inductor current remains zero and the load is supplied entirely by the output capacitor. In this mode the operating frequency is lower than in continuous conduction mode, and varies with load current. Conversion efficiency is maintained since the switching losses are reduced with the reduction in load and switching frequency. The discontinuous operating frequency can be calculated approximately as follows:

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# **Feature Description (continued)**

$$
F_{SW} = \frac{V_{OUT} (V_{IN} - 1) \times L \times 1.18 \times 10^{20} \times I_{OUT}}{(V_{IN} - V_{OUT}) \times R_{ON}^2}
$$
(1)

<span id="page-9-3"></span>For  $(V_{IN} - V_{OUT}) \times R_{ON}$ <br>tinuous conduction mode (C<br>f-time. In this mode, the op<br>operating frequency can be<br> $F_{SW} = \frac{V_{OUT}}{4.0 \times 10^{10} \text{ m/s}}$ In continuous conduction mode (CCM), current always flows through the inductor and never reaches zero during the off-time. In this mode, the operating frequency remains relatively constant with load and line variations. The CCM operating frequency can be calculated approximately as follows:

$$
T_{\text{SW}} = \frac{V_{\text{OUT}}}{1.3 \times 10^{-10} \times R_{\text{ON}}}
$$
 (2)

<span id="page-9-2"></span>The output voltage is set by two external resistors ( $R_{FB1}$ ,  $R_{FB2}$ ). The regulated output voltage is calculated as follows:

$$
V_{\text{OUT}} = 0.8 \text{ V} \times (R_{\text{FB1}} + R_{\text{FB2}})/R_{\text{FB2}} \tag{3}
$$

#### <span id="page-9-0"></span>**7.4 Device Functional Modes**

#### *7.4.1* **Start-up Regulator (V<sub>CC</sub>)**

The start-up regulator is integrated within LM3100. The input pin (VIN) can be connected directly to line voltage up to 36 V, with transient capability of 40 V. The V<sub>CC</sub> output regulates at 6 V, and is current limited to 65 mA. Upon power up, the regulator sources current into the external capacitor at  $V_{CC}$  (C<sub>VCC</sub>). C<sub>VCC</sub> must be at least 680 nF for stability. When the voltage on the VCC pin reaches the under-voltage lockout threshold of 3.75 V, the buck switch is enabled and the Soft-start pin is released to allow the soft-start capacitor  $(C_{SS})$  to charge.

The minimum input voltage is determined by the dropout voltage of  $V_{CC}$  regulator, and the  $V_{CC}$  UVLO falling threshold (≊3.7 V). If VIN is less than  $\approx$ 4.0 V, the V<sub>CC</sub> UVLO activates to shut off the output.

#### **7.4.2 Regulation Comparator**

The feedback voltage at FB pin is compared to the internal reference voltage of 0.8 V. In normal operation (the output voltage is regulated), an on-time period is initiated when the voltage at FB falls below 0.8 V. The buck switch stays on for the on-time, causing the FB voltage to rise above 0.8 V. After the on-time period, the buck switch stays off until the FB voltage falls below 0.8 V again. Bias current at the FB pin is nominally 100 nA.

#### **7.4.3 Over-Voltage Comparator**

The voltage at FB pin is compared to an internal 0.92 V reference. If the feedback voltage rises above 0.92 V the on-time pulse is immediately terminated. This condition can occur if the input voltage, or the output load, changes suddenly. Once the OVP is activated, the buck switch remains off until the voltage at FB pin falls below 0.92 V. The low side switch will stay on to discharge the inductor energy until the inductor current decays to zero. The low side switch will be turned off.

#### **7.4.4 ON-Time Timer, Shutdown**

The ON-Time of LM3100 main switch is determined by the  $R_{ON}$  resistor and the input voltage (V<sub>IN</sub>), and is calculated from:

$$
t_{ON} = \frac{1.3 \times 10^{-10} \times R_{ON}}{V_{IN}}
$$
(4)

where relation<br>of the selecte<br>thion. This related from Eq<br> $\frac{V_{\text{N}}}{V_{\text{N}}}\approx \frac{V_{\text{N}}}{V_{\text{N}}}\approx 1$ The inverse relationship of t<sub>ON</sub> and V<sub>IN</sub> results in a nearly constant switching frequency as V<sub>IN</sub> is varied. R<sub>ON</sub> should be selected for a minimum on-time (at maximum  $V_{IN}$ ) greater than 200 ns for proper current limit operation. This requirement limits the maximum frequency for each application, depending on  $V_{IN}$  and  $V_{OUT}$ , calculated from [Equation](#page-9-1) 5:

$$
F_{\text{SW(MAX)}} = \frac{V_{\text{OUT}}}{V_{\text{IN(MAX)}} \times 200 \text{ ns}} \tag{5}
$$

<span id="page-9-1"></span>The LM3100 can be remotely shut down by taking the EN pin below 1.1 V. Refer to [Figure](#page-10-0) 20. In this mode the SS pin is internally grounded, the on-timer is disabled, and bias currents are reduced. Releasing the EN pin allows normal operation to resume.





#### **Device Functional Modes (continued)**

For normal operation, the voltage at the EN pin is set between 1.5 V and 3.0 V, depending on  $V_{IN}$  and the external pull-up resistor. For all cases, this voltage must be limited not to exceed 7 V.



**Figure 20. Shutdown Implementation**

#### <span id="page-10-0"></span>**7.4.5 Current Limit**

Current limit detection occurs during the off-time by monitoring the re-circulating current through the low-side synchronous switch. Referring to Functional Block Diagram, when the buck switch is turned off, inductor current flows through the load, into PGND, and through the internal low-side synchronous switch. If that current exceeds 1.9 A the current limit comparator toggles, forcing a delay to the start of the next on-time period. The next cycle starts when the re-circulating current falls back below 1.9 A and the voltage at FB is below 0.8 V. The inductor current is monitored during the low-side switch on-time. As long as the overload condition persists and the inductor current exceeds 1.9 A, the high-side switch will remain inhibited. The operating frequency is lower during an over-current due to longer than normal off-times.

[Figure](#page-10-1) 21 illustrates an inductor current waveform, the average inductor current is equal to the output current,  $I_{\text{OUT}}$  in steady state. When an overload occurs, the inductor current will increase until it exceeds the current limit threshold, 1.9 A. Then the control keeps the high-side switch off until the inductor current ramps down below 1.9 A. Within each on-time period, the current ramps up an amount equal to:

$$
\Delta I = \frac{(V_{IN} - V_{OUT}) \times t_{ON}}{L}
$$
 (6)

During this time the LM3100 is in a constant current mode, with an average load current ( $I_{\text{OCL}}$ ) equal to 1.9 A +ΔI/2.



**Figure 21. Inductor Current - Current Limit Operation**

#### <span id="page-10-1"></span>**7.4.6 N-Channel Buck Switch and Driver**

The LM3100 integrates an N-Channel buck (high-side) switch and associated floating high voltage gate driver. The gate drive circuit works in conjunction with an external bootstrap capacitor and an internal high voltage diode. A 33 nF capacitor  $(C_{\text{BST}})$  connected between BST and SW pins provides voltage to the high-side driver during the buck switch on-time. During each off-time, the SW pin falls to approximately  $-1$  V and  $C_{\text{BST}}$  charges from the  $V_{CC}$  supply through the internal diode. The minimum off-time of 260 ns ensures adequate time each cycle to recharge the bootstrap capacitor.

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# **Device Functional Modes (continued)**

#### **7.4.7 Soft-Start**

The soft-start feature allows the converter to gradually reach a steady state operating point, thereby reducing start-up stresses and current surges. Upon turn-on, after  $V_{CC}$  reaches the under-voltage threshold, an internal 8 µA current source charges up the external capacitor at the SS pin. The ramping voltage at SS (and the noninverting input of the regulation comparator) ramps up the output voltage in a controlled manner.

An internal switch grounds the SS pin if any of the following cases happen: (i) VCC falls below the under-voltage lock-out threshold; (ii) a thermal shutdown occurs; or (iii) the EN pin is grounded. Alternatively, the converter can be disabled by connecting the SS pin to ground using an external switch. Releasing the switch allows the SS pin return to pull high and the output voltage returns to normal. The shut-down configuration is shown in [Figure](#page-11-0) 22 .



**Figure 22. Alternate Shutdown Implementation**

#### <span id="page-11-0"></span>**7.4.8 Thermal Protection**

The LM3100 should be operated so the junction temperature does not exceed the maximum limit. An internal Thermal Shutdown circuit, which activates (typically) at 165°C, takes the controller to a low power reset state by disabling the buck switch and the on-timer, and grounding the SS pin. This feature helps prevent catastrophic failures from accidental device overheating. When the junction temperature falls back below 145°C (typical hysteresis = 20°C), the SS pin is released and normal operation resumes.



### <span id="page-12-0"></span>**8 Applications and Implementation**

#### **NOTE**

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

#### <span id="page-12-1"></span>**8.1 Applications Information**

#### **8.1.1 External Components**

The following guidelines can be used to select the external components.

#### *8.1.1.1*  $R_{FR1}$  *and*  $R_{FR2}$

The ratio of these resistors is calculated from:

$$
\frac{R_{FB1}}{R_{FB2}} = \frac{V_{OUT}}{0.8V} - 1
$$
 (7)

R<sub>FB1</sub> and R<sub>FB2</sub> should be chosen from standard value resistors in the range of 1.0 kΩ - 10 kΩ which satisfy the above ratio.

For  $V_{\text{OUT}}$  = 0.8 V, the FB pin can be connected to the output directly. However, the converter operation needs a minimum inductor current ripple to maintain good regulation when no load is connected. This minimum load is about 10 µA and can be implemented by adding a pre-load resistor to the output.

#### *8.1.1.2 RON*

The minimum value for  $R_{ON}$  is calculated from:

$$
R_{ON} \ge \frac{200 \text{ ns} \times V_{IN(MAX)}}{1.3 \times 10^{-10}}
$$
 (8)

[Equation](#page-9-2) 2 in [Hysteretic](#page-8-4) Control Circuit Overview section can be used to select  $R_{ON}$  if a specific frequency is desired as long as the above limitation is met.

#### *8.1.1.3 L*

The main parameter affected by the inductor is the output current ripple amplitude  $(I_{OR})$ . The maximum allowable  $(I<sub>OR</sub>)$  must be determined at both the minimum and maximum nominal load currents. At minimum load current, the lower peak must not reach 0 A. At maximum load current, the upper peak must not exceed the current limit threshold (1.9 A). The allowable ripple current is calculated from the following equations:

$$
I_{OR(MAX1)} = 2 \times I_{O(min)} \tag{9}
$$

or

$$
I_{OR(MAX2)} = 2 \times (1.9 \text{ A} - I_{O(max)}) \tag{10}
$$

The lesser of the two ripple amplitudes calculated above is then used in the following equation:

$$
L = \frac{V_{\text{OUT}} \times (V_{\text{IN}} - V_{\text{OUT}})}{I_{\text{OR}} \times F_{\text{S}} \times V_{\text{IN}}}
$$
(11)

where  $V_{\text{IN}}$  is the maximum input voltage and Fs is determined from [Equation](#page-9-3) 1. This provides a value for L. The next larger standard value should be used. L should be rated for the  $I_{PK}$  current level shown in [Figure](#page-10-1) 21.



# **Applications Information (continued)**



**Figure** 23. **Inductor Selector** for  $V_{OUT} = 3.3$  **V** 



**Figure 24. Inductor Selector for**  $V_{OUT} = 0.8$  **V** 

### 8.1.1.4 *C*<sub>VCC</sub>

The capacitor on the  $V_{CC}$  output provides not only noise filtering and stability, but also prevents false triggering of the V<sub>CC</sub> UVLO at the buck switch on/off transitions. For this reason, C<sub>VCC</sub> should be no smaller than 680 nF for stability, and should be a good quality, low ESR, ceramic capacitor.

### *8.1.1.5 C<sup>O</sup> and CO3*

 $C<sub>O</sub>$  should generally be no smaller than 10  $\mu$ F. Experimentation is usually necessary to determine the minimum value for  $C_{\Omega}$ , as the nature of the load may require a larger value. A load which creates significant transients requires a larger value for  $C_{\Omega}$  than a fixed load.

 $C_{O3}$  is a small value ceramic capacitor to further suppress high frequency noise at V<sub>OUT</sub>. A 47 nF is recommended, located close to the LM3100.

#### *8.1.1.6 CIN and CIN3*

 $C_{1N}$ 's purpose is to supply most of the switch current during the on-time, and limit the voltage ripple at  $V_{1N}$ , assume the voltage source feeding  $V_{IN}$  has an output impedance greater than zero. If the source's dynamic impedance is high (effectively a current source),  $C_{IN}$  supplies the average input current, but not the ripple current.

At maximum load current, when the buck switch turns on, the current into  $V_{\text{IN}}$  suddenly increases to the lower peak of the inductor's ripple current, ramps up to the peak value, then drop to zero at turn-off. The average current during the on-time is the load current. For a worst case calculation,  $C_{\text{IN}}$  must supply this average load current during the maximum on-time.  $C_{\text{IN}}$  is calculated from:



# **Applications Information (continued)**

$$
C_{IN} = \frac{I_{OUT} \times t_{ON}}{\Delta V} \tag{12}
$$

where  $I_{\text{OUT}}$  is the load current, t<sub>ON</sub> is the maximum on-time, and  $\Delta V$  is the allowable ripple voltage at V<sub>IN</sub>.

 $C_{1N3}$ 's purpose is to help avoid transients and ringing due to long lead inductance at V<sub>IN</sub>. A low ESR, 0.1 µF ceramic chip capacitor is recommended, located close to the LM3100.

### 8.1.1.7 *C<sub>BST</sub>*

The recommended value for  $C_{\text{BST}}$  is 33 nF. A high quality ceramic capacitor with low ESR is recommended as  $C_{\text{BST}}$  supplies a surge current to charge the buck switch gate at turn-on. A low ESR also helps ensure a complete recharge during each off-time.

# *8.1.1.8 CSS*

The capacitor at the SS pin determines the soft-start time, i.e. the time for the reference voltage at the regulation comparator, and the output voltage, to reach their final value. The time is determined from the following:

$$
t_{SS} = \frac{C_{SS} \times 0.8V}{8 \mu A}
$$
 (13)

#### *8.1.1.9*  $C_{\text{FB}}$

If output voltage is higher than 1.6 V, this feedback capacitor is needed for Discontinuous Conduction Mode to improve the output ripple performance, the recommended value for  $C_{FB}$  is 10 nF.

# <span id="page-14-0"></span>**8.2 Typical Application**







# <span id="page-15-0"></span>**Typical Application (continued)**



**Figure** 26. **Typical Application Schematic for**  $V_{OUT} = 0.8 V$ 



# <span id="page-16-0"></span>**9 Layout**

### <span id="page-16-1"></span>**9.1 Layout Guidelines**

#### **9.1.1 PC Board Layout**

The LM3100 regulation, over-voltage, and current limit comparators are very fast, and will respond to short duration noise pulses. Layout considerations are therefore critical for optimum performance. The layout must be as neat and compact as possible, and all external components must be as close as possible to their associated pins. Refer to the functional block diagram, the loop formed by  $C_{\text{IN}}$ , the high and low-side switches internal to the IC, and the PGND pin should be as small as possible. The PGND connection to Cin should be as short and direct as possible. There should be several vias connecting the Cin ground terminal to the ground plane placed as close to the capacitor as possible. The boost capacitor should be connected as close to the SW and BST pins as possible. The feedback divider resistors and the  $C_{FB}$  capacitor should be located close to the FB pin. A long trace run from the top of the divider to the output is generally acceptable since this is a low impedance node. Ground the bottom of the divider directly to the GND (pin 7). The output capacitor,  $C_{\text{OUT}}$ , should be connected close to the load and tied directly into the ground plane. The inductor should connect close to the SW pin with as short a trace as possible to help reduce the potential for EMI (electro-magnetic interference) generation.

If it is expected that the internal dissipation of the LM3100 will produce excessive junction temperatures during normal operation, good use of the PC board's ground plane can help considerably to dissipate heat. The exposed pad on the bottom of the IC package can be soldered to a ground plane and that plane should extend out from beneath the IC to help dissipate the heat. The exposed pad is internally connected to the IC substrate. Additionally the use of thick copper traces, where possible, can help conduct heat away from the IC. Using numerous vias to connect the die attach pad to an internal ground plane is a good practice. Judicious positioning of the PC board within the end product, along with the use of any available air flow (forced or natural convection) can help reduce the junction temperature.

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### <span id="page-17-0"></span>**10** 器件和文档支持

#### <span id="page-17-1"></span>**10.1** 接收文档更新通知

要接收文档更新通知, 请转至 Tl.com 上的器件产品文件夹。单击右上角的通知我 进行注册, 即可每周接收产品信 息更改摘要。有关更改的详细信息,请查看任何已修订文档中包含的修订历史记录。

#### <span id="page-17-2"></span>**10.2** 社区资源

下列链接提供到 TI 社区资源的连接。链接的内容由各个分销商"按照原样"提供。这些内容并不构成 TI 技术规范, 并且不一定反映 TI 的观点;请参阅 TI 的 [《使用条款》。](http://www.ti.com/corp/docs/legal/termsofuse.shtml)

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#### <span id="page-17-3"></span>**10.3** 商标

E2E is a trademark of Texas Instruments.

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#### <span id="page-17-4"></span>**10.4** 静电放电警告



ESD 可能会损坏该集成电路。德州仪器 (TI) 建议通过适当的预防措施处理所有集成电路。如果不遵守正确的处理措施和安装程序 , 可 能会损坏集成电路。

ESD 的损坏小至导致微小的性能降级 , 大至整个器件故障。 精密的集成电路可能更容易受到损坏 , 这是因为非常细微的参数更改都可 能会导致器件与其发布的规格不相符。

### <span id="page-17-5"></span>**10.5 Glossary**

[SLYZ022](http://www.ti.com/cn/lit/pdf/SLYZ022) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

# <span id="page-17-6"></span>**11** 机械、封装和可订购信息

以下页面包含机械、封装和可订购信息。这些信息是指定器件的最新可用数据。这些数据如有变更,恕不另行通知 和修订此文档。如欲获取此数据表的浏览器版本,请参阅左侧的导航。



# **PACKAGING INFORMATION**



**(1)** The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

<sup>(2)</sup> RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures. "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

**(3)** MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

**(4)** There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

**(5)** Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

<sup>(6)</sup> Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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# **PACKAGE OPTION ADDENDUM**

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**TEXAS** 

**Pin1**

# **TAPE AND REEL INFORMATION**

**STRUMENTS** 





#### **QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**







# **PACKAGE MATERIALS INFORMATION**

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\*All dimensions are nominal



# **TEXAS INSTRUMENTS**

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# **TUBE**



# **B - Alignment groove width**

\*All dimensions are nominal



PWP (R-PDSO-G20)

PowerPAD<sup>™</sup> PLASTIC SMALL OUTLINE



This drawing is subject to change without notice. В.

Body dimensions do not include mold flash or protrusions. Mold flash and protrusion shall not exceed 0.15 per side. C.

This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad D.

Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding<br>recommended board layout. This document is available at www.ti.com <http://www.ti.com>.<br>E. See the additional figure in the Pro E. Falls within JEDEC MO-153

PowerPAD is a trademark of Texas Instruments.



# **MECHANICAL DATA**

# PWP0020A





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