TEXAS INSTRUMENTS

TPS259270, TPS259271

ZHCSE37E −AUGUST 2015−REVISED NOVEMBER 2017

TPS25927x 具有阻断 FET 控制功能的 4.5V 至 18V 电子熔丝

1 特性

- 4.5V 至 18V 保护
- 集成 28mΩ 导通金属氧化物半导体场效应晶体管 (MOSFET)
- 最大绝对电压 20V
- 1A 至 5A 可调电流 I_{LIMIT}
- ±8% I_{LIMIT} 精度（3.7A 时）
- 支持反向电流阻断
- 可编程 OUT（输出）转换率，欠压闭锁 (UVLO)
- 内置热关断
- 通过 UL 2367 认证 − 文件编号 E339631*
  - *RILIM ≤ 130 kΩ（最大电流 5A）
- 单点故障测试期间安全 (UL60950)
- 小型封装尺寸 - 10L (3mm x 3mm) 超薄小外形尺寸无引线封装 (VSON)

2 应用

- 硬盘 (HDD) 和固态硬盘 (SSD)
- 机顶盒
- 服务器/辅助 (AUX) 电源
- 风扇控制
- PCI/PCIe 卡
- 适配器供电器件
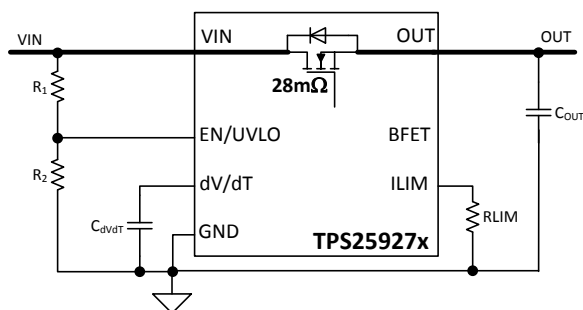
3 说明

TPS25927x 系列电子熔丝是采用小型封装的高度集成电路保护和电源管理解决方案。该器件使用极少的外部组件并可提供多重保护模式。它们能够有效地防止过载、短路、过高浪涌电流和反向电流。

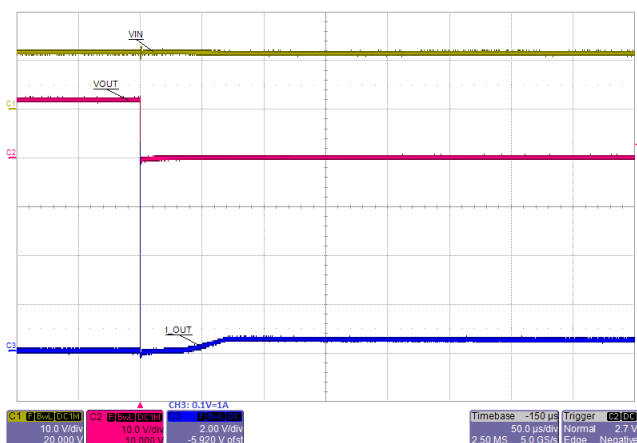电流限制级别可通过单个外部电阻设定。对于 电压斜坡有特别要求的应用可以通过单个电容器来设定 dV/dT 引脚，以确保合适的输出斜率。

许多系统（例如 SSD）禁止将储存的电容能量通过 FET 二极管倒流到降压或短路输入总线。BFET 引脚专用于这类系统。外部 NFET 可与 TPS25927x 输出形成"背靠背 (B2B)"连接，而由 BFET 驱动的栅极可防止电流从负载流回电源。

器件信息[1]

器件型号	封装	封装尺寸（标称值）
TPS259270	VSON (10)	3.00mm × 3.00mm
TPS259271		

(1) 要了解所有可用封装，请参阅数据表末尾的可订购产品附录。

应用电路原理图

瞬态：输出短路

English Data Sheet: SLVSCU8

目录

4 修订历史记录

Changes from Revision D (January 2017) to Revision E   **Page**

• 已删除 删除了*功能方框图* 中的过压 1

Changes from Revision C (September 2017) to Revision D   **Page**

• Changed status of TPS259270 from Preview to Active in the *Table 1* 3

Changes from Revision B (September 2016) to Revision C   **Page**

• Added Transient junction temperature to *Absolute Maximum Ratings* table 4

Changes from Revision A (August 2015) to Revision B   **Page**

• Added section:*Controlled Power Down using TPS25927x* 20

Changes from Original (August 2015) to Revision A   **Page**

• 已更改 "产品预览"至"量产数据" 1

Table 1. Device Comparison Table

PART NUMBER	UV	OV CLAMP	FAULT RESPONSE	STATUS
TPS259271	4.3 V	—	Auto-retry	Active
TPS259270	4.3 V	—	Latched	Active

5 Pin Configuration and Functions

DRC Package
10-Pin VSON
Top View
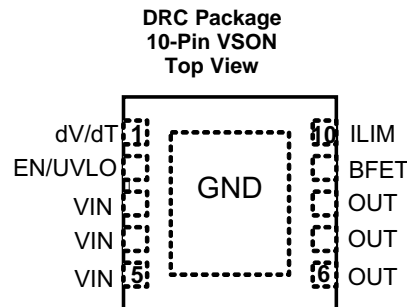
Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
BFET	9	O	Connect this pin to the gate of a blocking NFET. See the *Feature Description* section. This pin can be left floating if it is not used
dV/dT	1	O	Connect a capacitor from this pin to GND to control the ramp rate of OUT at device turnon
EN/UVLO	2	I	This is a dual function control pin. When used as an ENABLE pin and pulled down, it shuts off the internal pass MOSFET and pulls BFET to GND. When pulled high, it enables the device and BFET. As an UVLO pin, it can be used to program different UVLO trip point via external resistor divider
GND	Thermal Pad	—	GND
ILIM	10	O	A resistor from this pin to GND sets the overload and short circuit limit
OUT	6-8	O	Output of the device
VIN	3-5	I	Input supply voltage

6 Specifications

6.1 Absolute Maximum Ratings

over operating temperature range (unless otherwise noted) [1] [2]

		MIN	MAX	UNIT
VIN	Supply voltage[1]	−0.3	20	V
VIN (10 ms Transient)			22	
OUT	Output voltage	−0.3	VIN + 0.3	V
OUT (Transient < 1 µs)			−1.2	V
ILIM	Voltage	−0.3	7	V
EN/UVLO		−0.3	7	
dV/dT		−0.3	7	
BFET		−0.3	30	
	Transient junction temperature	−65	T$_{SHDN}$	°C
T$_{stg}$	Storage temperature	−65	150	°C

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
(2) All voltage values, except differential voltages, are with respect to network ground terminal.

6.2 ESD Ratings

			MAX	UNIT
V$_{(ESD)}$	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001[1]	±2000	V
		Charged device model (CDM), per JEDEC specification JESD22-C101[2]	±500	

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	TYP	MAX	UNIT
VIN	Input voltage	4.5		18[1]	V
BFET		0		VIN+6	
dV/dT, EN/UVLO		0		6	
ILIM		0		3	
I$_{OUT}$	Continuous output current	0		5	A
ILIM	Resistance	10	100	162	kΩ
OUT	External capacitance	0.1	1	1000	µF
dV/dT			1	1000	nF
T$_J$	Operating junction temperature	−40	25	125	°C
T$_A$	Operating Ambient temperature	−40	25	85	°C

(1) Maximum voltage (including input transients) at VIN pin must not exceed absolute maximum rating as specified in the *Absolute Maximum Ratings* table.

6.4 Thermal Information[1]

over operating free-air temperature range (unless otherwise noted)

THERMAL METRIC		TPS25927x DRC (VSON) 10 PINS	UNIT
$R_{\theta JA}$	Junction-to-ambient thermal resistance	45.9	°C/W
$R_{\theta JCtop}$	Junction-to-case (top) thermal resistance	53	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	21.2	°C/W
ψ_{JT}	Junction-to-top characterization parameter	1.2	°C/W
ψ_{JB}	Junction-to-board characterization parameter	21.4	°C/W
$R_{\theta JCbot}$	Junction-to-case (bottom) thermal resistance	5.9	°C/W

(1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report.

6.5 Electrical Characteristics

−40°C ≤ T_J ≤ +125°C, VIN = 12 V, $V_{EN/UVLO}$ = 2 V, R_{ILIM} = 100 kΩ, C_{dVdT} = OPEN. All voltages referenced to GND (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
VIN (INPUT SUPPLY)						
V_{UVR}	UVLO threshold, rising		4.15	4.3	4.45	V
V_{UVhyst}	UVLO hysteresis[1]			5%		
IQ_{ON}	Supply current	Enabled: EN/UVLO = 2 V	0.3	0.42	0.55	mA
IQ_{OFF}		EN/UVLO = 0 V		0.13	0.225	mA
EN/UVLO (ENABLE/UVLO INPUT)						
V_{ENR}	EN threshold voltage, rising		1.37	1.4	1.44	V
V_{ENF}	EN threshold voltage, falling		1.32	1.35	1.39	V
I_{EN}	EN Input leakage current	0 V ≤ V_{EN} ≤ 5 V	−100	0	100	nA
dV/dT (OUTPUT RAMP CONTROL)						
I_{dVdT}	dV/dT charging current[1]	V_{dVdT} = 0 V		220		nA
R_{dVdT_disch}	dV/dT discharging resistance	EN/UVLO = 0 V, I_{dVdT} = 10 mA sinking	50	73	100	Ω
$V_{dVdTmax}$	dV/dT Max capacitor voltage[1]			5.5		V
$GAIN_{dVdT}$	dV/dT to OUT gain[1]	ΔV_{dVdT}		4.85		V/V
ILIM (CURRENT LIMIT PROGRAMMING)						
I_{ILIM}	ILIM bias current[1]			10		µA
I_{OL}	Overload current limit[2]	R_{ILIM} = 10 kΩ, $V_{VIN–OUT}$ = 1 V		1.02		A
		R_{ILIM} = 45.3 kΩ, $V_{VIN–OUT}$ = 1 V	1.79	2.10	2.42	A
		R_{ILIM} = 100 kΩ, $V_{VIN–OUT}$ = 1 V	3.46	3.75	4.03	A
		R_{ILIM} = 150 kΩ, $V_{VIN–OUT}$ = 1 V	4.5	5.1	5.7	A
$I_{OL-R-Short}$		R_{ILIM} = 0 Ω, shorted resistor current limit (single point failure test: UL60950)[1]		0.84		A
$I_{OL-R-Open}$		R_{ILIM} = OPEN, open resistor current limit (single point failure test: UL60950)[1]		0.73		A
I_{SCL}	Short-circuit current limit[2]	R_{ILIM} = 10 kΩ, $V_{VIN–OUT}$ = 12 V		1		A
		R_{ILIM} = 45.3 kΩ, $V_{VIN–OUT}$ = 12 V	1.66	1.98	2.37	A
		R_{ILIM} = 100 kΩ, $V_{VIN–OUT}$ = 12 V	2.90	3.32	3.85	A
		R_{ILIM} = 150 kΩ, $V_{VIN–OUT}$ = 12 V	3.7	4.5	5.5	A
$RATIO_{FASTRIP}$	Fast-trip comparator level w.r.t. overload current limit[1]	$I_{FASTRIP}$: I_{OL}		160%		
$V_{OpenILIM}$	ILIM open resistor detect threshold[1]	V_{ILIM} Rising, R_{ILIM} = OPEN		3.1		V

(1) These parameters are provided for reference only and do not constitute part of TI's published device specifications for purposes of TI's product warranty.
(2) Pulsed testing techniques used during this test maintain junction temperature approximately equal to ambient temperature.

Electrical Characteristics (continued)

−40°C ≤ T_J ≤ +125°C, VIN = 12 V, $V_{EN\ /UVLO}$ = 2 V, R_{ILIM} = 100 kΩ, C_{dVdT} = OPEN. All voltages referenced to GND (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
OUT (PASS FET OUTPUT)						
$R_{DS(on)}$	FET ON resistance	T_J = 25°C	21	28	37	mΩ
		T_J = 125°C		39	48	
$I_{OUT-OFF-LKG}$	OUT Bias current in off state	$V_{EN/UVLO}$ = 0 V, V_{OUT} = 0 V (sourcing)	−5	0	1.2	μA
$I_{OUT-OFF-SINK}$		$V_{EN/UVLO}$ = 0 V, V_{OUT} = 300 mV (sinking)	10	15	20	
BFET (BLOCKING FET GATE DRIVER)						
I_{BFET}	BFET charging current[1]	V_{BFET} = V_{OUT}		2		μA
$V_{BFETmax}$	BFET clamp voltage[1]			V_{VIN} + 6.4		V
$R_{BFETdisch}$	BFET discharging resistance to GND	$V_{EN/UVLO}$ = 0 V, I_{BFET} = 100 mA	15	26	36	Ω
TSD (THERMAL SHUT DOWN)						
T_{SHDN}	TSD threshold, rising[1]			150		°C
$T_{SHDNhyst}$	TSD hysteresis[1]			10		°C
	Thermal fault: latched or auto-retry	TPS259270		Latched		
		TPS259271		Auto-retry		

6.6 Timing Requirements

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
T_{ON}	Turnon delay[1]	EN/UVLO → H to I_{VIN} = 100 mA, 1-A resistive load at OUT		220		μs
t_{OFFdly}	Turnoff delay[1]	EN↓ to BFET↓, C_{BFET} = 0		0.4		μs
dV/dT (OUTPUT RAMP CONTROL)						
t_{dVdT}	Output ramp time	EN/UVLO → H to OUT = 11.7 V, C_{dVdT} = 0	0.7	1	1.3	ms
		EN/UVLO → H to OUT = 11.7 V, C_{dVdT} = 1 nF[1]		12		
ILIM (CURRENT LIMIT PROGRAMMING)						
$t_{FastOffDly}$	Fast-trip comparator delay[1]	I_{OUT} > $I_{FASTRIP}$ to I_{OUT} = 0 (Switch off)		300		ns
BFET (BLOCKING FET GATE DRIVER)						
$t_{BFET-ON}$	BFET turnon duration[1]	EN/UVLO → H to V_{BFET} = 12 V, C_{BFET} = 1 nF		4.2		ms
		EN/UVLO → H to VB_{FET} = 12 V, C_{BFET} = 10 nF		42		
$t_{BFET-OFF}$	BFET Turnoff duration[1]	EN/UVLO → L to $_{V}BFET$ = 1 V, C_{BFET} = 1 nF		0.4		μs
		EN/UVLO → L to V_{BFET} = 1 V, C_{BFET} = 10 nF		1.4		
Thermal Shutdown (TSD)						
t_{TSDdly}	Retry delay after TSD recovery, T_J < [T_{SHDN} − 10°C][1]	TPS259271 only		100		μs

(1) These parameters are provided for reference only and do not constitute part of TI's published device specifications for purposes of TI's product warranty.

6.7 Typical Characteristics

T_J = 25°C, V_{VIN} = 12 V, $V_{EN/UVLO}$ = 2 V, R_{ILIM} = 100 kΩ, C_{VIN} = 0.1 µF, C_{OUT} = 1 µF, C_{dVdT} = OPEN (unless stated otherwise)
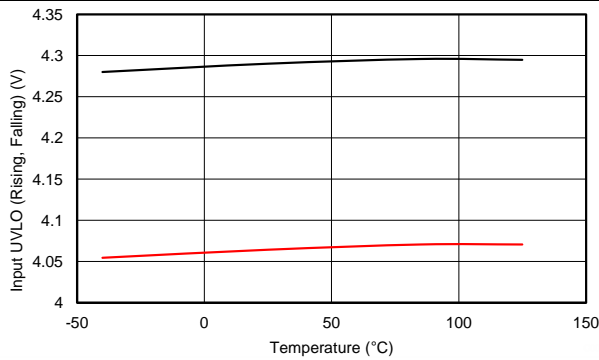
Figure 1. Input UVLO vs Temperature
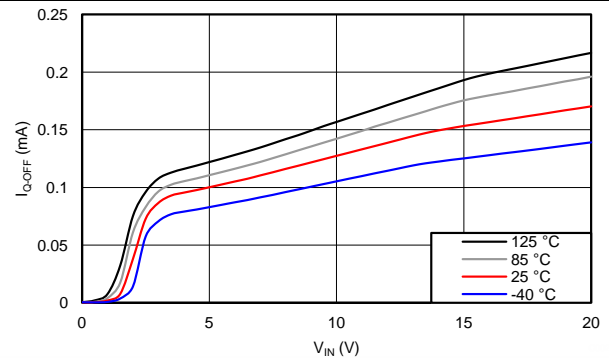
Figure 2. I_{Q-OFF} vs V_{IN}
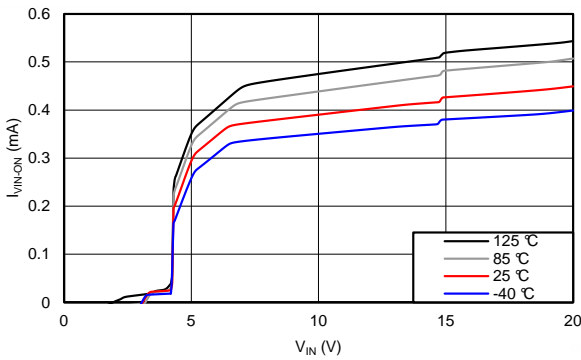
Figure 3. I_{VIN-ON} vs V_{IN}
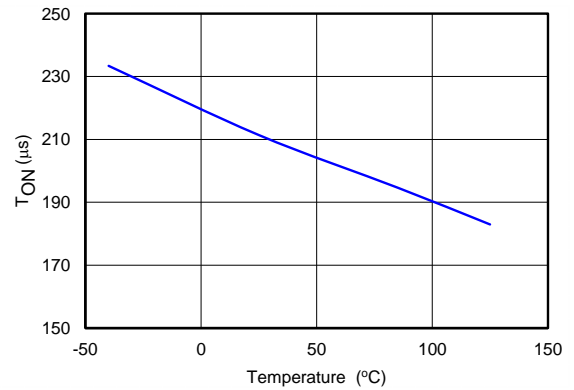
Figure 4. T_{ON} vs Temperature
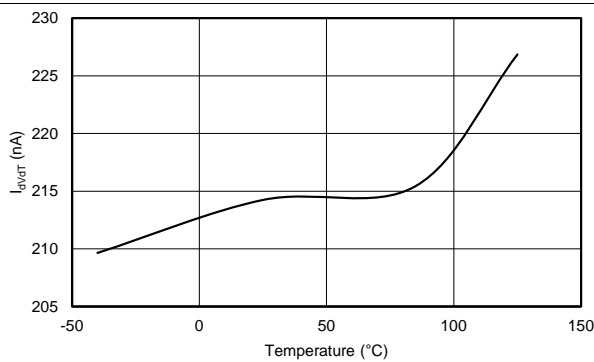
Figure 5. I_{dVdT} vs Temperature
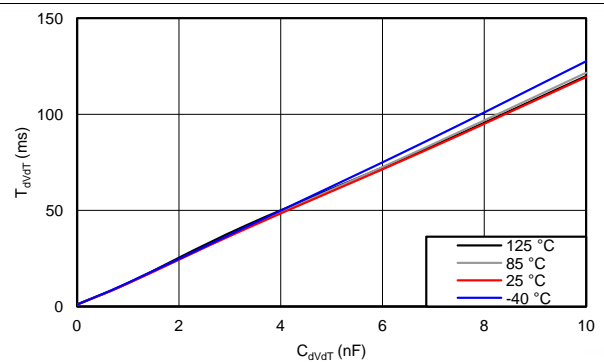
Figure 6. T_{dVdT} vs C_{dVdT}

Typical Characteristics (continued)

T_J = 25°C, V_{VIN} = 12 V, $V_{EN/UVLO}$ = 2 V, R_{ILIM} = 100 kΩ, C_{VIN} = 0.1 µF, C_{OUT} = 1 µF, C_{dVdT} = OPEN (unless stated otherwise)
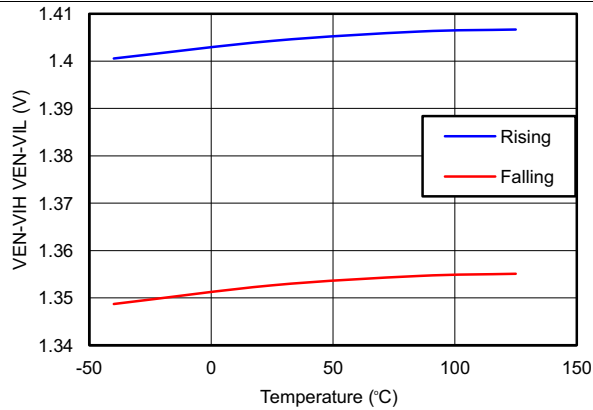
Figure 7. V_{EN-VIH}, V_{EN-VIL} vs Temperature
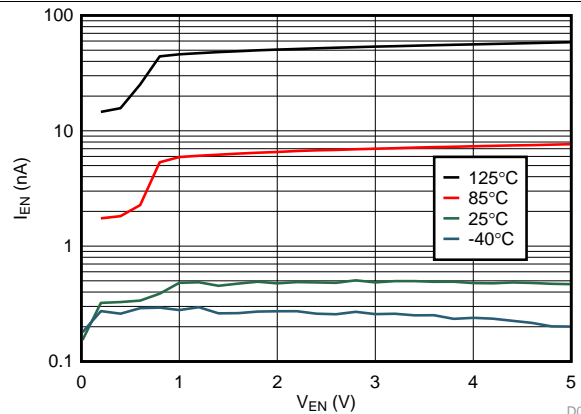
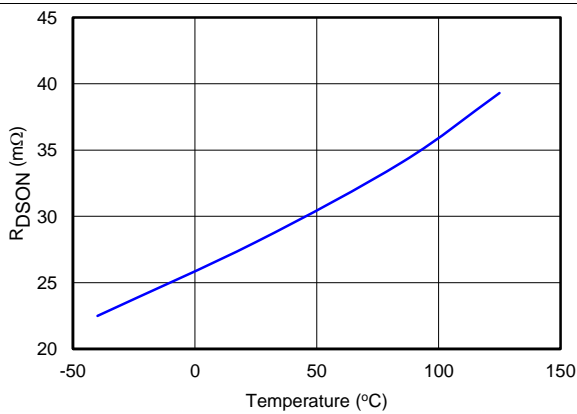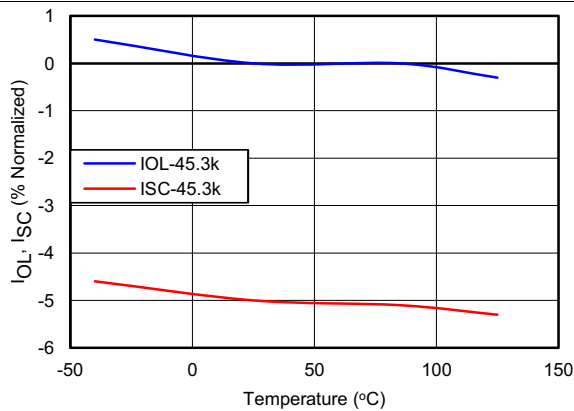**Figure 8. I_{EN} (Leakage Current) vs V_{EN}**
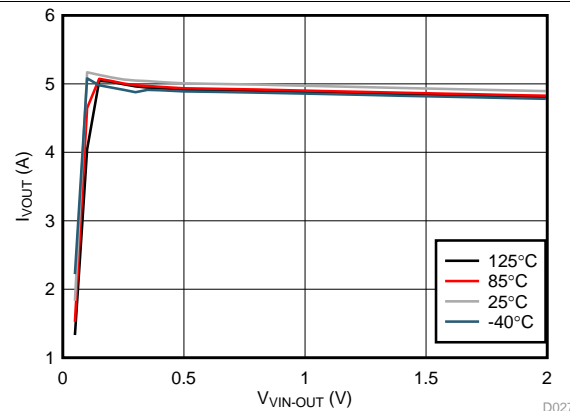

Figure 9. R_{DSON} vs Temperature
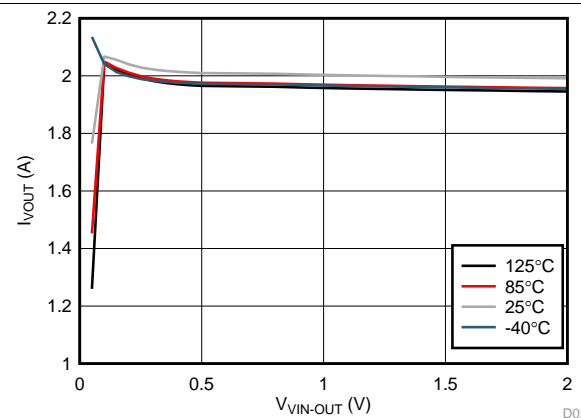
R_{ILIM} = 45.3 kΩ

Figure 10. I_{VOUT} vs $V_{VIN-OUT}$

R_{ILIM} = 45.3 kΩ

Figure 11. I_{OL}, I_{SC} vs Temperature

R_{ILIM} = 150 kΩ

Figure 12. I_{VOUT} vs $V_{VIN-OUT}$

Typical Characteristics (continued)

$T_J = 25°C$, $V_{VIN} = 12$ V, $V_{EN/UVLO} = 2$ V, $R_{ILIM} = 100$ kΩ, $C_{VIN} = 0.1$ µF, $C_{OUT} = 1$ µF, $C_{dVdT} = OPEN$ (unless stated otherwise)

$R_{ILIM} = 150$ kΩ

Figure 13. I_{OL}, I_{SC} vs Temperature

$R_{ILIM} = 100$ kΩ

Figure 14. I_{VOUT} vs $V_{VIN-OUT}$

$R_{ILIM} = 100$ kΩ

Figure 15. I_{OL}, I_{SC} vs Temperature

$R_{ILIM} = 0$ Ω

Figure 16. $I_{OL-R-Short}$ vs Temperature

$R_{ILIM} = OPEN$

Figure 17. $I_{OL-R-Open}$ vs Temperature

Figure 18. Overload Current Limit vs RILIM Resistor
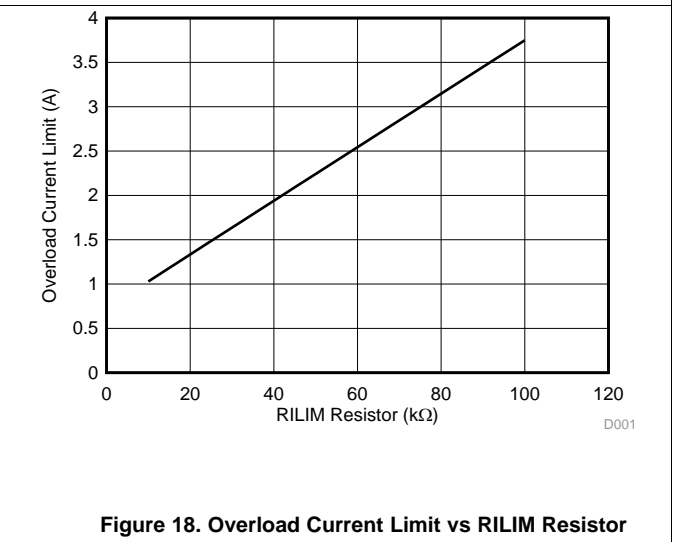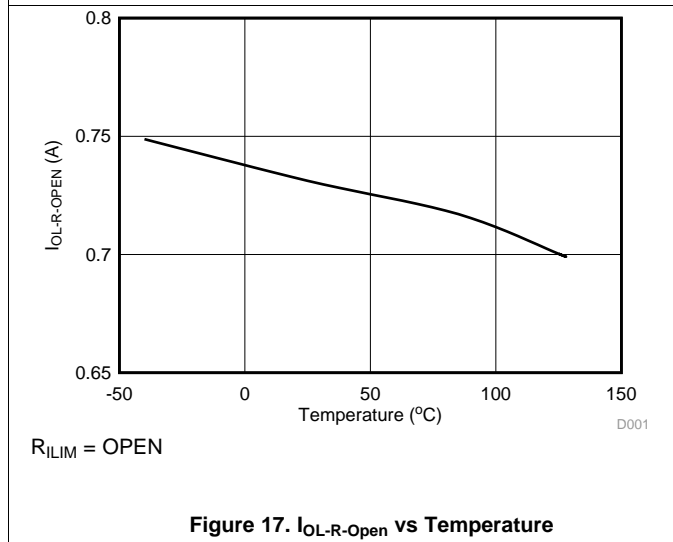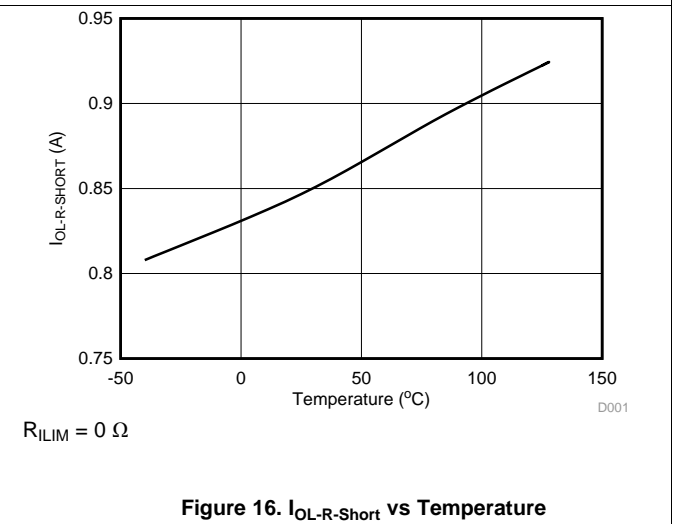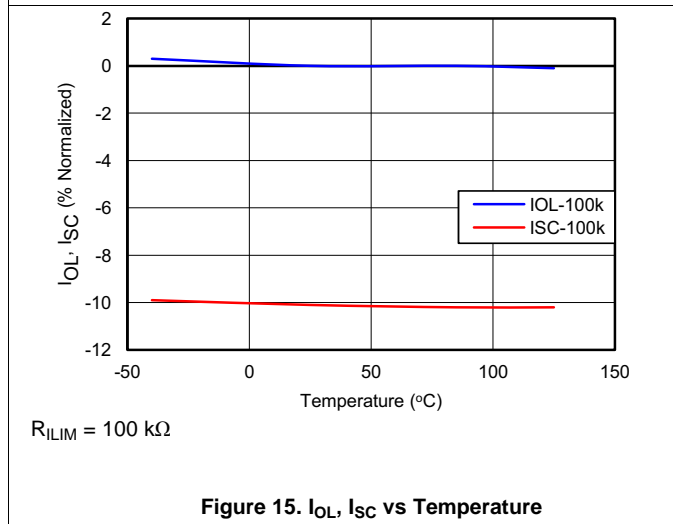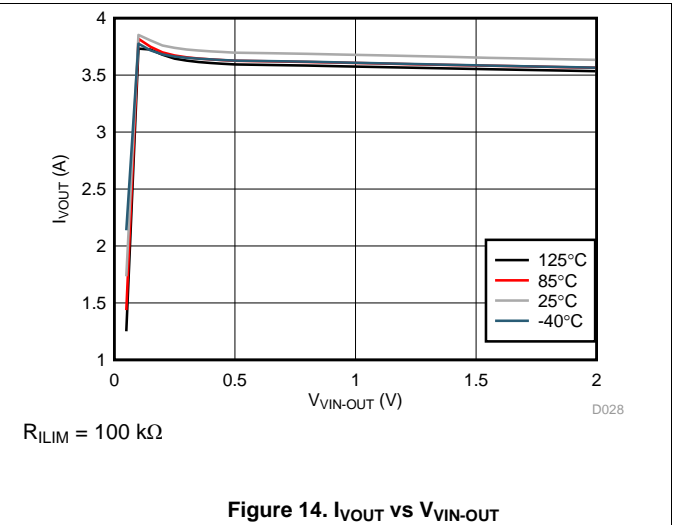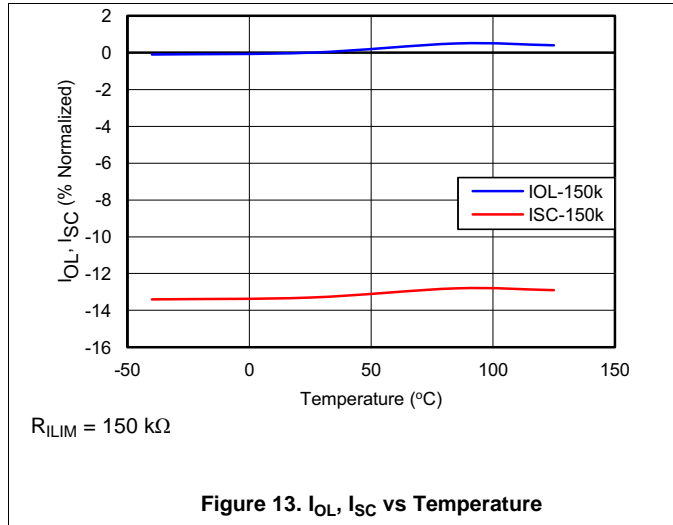
Typical Characteristics (continued)

T_J = 25°C, V_{VIN} = 12 V, $V_{EN/UVLO}$ = 2 V, R_{ILIM} = 100 kΩ, C_{VIN} = 0.1 µF, C_{OUT} = 1 µF, C_{dVdT} = OPEN (unless stated otherwise)

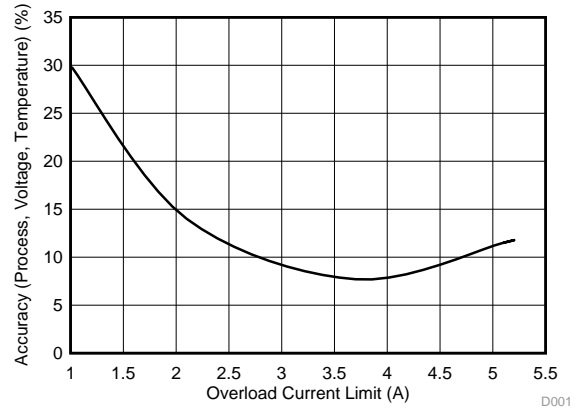**Figure 19. $V_{OpenILIM}$ vs Temperature**
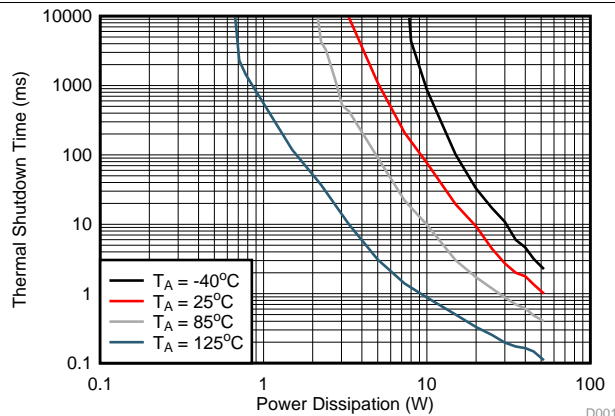

Figure 20. Accuracy vs Overload Current Limit

Figure 21. Thermal Shutdown Time vs Power Dissipation
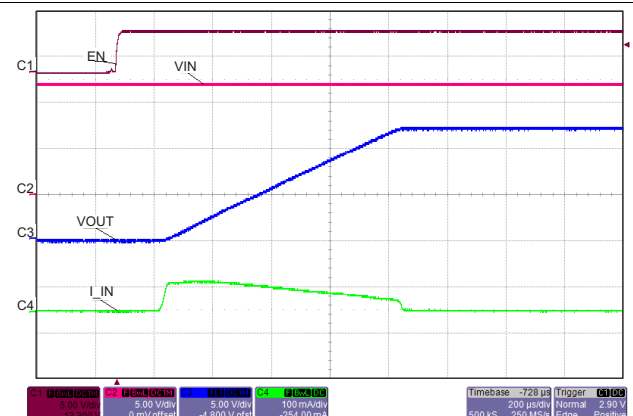
TPS25927x, C_{dVdT} = OPEN, C_{OUT} = 4.7 µF

Figure 22. Transient: Output Ramp
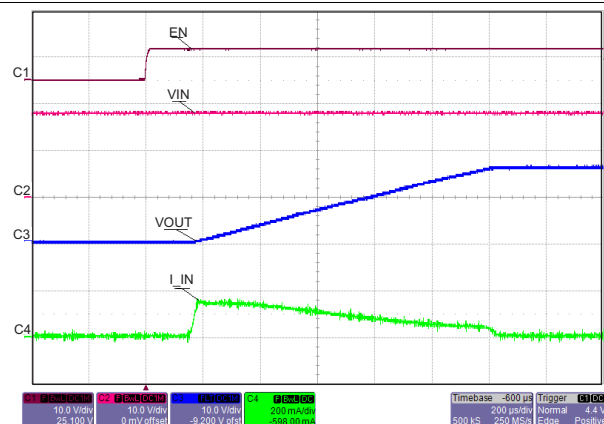
TPS25927x, VIN = 18 V, C_{dVdT} = OPEN, C_{OUT} = 10 µF

Figure 23. Transient: Output Ramp
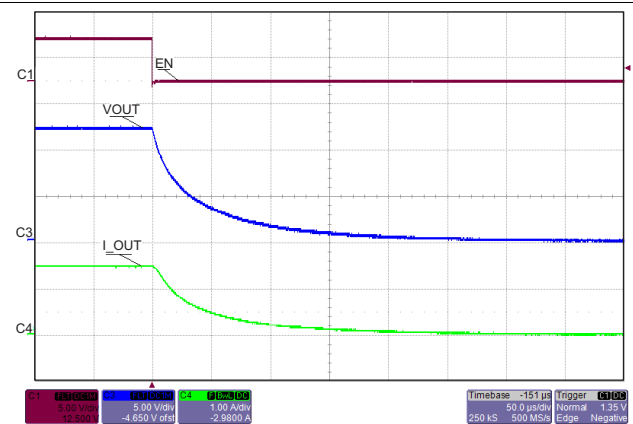
EN ↓

Figure 24. Transient: Turnoff Delay

Typical Characteristics (continued)

T_J = 25°C, V_{VIN} = 12 V, $V_{EN/UVLO}$ = 2 V, R_{ILIM} = 100 kΩ, C_{VIN} = 0.1 µF, C_{OUT} = 1 µF, C_{dVdT} = OPEN (unless stated otherwise)

EN ↓
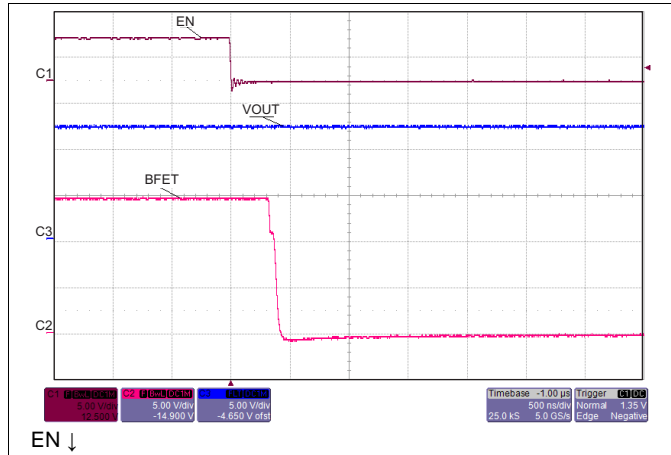
Figure 25. Turnoff Delay to BFET

VIN ↓
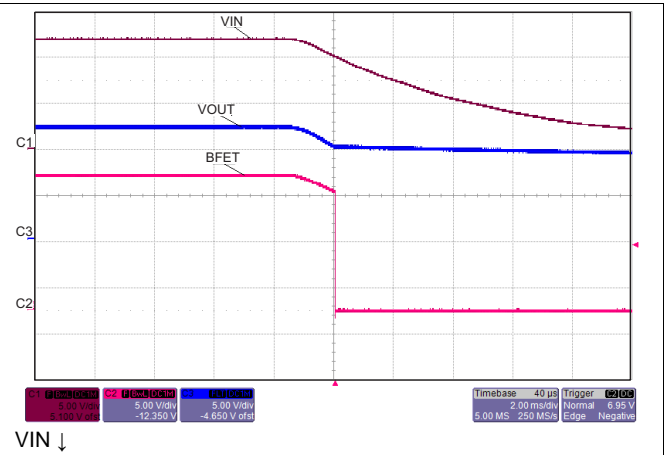
Figure 26. Turnoff Delay to BFET
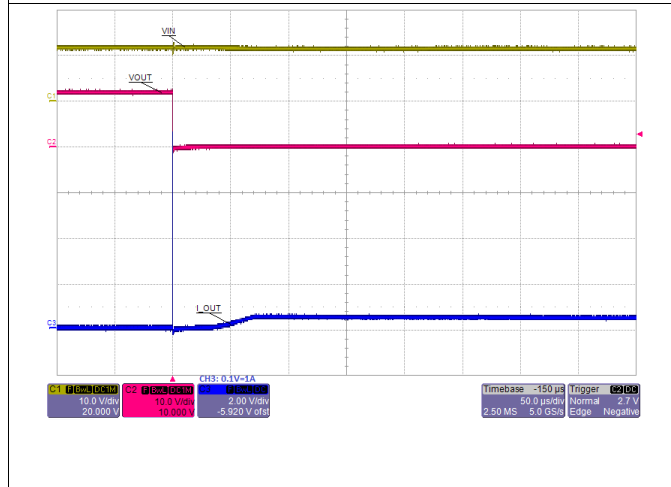
Figure 27. Transient: Output Short Circuit
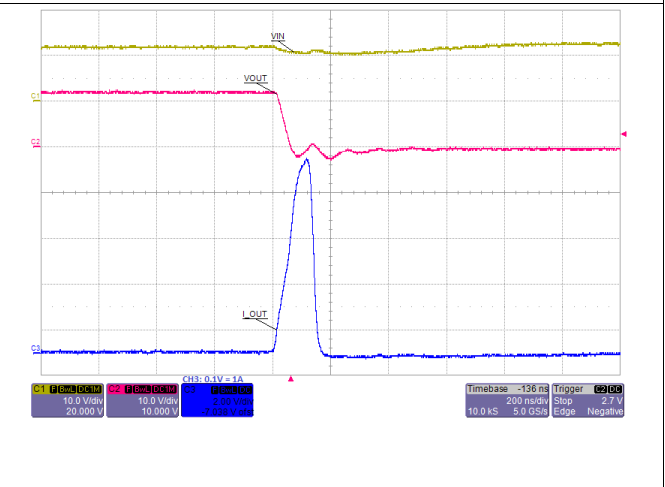
Figure 28. Short Circuit (Zoom): Fast-Trip Comparator

TPS259271
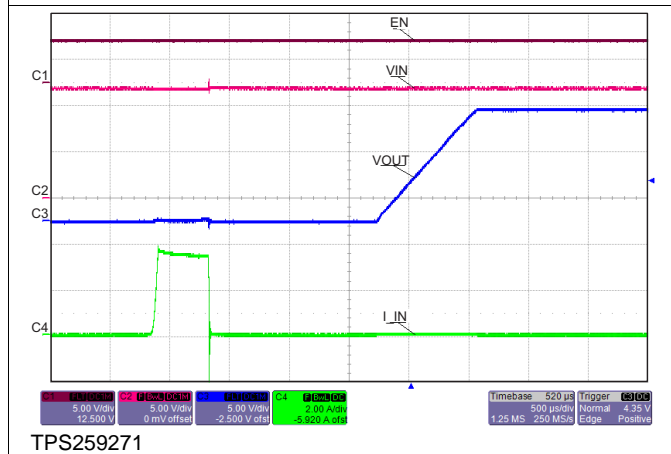
Figure 29. Transient: Recovery from Short Circuit-Over Current
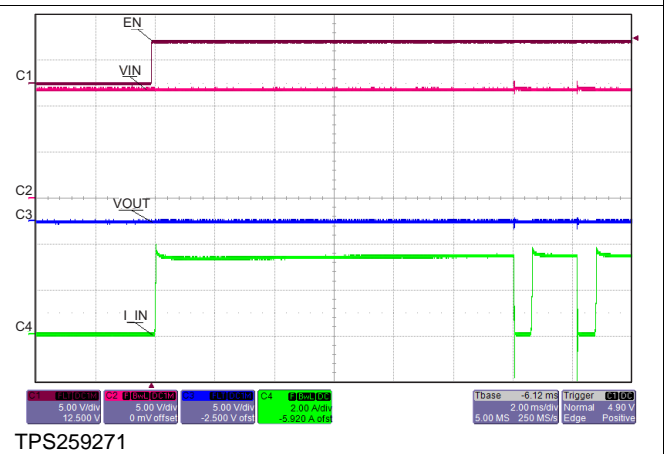
TPS259271

Figure 30. Transient: Wake Up to Short Circuit

Typical Characteristics (continued)

T_J = 25°C, V_{VIN} = 12 V, $V_{EN/UVLO}$ = 2 V, R_{ILIM} = 100 kΩ, C_{VIN} = 0.1 µF, C_{OUT} = 1 µF, C_{dVdT} = OPEN (unless stated otherwise)

I_{LOAD} Stepped from 50% to 120%, Back to 50%

Figure 31. Transient: Overload Current Limit

TPS259271

Figure 32. Transient: Thermal Fault Auto-Retry

TPS259270, VIN = 5 V

Figure 33. Transient: Thermal Fault Latched
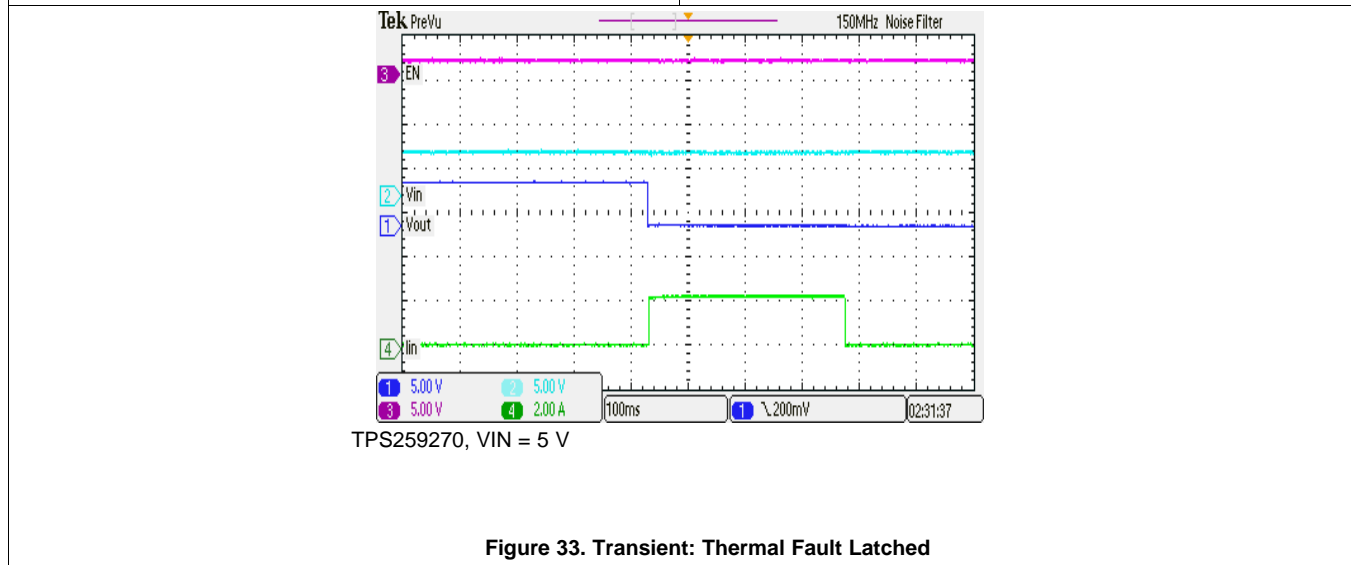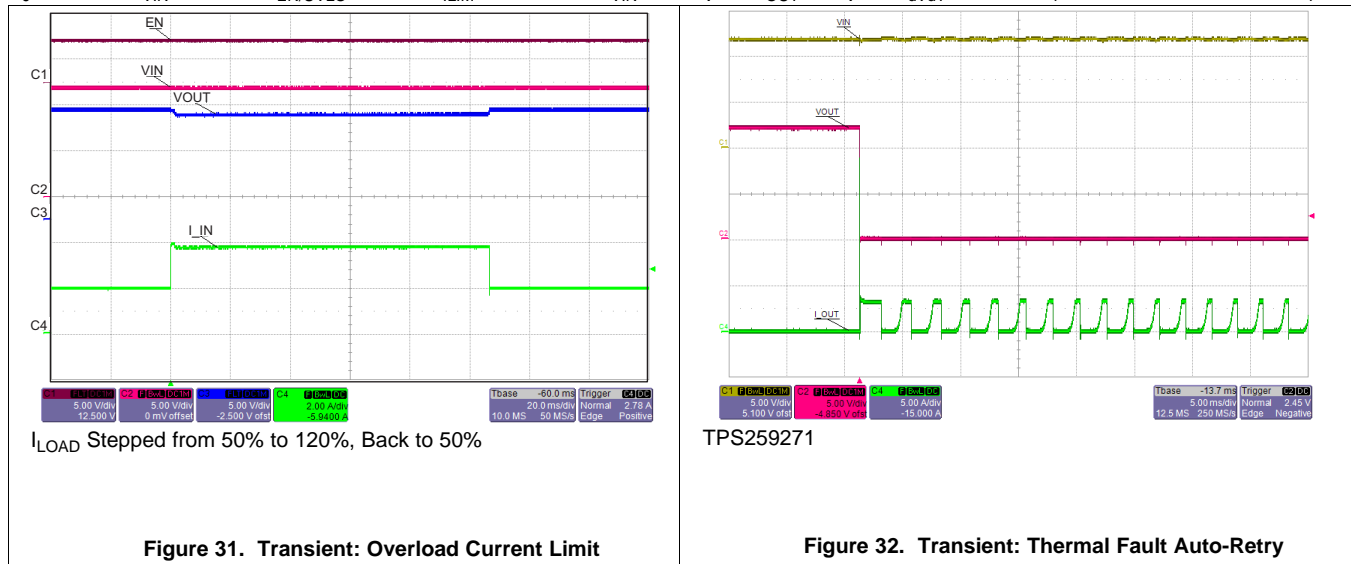
7 Detailed Description

7.1 Overview

The TPS25927x is an e-fuse with integrated power switch that is used to manage current, voltage and start-up voltage ramp to a connected load. The device starts its operation by monitoring the VIN bus. When VIN exceeds the undervoltage-lockout threshold (V_{UVR}), the device samples the EN/UVLO pin. A high level on this pin enables the internal MOSFET. As VIN rises, the internal MOSFET of the device starts conducting and allow current to flow from VIN to OUT. When EN/UVLO is held low (below V_{ENF}), internal MOSFET is turned off. User also has the ability to modify the output voltage ramp time by connecting a capacitor between dV/dT pin and GND.

After a successful start-up sequence, the device now actively monitors its load current, ensuring that the adjustable overload current limit I_{OL} is not exceeded. The device also has built-in thermal sensor. In the event device temperature (T_J) exceeds T_{SHDN}, typically 150°C, the thermal shutdown circuitry shuts down the internal MOSFET thereby disconnecting the load from the supply. In TPS259270, the output remains disconnected (MOSFET open) until power to device is recycled or EN/UVLO is toggled (pulled low and then high). The TPS259271 device remains off during a cooling period until device temperature falls below $T_{SHDN} - 10°C$, after which it attempts to restart. This ON and OFF cycle continues until fault is cleared.

7.2 Functional Block Diagram
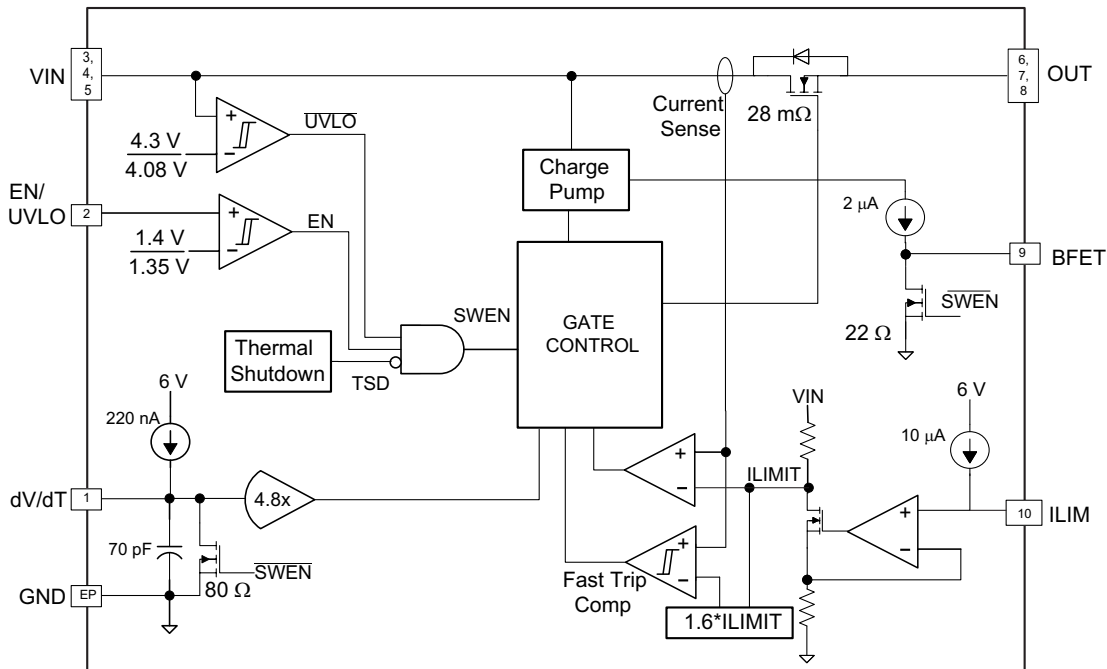
Copyright © 2017, Texas Instruments Incorporated

7.3 Feature Description

7.3.1 GND

This is the most negative voltage in the circuit and is used as a reference for all voltage measurements unless otherwise specified.

7.3.2 VIN

Input voltage to the TPS25927x. A ceramic bypass capacitor close to the device from VIN to GND is recommended to alleviate bus transients. The recommended operating voltage range is 4.5 V to 18 V for TPS25927x. The device can continuously sustain a voltage of 20 V on VIN pin. However, above the recommended maximum bus voltage, the device is going to be in over-voltage protection (OVP) mode, limiting the output voltage to V_{OVC}. The power dissipation in OVP mode is $P_{D\_OVP} = (V_{VIN} - V_{OVC}) \times I_{OUT}$, which can potentially heat up the device and cause thermal shutdown.

Feature Description (continued)

7.3.3 dV/dT

Connect a capacitor from this pin to GND to control the slew rate of the output voltage at power-on. This pin can be left floating to obtain a predetermined slew rate (minimum T_{dVdT}) on the output. Equation governing slew rate at start-up is shown in Equation 1:

$$\frac{dV_{OUT}}{dt} = \frac{I_{dVdT} \times GAIN_{dVdT}}{C_{dVdT} + C_{INT}}$$

where

- I_{dVdT} = 220 nA (Typical)
- C_{INT} = 70 pF (Typical)
- $GAIN_{dVdT}$ = 4.85

$$\frac{dV_{OUT}}{dT} = \text{Desired output slew rate}$$

(1)

The total ramp time (T_{dVdT}) for 0 to VIN can be calculated using Equation 2:

$$T_{dVdT} = 10^6 \times V_{IN} \times \left(C_{dVdT} + 70 \text{ pF}\right)$$

(2)

For details on how to select an appropriate charging time/rate, refer to the applications section *Setting Output Voltage Ramp Time (T_{dVdT})*.

7.3.4 BFET

Connect this pin to an external NFET that can be used to disconnect input supply from rest of the system in the event of power failure at VIN. The BFET pin is controlled by either input UVLO (V_{UVR}) event or EN/UVLO (see Table 2). BFET can source charging current of 2 µA (typical) and sink (discharge) current from the gate of the external FET via a 26-Ω internal discharge resistor to initiate fast turnoff, typically <1 µs. Due to 2-µA charging current, it is recommended to use >10 MΩ impedance when probing the BFET node.

Table 2. BFET

EN/UVLO > V_{ENR}	VIN>V_{UVR}	BFET MODE
H	H	Charge
X	L	Discharge
L	X	Discharge

7.3.5 EN/UVLO

As an input pin, it controls both the ON and OFF state of the internal MOSFET and that of the external blocking FET. In its high state, the internal MOSFET is enabled and charging begins for the gate of external FET. A low on this pin turns off the internal MOSFET and pull the gate of the external FET to GND via the built-in discharge resistor. High and Low levels are specified in the parametric table of the datasheet. The EN/UVLO pin is also used to clear a thermal shutdown latch in the TPS259270 by toggling this pin (H→L).

The internal de-glitch delay on EN/UVLO falling edge is intentionally kept low (1 us typical) for quick detection of power failure. When used with a resistor divider from supply to EN/UVLO to GND, power-fail detection on EN/UVLO helps in quick turnoff of the BFET driver, thereby stopping the flow of reverse current. For applications where a higher de-glitch delay on EN/UVLO is desired, or when the supply is particularly noisy, it is recommended to use an external bypass capacitor from EN/UVLO to GND.

7.3.6 ILIM

The device continuously monitors the load current and keeps it limited to the value programmed by R_{ILIM}. After start-up event and during normal operation, current limit is set to I_{OL} (over-load current limit). as shown in Equation 3:

$$I_{OL} = \left(0.7 + 3 \times 10^{-5} \times R_{ILIM}\right)$$

(3)

When power dissipation in the internal MOSFET [$P_D = (V_{VIN} - V_{OUT}) \times I_{OUT}$] exceeds 10 W, there is a 2% – 12% thermal foldback in the current limit value so that I_{OL} drops to I_{SC}. In each of the two modes, MOSFET gate voltage is regulated to throttle short-circuit and overload current flowing to the load. Eventually, the device shuts down due to over temperature. See Figure 34.
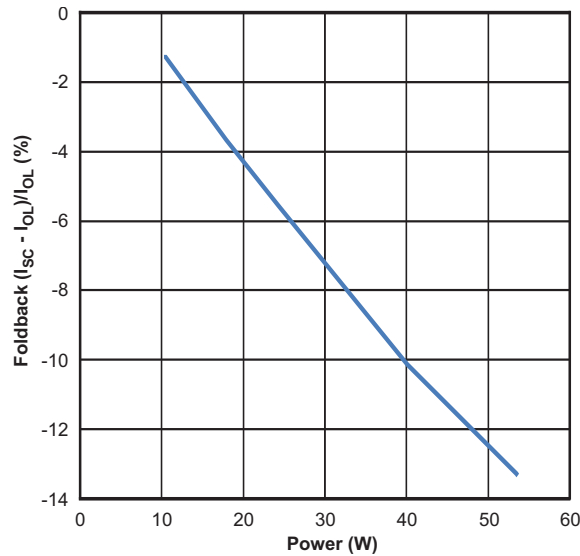
Figure 34. Thermal Foldback in Current Limit

During a transient short circuit event, the current through the device increases very rapidly. The current-limit amplifier cannot respond very quickly to this event due to its limited bandwidth. Therefore, the TPS25927x incorporates a fast-trip comparator, which shuts down the pass device very quickly when $I_{OUT} > I_{FASTRIP}$, and terminates the rapid short-circuit peak current. The trip threshold is set to 60% higher than the programmed over-load current limit ($I_{FASTRIP} = 1.6 \times I_{OL}$). After the transient short-circuit peak current has been terminated by the fast-trip comparator, the current limit amplifier smoothly regulates the output current to I_{OL} (see Figure 35 and Figure 36).
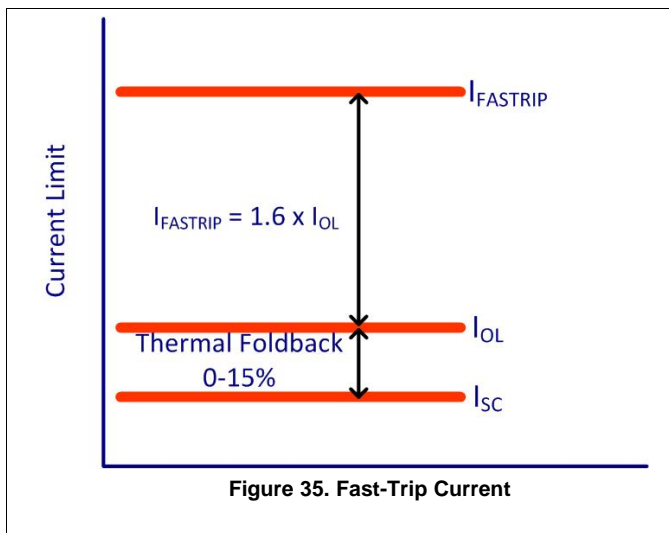
Figure 35. Fast-Trip Current
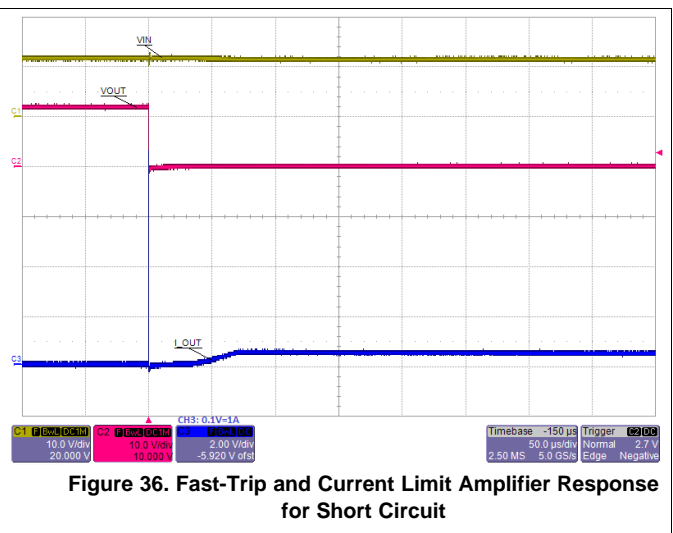
Figure 36. Fast-Trip and Current Limit Amplifier Response for Short Circuit

7.4 Device Functional Modes

The TPS25927x is a hot-swap controller with integrated power switch that is used to manage current, voltage and start-up voltage ramp to a connected load. The device starts its operation by monitoring the VIN bus. When V_{VIN} exceeds the undervoltage-lockout threshold (V_{UVR}), the device samples the EN/UVLO pin. A high level on this pin enables the internal MOSFET and also start charging the gate of external blocking FET (if connected) via the BFET pin. As VIN rises, the internal MOSFET of the device and external FET (if connected) starts conducting and allow current to flow from VIN to OUT. When EN/UVLO is held low (that is, below V_{ENF}), the internal MOSFET is turned off and BFET pin is discharged, thereby, blocking the flow of current from VIN to OUT. User also has the ability to modify the output voltage ramp time by connecting a capacitor between dV/dT pin and GND.

Having successfully completed its start-up sequence, the device now actively monitors its load current, ensuring that the adjustable overload current limit I_{OL} is not exceeded. This keeps the output device safe from harmful current transients. The device also has built-in thermal sensor. In the event device temperature (T_J) exceeds T_{SHDN} , typically 150°C, the thermal shutdown circuitry shuts down the internal MOSFET thereby disconnecting the load from the supply. In the TPS259270, the output remains disconnected (MOSFET open) until power to device is recycled or EN/UVLO is toggled (pulled low and then high). The TPS259271 device remains off during a cooling period until device temperature falls below $T_{SHDN} - 10°C$, after which it attempts to restart. This ON and OFF cycle continues until fault is cleared.

8 Application and Implementation

8.1 Application Information

The TPA25927x is a smart eFuse. It is typically used for Hot-Swap and Power rail protection applications. It operates from 4.5 V to 18 V with programmable current limit and undervoltage protection. The device aids in controlling the in-rush current and provides precise current limiting during overload conditions for systems such as Set-Top-Box, DTVs, Gaming Consoles, SSDs/HDDs and Smart Meters. The device also provides robust protection for multiple faults on the sub-system rail.

The following design procedure can be used to select component values for the device. Alternatively, the WEBENCH® software may be used to generate a complete design. The WEBENCH® software uses an iterative design procedure and accesses a comprehensive database of components when generating a design. Additionally, a spreadsheet design tool *TPS2592xx Design Calculator* (SLUC570) is available on web folder. This section presents a simplified discussion of the design process.

8.2 Typical Application

8.2.1 Simple 2.1-A eFuse Protection for Set Top Boxes
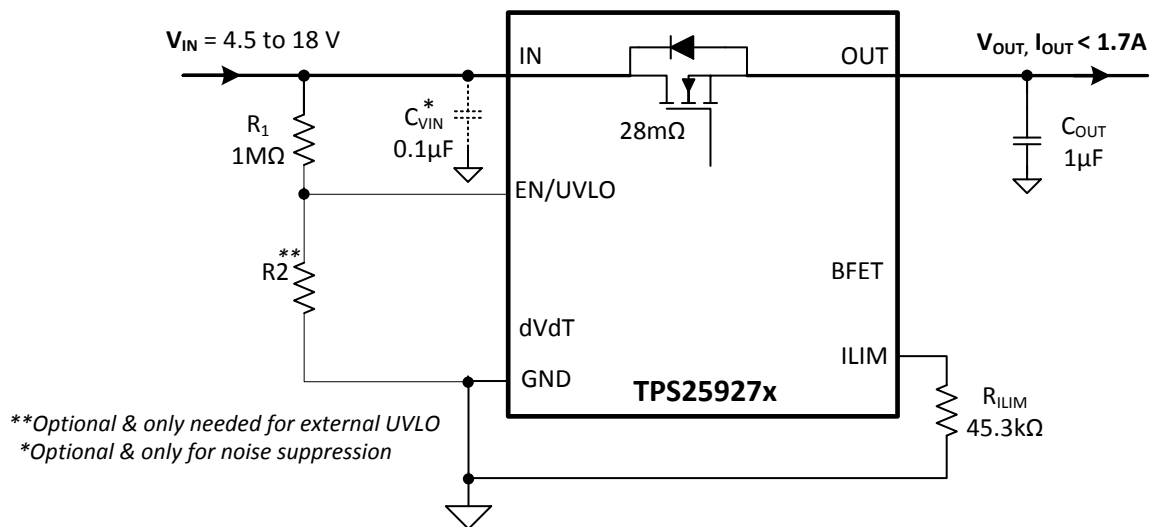
Figure 37. Typical Application Schematic: Simple e-Fuse for STBs

8.2.1.1 Design Requirements

Table 3 shows the design parameters for this application.

Table 3. Design Parameters

DESIGN PARAMETER	EXAMPLE VALUE
Input voltage range, V_{IN}	12 V
Undervoltage lockout set point, $V_{(UV)}$	Default: V_{UVR} = 4.3 V
Load at start-up, $R_{L(SU)}$	8 Ω
Current limit, $I_{OL} = I_{ILIM}$	2.1 A
Load capacitance, C_{OUT}	1 µF

Typical Application (continued)

Table 3. Design Parameters (continued)

DESIGN PARAMETER	EXAMPLE VALUE
Maximum ambient temperature, T_A	85°C

8.2.1.2 Detailed Design Procedure

The following design procedure can be used to select component values for the TPS25927x.

8.2.1.2.1 Step by Step Design Procedure

This design procedure below seeks to control the junction temperature of device under both static and transient conditions by proper selection of output ramp-up time and associated support components. The designer can adjust this procedure to fit the application and design criteria.

8.2.1.2.2 Programming the Current-Limit Threshold: R_{ILIM} Selection

The R_{ILIM} resistor at the ILIM pin sets the over load current limit, this can be set using Equation 4:

$$R_{ILIM} = \frac{I_{ILIM} - 0.7}{3 \times 10^{-5}}$$

(4)

For $I_{OL} = I_{ILIM} = 2.1$ A, from Equation 4, $R_{ILIM} = 45.3$ kΩ, choose closest standard value resistor with 1% tolerance.

8.2.1.2.3 Undervoltage Lockout Set Point

The undervoltage lockout (UVLO) trip point is adjusted using the external voltage divider network of R_1 and R_2 as connected between IN, EN/UVLO and GND pins of the device. The values required for setting the undervoltage are calculated solving Equation 5:

$$V_{(UV)} = \frac{R_1 + R_2}{R_2} \times V_{ENR}$$

(5)

Where $V_{ENR} = 1.4$ V is enable voltage rising threshold.

Since R_1 and R_2 leak the current from input supply (VIN), these resistors must be selected based on the acceptable leakage current from input power supply (VIN). The current drawn by R_1 and R_2 from the power supply {$I_{R12} = V_{IN}/(R_1 + R_2)$}.

However, leakage currents due to external active components connected to the resistor string can add error to these calculations. So, the resistor string current, I_{R12} must be chosen to be 20x greater than the leakage current expected.

For default UVLO of $V_{UVR} = 4.3$ V, select $R_2 = $ OPEN, and $R_1 = 1$ MΩ. Since EN/UVLO pin is rated only to 7 V, it cannot be connected directly to VIN = 12 V. It has to be connected through $R_1 = 1$ MΩ only, so that the pull-up current for EN/UVLO pin is limited to < 20 µA.

The power failure threshold is detected on the falling edge of supply. This threshold voltage is 4% lower than the rising threshold, V_{UVR}. This is calculated using Equation 6:

$$V_{(PFAIL)} = 0.96 \times V_{UVR}$$

(6)

Where V_{UVR} is 4.3 V, Power fail threshold set is : 4.1 V.

8.2.1.2.4 Setting Output Voltage Ramp Time (T_{dVdT})

For a successful design, the junction temperature of device must be kept below the absolute-maximum rating during both dynamic (start-up) and steady state conditions. Dynamic power stresses often are an order of magnitude greater than the static stresses, so it is important to determine the right start-up time and in-rush current limit required with system capacitance to avoid thermal shutdown during start-up with and without load.

The ramp-up capacitor C_{dVdT} needed is calculated considering the two possible cases:

8.2.1.2.4.1 Case 1: Start-Up without Load: Only Output Capacitance C_{OUT} Draws Current During Start-Up

During start-up, as the output capacitor charges, the voltage difference as well as the power dissipated across the internal FET decreases. The average power dissipated in the device during start-up is calculated using Equation 8.

For TPS25927x, the inrush current is determined using Equation 7:

$$I_{(INRUSH)} = C_{(OUT)} \text{ x } \frac{V_{(IN)}}{T_{dVdT}}$$

(7)

Power dissipation during start-up is given by Equation 8:

$$P_{D(INRUSH)} = 0.5 \text{ x } V_{(IN)} \text{ x } I_{(INRUSH)}$$

(8)

Equation 8 assumes that load does not draw any current until the output voltage has reached its final value.

8.2.1.2.4.2 Case 2: Start-Up with Load: Output Capacitance C_{OUT} and Load Draws Current During Start-Up

When load draws current during the turnon sequence, there is additional power dissipated. Considering a resistive load during start-up ($R_{L(SU)}$), load current ramps up proportionally with increase in output voltage during T_{dVdT} time. The average power dissipation in the internal FET during charging time due to resistive load is given by Equation 9:

$$P_{D(LOAD)} = \left(\frac{1}{6}\right) \text{ x } \frac{V^2_{(IN)}}{R_{L(SU)}}$$

(9)

Total power dissipated in the device during startup is given by Equation 10:

$$P_{D(STARTUP)} = P_{D(INRUSH)} + P_{D(LOAD)}$$

(10)

Total current during start-up is given by Equation 11:

$$I_{(STARTUP)} = I_{(INRUSH)} + I_L(t)$$

(11)

If $I_{(STARTUP)} > I_{OL}$, the device limits the current to I_{OL} and the current limited charging time is determined by Equation 12:

$$T_{dVdT(Current-Limited)} = C_{OUT} \text{ x } R_{L(SU)} \text{ x } \left[\frac{I_{OL}}{I_{(INRUSH)}} - 1 + LN\left(\frac{I_{(INRUSH)}}{I_{OL} - \frac{V_{(IN)}}{R_{L(SU)}}} \right) \right]$$

(12)

The power dissipation, with and without load, for selected start-up time must not exceed the shutdown limits as shown in Figure 38.
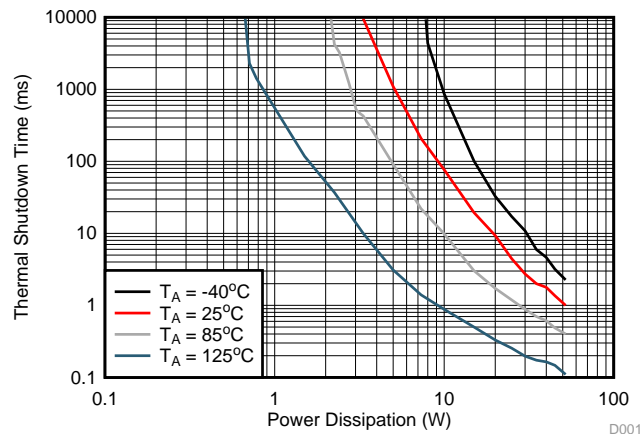

Figure 38. Thermal Shutdown Limit Plot

For the design example under discussion, select ramp-up capacitor C_{dVdT} = OPEN. Then, using Equation 2 we get Equation 13:

$$T_{dVdT} = 10^6 \text{ x } 12 \text{ x } (0 + 70 \text{ pF}) = 840 \text{ } \mu s \tag{13}$$

The inrush current drawn by the load capacitance (C_{OUT}) during ramp-up using Equation 7 is given by Equation 14:

$$I_{(INRUSH)} = 1 \text{ } \mu F \text{ x } \frac{12}{840 \text{ } \mu s} = 15 \text{ mA} \tag{14}$$

The inrush power dissipation is calculated, using Equation 8 as shown in Equation 15:

$$P_{D(INRUSH)} = 0.5 \text{ x } 12 \text{ x } 15 \text{ m} = 90 \text{ mW} \tag{15}$$

For 90 mW of power loss, the thermal shut down time of the device must not be less than the ramp-up time T_{dVdT} to avoid the false trip at maximum operating temperature. From thermal shutdown limit graph Figure 38 at T_A = 85°C, for 90 mW of power, the shutdown time is infinite. So it is safe to use 0.79 ms as start-up time without any load on output.

Considering the start-up with load 8 Ω, the additional power dissipation, when load is present during start-up is calculated, using Equation 9 we get Equation 16:

$$P_{D(LOAD)} = \frac{12 \text{ x } 12}{6 \times 8} = 3 \text{ W} \tag{16}$$

The total device power dissipation during start-up is given by Equation 17:

$$P_{D(STARTUP)} = 3 + 90 \text{ m} = 3.09 \text{ W} \tag{17}$$

From thermal shutdown limit graph at T_A = 85°C, the thermal shutdown time for 3.09 W is more than 100 ms. So it is well within acceptable limits to use no external capacitor ($C_{dV/dT}$) with start-up load of 8 Ω.

If, due to large C_{OUT}, there is a need to decrease the power loss during start-up, it can be done with increase of C_{dVdT} capacitor.

8.2.1.2.5 Support Component Selection—C_{VIN}

C_{VIN} is a bypass capacitor to help control transient voltages, unit emissions, and local supply noise. Where acceptable, a value in the range of 0.001 µF to 0.1 µF is recommended for C_{VIN}.

8.2.1.3 Application Curves

Figure 39. Output Ramp without Load on Output

Figure 40. Output Ramp with 4-Ω Load at Start-Up
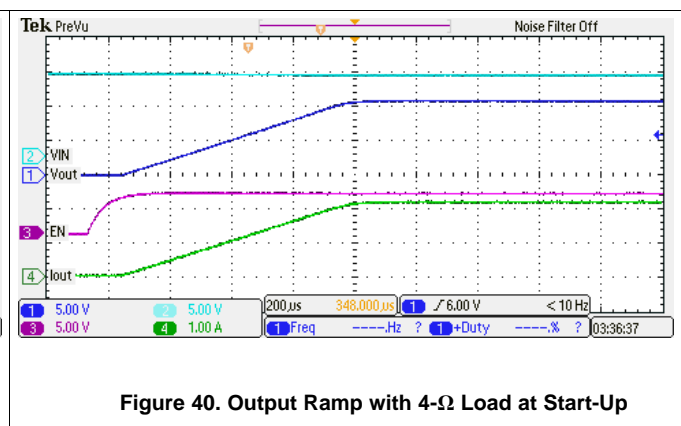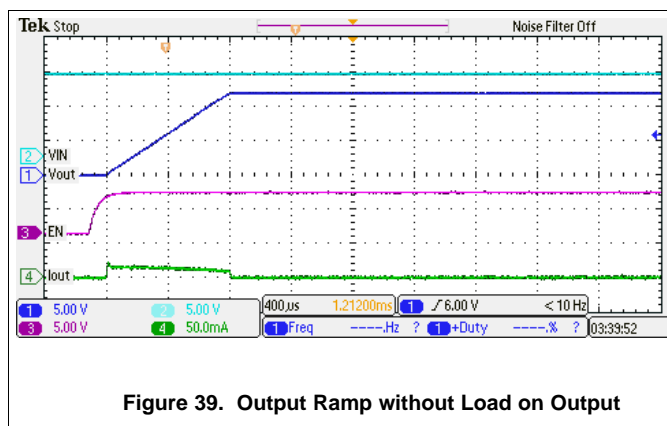
8.2.2 Controlled Power Down using TPS25927x

When the device is disabled, the output voltage is left floating and power down profile is entirely dictated by the load. In some applications, this can lead to undesired activity as the load is not powered down to a defined state. Controlled output discharge can ensure the load is turned off completely and not in an undefined operational state. The BFET pin in TPS25927x family of eFuses facilitates Quick Output Discharge (QOD) function as illustrated in Figure 41 . When the device is/gets disabled, the BFET pin pulls low which enables the external P-MOSFET Q1 for discharge feature to function. The output voltage discharge rate is dictated by the output capacitor C_{OUT}, the discharge resistance R_{DCHG} and the load.
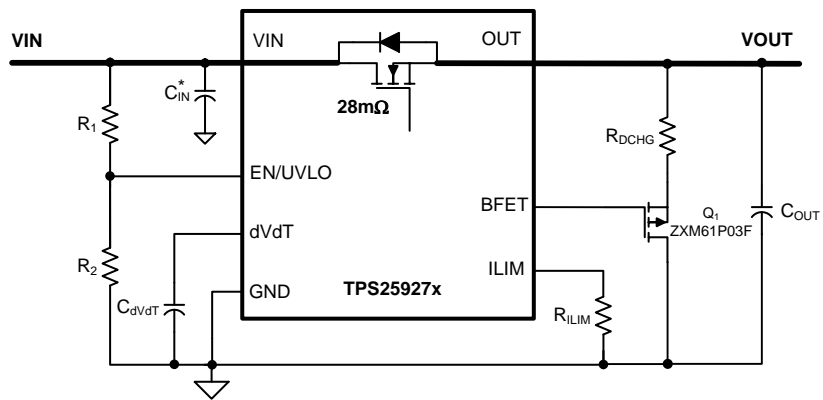
Optional & only for noise suppression

Figure 41. Circuit Implementation with Quick Output Discharge Function

9 Power Supply Recommendations

The device is designed for supply voltage range of 4.5 V ≤ V_{IN} ≤ 18 V. If the input supply is located more than a few inches from the device an input ceramic bypass capacitor higher than 0.1 μF is recommended. Power supply must be rated higher than the current limit set to avoid voltage droops during over current and short-circuit conditions.

9.1 Transient Protection

In case of short circuit and over load current limit, when the device interrupts current flow, input inductance generates a positive voltage spike on the input and output inductance generates a negative voltage spike on the output. The peak amplitude of voltage spikes (transients) is dependent on value of inductance in series to the input or output of the device. Such transients can exceed the *Absolute Maximum Ratings* of the device if steps are not taken to address the issue.

Typical methods for addressing transients include:
- Minimizing lead length and inductance into and out of the device
- Using large PCB GND plane
- Schottky diode across the output to absorb negative spikes
- A low value ceramic capacitor ($C_{(IN)}$ = 0.001 μF to 0.1 μF) to absorb the energy and dampen the transients. The approximate value of input capacitance can be estimated with Equation 18:

$$V_{SPIKE(Absolute)} = V_{(IN)} + I_{(LOAD)} \times \sqrt{\frac{L_{(IN)}}{C_{(IN)}}}$$

where

- $V_{(IN)}$ is the nominal supply voltage
- $I_{(LOAD)}$ is the load current
- $L_{(IN)}$ equals the effective inductance seen looking into the source
- $C_{(IN)}$ is the capacitance present at the input   (18)

Some applications may require the addition of a Transient Voltage Suppressor (TVS) to prevent transients from exceeding the *Absolute Maximum Ratings* of the device.

The circuit implementation with optional protection components (a ceramic capacitor, TVS and schottky diode) is shown in Figure 42.
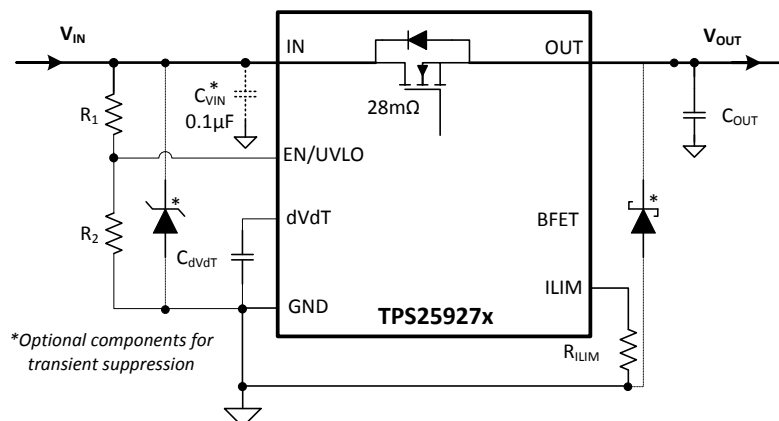
Figure 42. Circuit Implementation with Optional Protection Components

9.2 Output Short-Circuit Measurements

It is difficult to obtain repeatable and similar short-circuit testing results. Source bypassing, input leads, circuit layout and component selection, output shorting method, relative location of the short, and instrumentation all contribute to variation in results. The actual short itself exhibits a certain degree of randomness as it microscopically bounces and arcs. Care in configuration and methods must be used to obtain realistic results. Do not expect to see waveforms exactly like those in the data sheet; every setup differs.

10 Layout

10.1 Layout Guidelines

- For all applications, a 0.01-uF or greater ceramic decoupling capacitor is recommended between IN terminal and GND. For hot-plug applications, where input power path inductance is negligible, this capacitor can be eliminated/minimized.
- The optimum placement of decoupling capacitor is closest to the IN and GND terminals of the device. Care must be taken to minimize the loop area formed by the bypass-capacitor connection, the IN terminal, and the GND terminal of the IC. See Figure 43 for a PCB layout example.
- High current carrying power path connections must be as short as possible and must be sized to carry at least twice the full-load current.
- The GND terminal must be tied to the PCB ground plane at the terminal of the IC. The PCB ground must be a copper plane or island on the board.
- Locate all support components: R_{ILIM}, C_{dVdT} and resistors for EN/UVLO, close to their connection pin. Connect the other end of the component to the GND pin of the device with shortest trace length. The trace routing for the R_{ILIM} and C_{dVdT} components to the device must be as short as possible to reduce parasitic effects on the current limit and soft start timing. These traces must not have any coupling to switching signals on the board.
- Protection devices such as TVS, snubbers, capacitors, or diodes must be placed physically close to the device they are intended to protect, and routed with short traces to reduce inductance. For example, a protection Schottky diode is recommended to address negative transients due to switching of inductive loads, and it must be physically close to the OUT pins.
- Obtaining acceptable performance with alternate layout schemes is possible; however this layout has been shown to produce good results and is intended as a guideline.
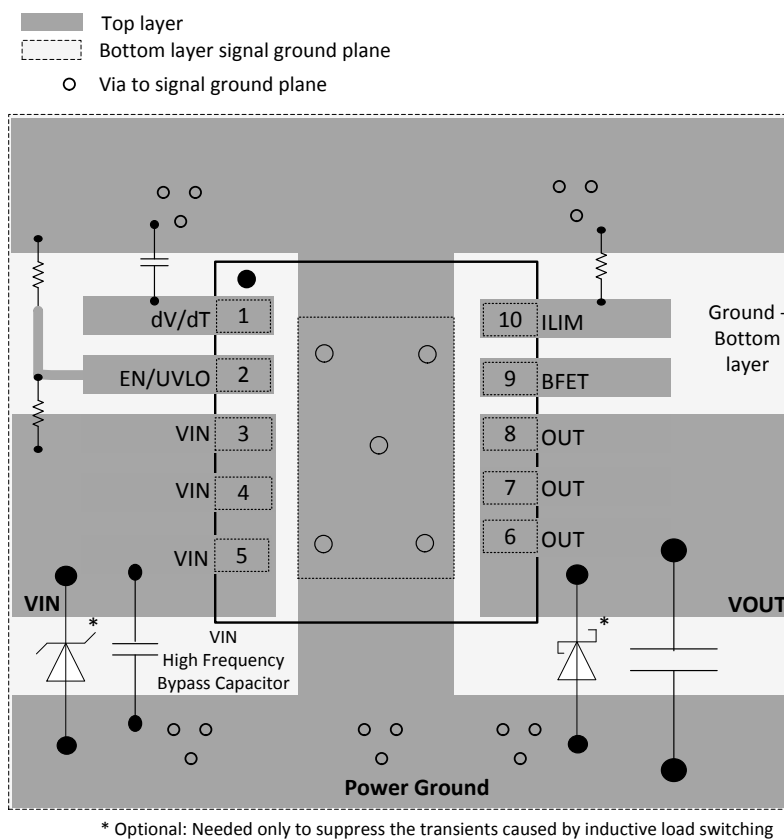
10.2 Layout Example

* Optional: Needed only to suppress the transients caused by inductive load switching

Figure 43. Layout Example

11 器件和文档支持

11.1 器件支持

11.1.1 Third-Party Products Disclaimer

TI'S PUBLICATION OF INFORMATION REGARDING THIRD-PARTY PRODUCTS OR SERVICES DOES NOT CONSTITUTE AN ENDORSEMENT REGARDING THE SUITABILITY OF SUCH PRODUCTS OR SERVICES OR A WARRANTY, REPRESENTATION OR ENDORSEMENT OF SUCH PRODUCTS OR SERVICES, EITHER ALONE OR IN COMBINATION WITH ANY TI PRODUCT OR SERVICE.

11.1.2 开发支持

有关 TPS259270 PSpice 瞬态模型，请参阅 SLVMB88

有关 TPS259271 PSpice 瞬态模型，请参阅 SLVMB91

11.2 文档支持

11.2.1 相关文档

请参阅如下相关文档：

《TPS2592xx 设计计算器》

11.3 相关链接

下面的表格列出了快速访问链接。类别包括技术文档、支持与社区资源、工具和软件，以及申请样片或购买产品的快速链接。

表 **4.** 相关链接

器件	产品文件夹	样片与购买	技术文档	工具和软件	支持和社区
TPS259270	请单击此处	请单击此处	请单击此处	请单击此处	请单击此处
TPS259271	请单击此处	请单击此处	请单击此处	请单击此处	请单击此处

11.4 接收文档更新通知

如需接收文档更新通知，请访问 ti.com 上的器件产品文件夹。单击右上角的*通知我* 进行注册，即可每周接收产品信息更改摘要。有关更改的详细信息，请查看任何已修订文档中包含的修订历史记录。

11.5 社区资源

下列链接提供到 TI 社区资源的连接。链接的内容由各个分销商"按照原样"提供。这些内容并不构成 TI 技术规范，并且不一定反映 TI 的观点；请参阅 TI 的 *《使用条款》*。

TI E2E™ 在线社区 *TI 的工程师对工程师 (E2E) 社区。*此社区的创建目的在于促进工程师之间的协作。在 e2e.ti.com 中，您可以咨询问题、分享知识、拓展思路并与同行工程师一道帮助解决问题。

设计支持 *TI 参考设计支持* 可帮助您快速查找有帮助的 E2E 论坛、设计支持工具以及技术支持的联系信息。

11.6 商标

E2E is a trademark of Texas Instruments.
WEBENCH is a registered trademark of Texas Instruments.
All other trademarks are the property of their respective owners.

11.7 静电放电警告

ESD 可能会损坏该集成电路。德州仪器 (TI) 建议通过适当的预防措施处理所有集成电路。如果不遵守正确的处理措施和安装程序，可能会损坏集成电路。

ESD 的损坏小至导致微小的性能降级，大至整个器件故障。 精密的集成电路可能更容易受到损坏，这是因为非常细微的参数更改都可能会导致器件与其发布的规格不相符。

11.8 Glossary

SLYZ022 — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

12 机械、封装和可订购信息

以下页面包含机械、封装和可订购信息。这些信息是指定器件的最新可用数据。这些数据如有变更，恕不另行通知和修订此文档。如欲获取此数据表的浏览器版本，请参阅左侧的导航。

PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TPS259270DRCR	ACTIVE	VSON	DRC	10	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 85	259270	Samples
TPS259270DRCT	ACTIVE	VSON	DRC	10	250	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 85	259270	Samples
TPS259271DRCR	ACTIVE	VSON	DRC	10	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 85	259271	Samples
TPS259271DRCT	ACTIVE	VSON	DRC	10	250	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 85	259271	Samples

(1) The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.
PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".
RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.
Green: TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

Important Information and Disclaimer: The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and

continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

TAPE AND REEL INFORMATION

REEL DIMENSIONS

TAPE DIMENSIONS

A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS259270DRCR	VSON	DRC	10	3000	330.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
TPS259270DRCT	VSON	DRC	10	250	180.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
TPS259271DRCR	VSON	DRC	10	3000	330.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
TPS259271DRCT	VSON	DRC	10	250	180.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2

TAPE AND REEL BOX DIMENSIONS

*All dimensions are nominal

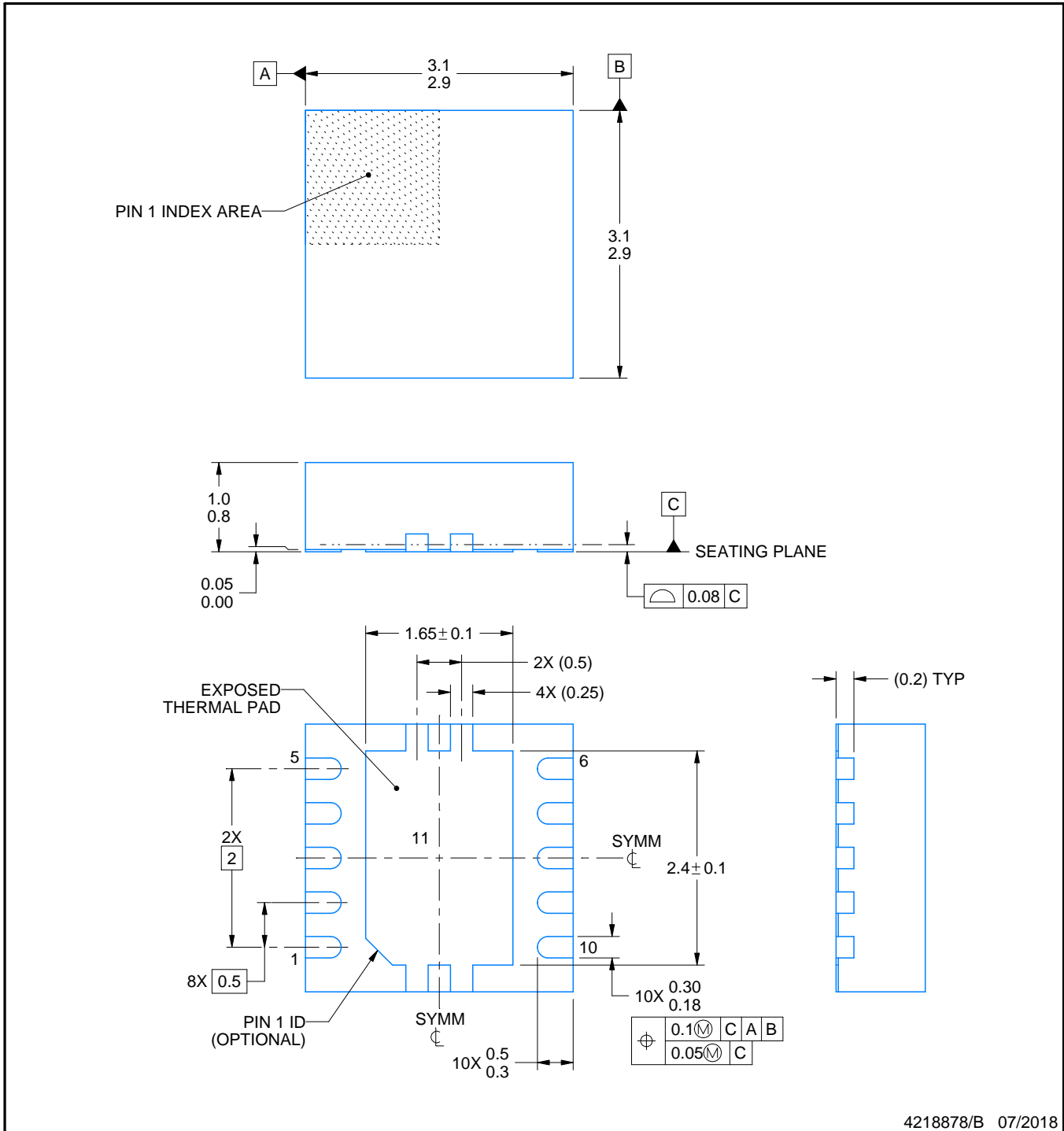| Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS259270DRCR	VSON	DRC	10	3000	346.0	346.0	33.0
TPS259270DRCT	VSON	DRC	10	250	210.0	185.0	35.0
TPS259271DRCR	VSON	DRC	10	3000	346.0	346.0	33.0
TPS259271DRCT	VSON	DRC	10	250	210.0	185.0	35.0

DRC 10

3 x 3, 0.5 mm pitch

This image is a representation of the package family, actual package may vary.
Refer to the product data sheet for package details.

4226193/A

A

3.1
2.9

B

PIN 1 INDEX AREA

3.1
2.9

1.0
0.8

C

SEATING PLANE

0.05
0.00

⬠ 0.08 C

1.65± 0.1

2X (0.5)

4X (0.25)

EXPOSED
THERMAL PAD

(0.2) TYP

5

6

2X
2

11

SYMM
₵

2.4± 0.1

1

10

8X 0.5

10X 0.30
0.18

PIN 1 ID
(OPTIONAL)

SYMM
₵

⊕ 0.1Ⓜ C A B
0.05Ⓜ C

10X 0.5
0.3
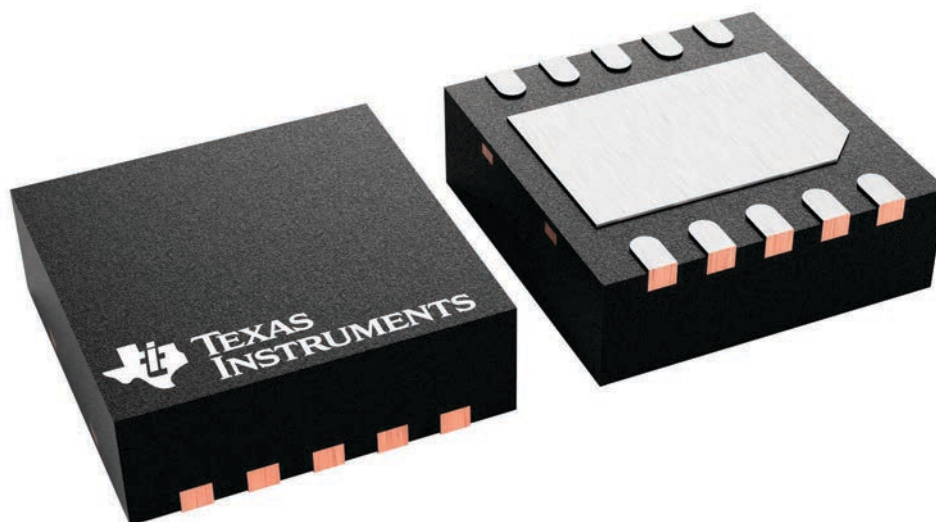
4218878/B   07/2018

NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for optimal thermal and mechanical performance.

(1.65)

(0.5)

10X (0.6)

1

10X (0.24)

10

SYMM
₵

11

(2.4)

(3.4)

8X (0.5)

(0.95)

5

6

(R0.05) TYP

(∅ 0.2) VIA
TYP

(0.25)

(0.575)

SYMM
₵

(2.8)

LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE:20X

0.07 MAX
ALL AROUND

EXPOSED METAL

0.07 MIN
ALL AROUND

EXPOSED METAL

SOLDER MASK
OPENING

METAL

METAL UNDER
SOLDER MASK

SOLDER MASK
OPENING

NON SOLDER MASK
DEFINED
(PREFERRED)

SOLDER MASK
DEFINED

SOLDER MASK DETAILS

4218878/B   07/2018

NOTES: (continued)

4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature
   number SLUA271 (www.ti.com/lit/slua271).
5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown
   on this view. It is recommended that vias under paste be filled, plugged or tented.

2X (1.5)

(0.5)

SYMM

EXPOSED METAL
TYP

11

10X (0.6)

1

10X (0.24)

SYMM

10

2X (1.53)

(1.06)

(0.63)

8X (0.5)

5

6

(R0.05) TYP

4X (0.34)

4X (0.25)

(2.8)

SOLDER PASTE EXAMPLE
BASED ON 0.125 mm THICK STENCIL

EXPOSED PAD 11:
80% PRINTED SOLDER COVERAGE BY AREA
SCALE:25X

4218878/B   07/2018

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate
   design recommendations.

重要声明和免责声明