

# TI Designs: TIDA-01535

## 适用于电源隔离式超紧凑型模拟输出模块的参考设计



### 说明

该单通道电源隔离式模拟输出模块参考设计使用高度集成的 DAC8771 数模转换器 (DAC) 提供电流和电压输出。DAC8771 的高集成度与 LM25180 初级侧调节反激式转换器相结合, 实现了板尺寸为 52mm x 40mm、最大组件高度为 4mm 的紧凑型隔离式设计。此外, 该设计采用外部电路来提供电磁干扰 (EMI) 和电磁兼容性 (EMC) 瞬态保护。

### 资源

<a href="#">TIDA-01535</a>	设计文件夹
<a href="#">DAC8771</a>	产品文件夹
<a href="#">LM25180</a>	产品文件夹
<a href="#">ISO7741</a>	产品文件夹
<a href="#">ISO7721</a>	产品文件夹

### 特性

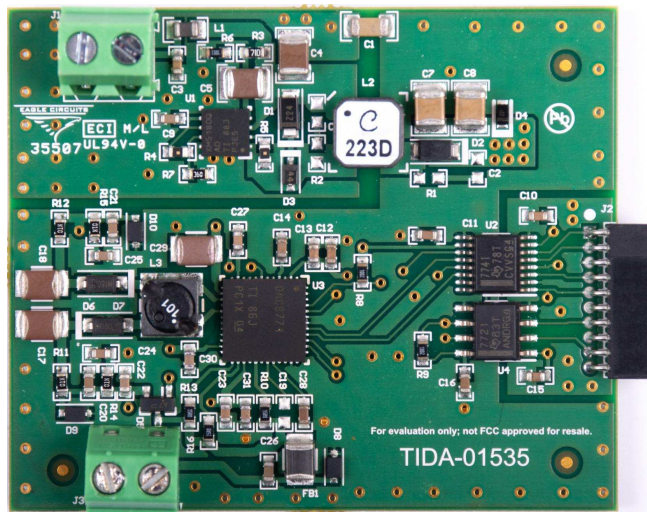
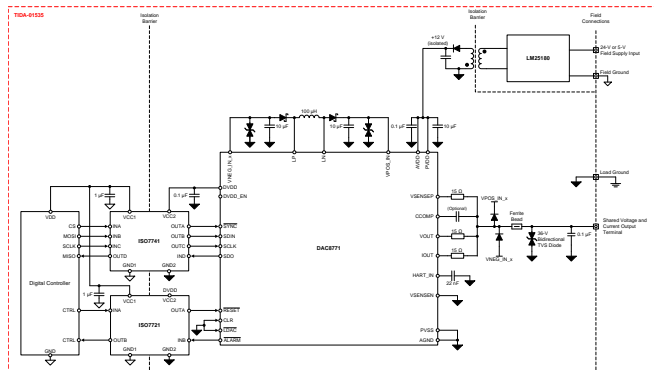
- 适用于工厂自动化和控制的隔离式模拟输出
- 16 位分辨率
- 数字输入隔离
- -24mA 至 +24mA 电流输出
- ±12V 电压输出
- 12V 至 42V 电源输入
- 针对电流输出的自适应电源管理
- 紧凑型设计: 52mm x 40mm

### 应用

- 工厂自动化和控制
- 楼宇自动化
- 电机驱动器
- 电网基础设施: 保护继电器、DCIO 模块



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## 1 System Description

This analog output design accepts a standard industrial supply voltage of 12 V to 42 V. The system features a 16-bit voltage ( $\pm 12$  V) or current output ( $\pm 24$  mA), with a total unadjusted error (TUE) of less than 0.1% full-scale range (FSR). The use of an isolated power supply maintains the functional isolation from the power and data inputs to the output. The included external circuitry provides protection against transient electromagnetic interference (EMI). The system uses adaptive power management to minimize power and heat dissipation in the DAC8771, which improves accuracy by reducing self-heating and enabling smaller system enclosures.

### 1.1 Key System Specifications

表 1. Key System Specifications

PARAMETER	SPECIFICATIONS	DETAILS
Supply voltage	12 V to 42 V	<a href="#">节 2.2.3</a>
Input	Four-wire serial peripheral interface (SPI) – isolated	<a href="#">节 2.2.1</a>
Voltage output	$\pm 12$ V	<a href="#">节 2.2.1</a>
Current output	-24 mA to +24 mA	<a href="#">节 2.2.1</a>
Total unadjusted error (TUE)	0.1% FSR	<a href="#">节 2.2.1</a>
Maximum component height	< 4 mm	<a href="#">节 2.2.3</a>

## 2 System Overview

### 2.1 Block Diagram

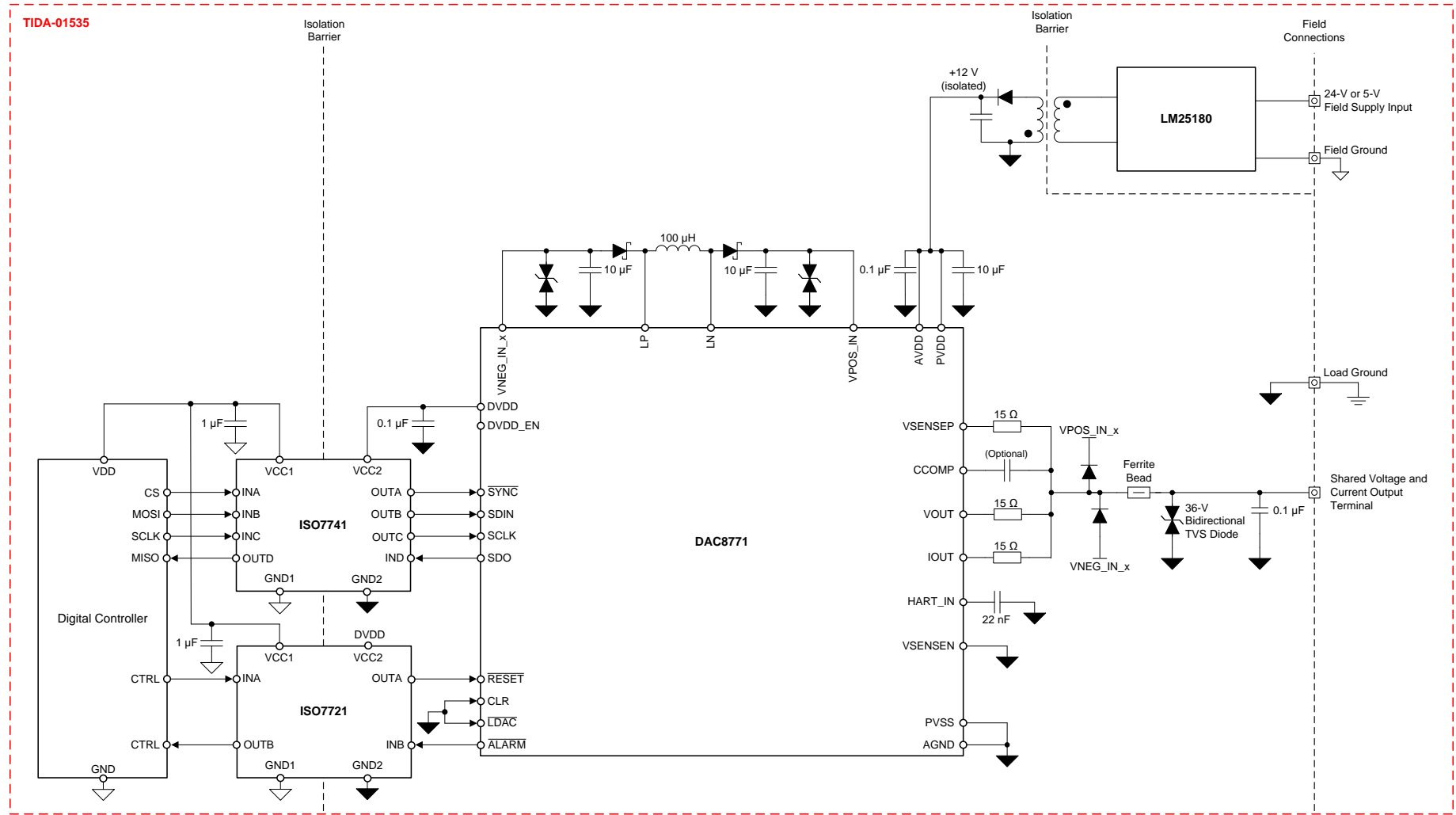


图 1. TIDA-01535 Block Diagram

## 2.2 Design Considerations

### 2.2.1 Specifications for Isolated Power Supply Design

A 12-V isolated supply voltage is selected to power the DAC8771. The device operates most efficiently at the low end of its input voltage range when it is boosting the voltage. 图 2 shows the efficiency of the integrated buck-boost converter for the DAC8771.

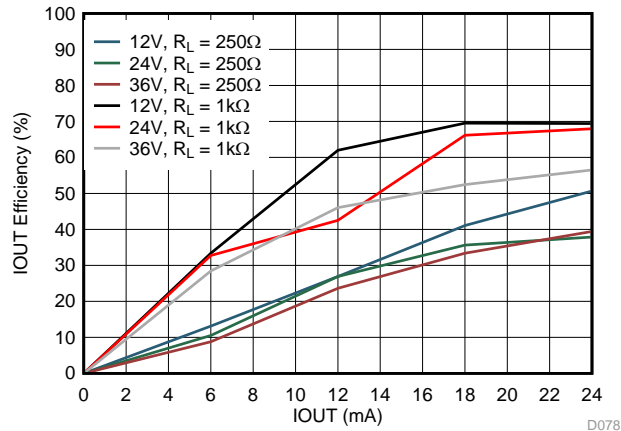


图 2. DAC8771 Internal Buck-Boost Converter Efficiency vs Load

The internal buck-boost converter of the DAC8771 uses the 12-V to 36-V supply to generate its own positive and negative voltages, as well as the required digital supply voltage. The inductor current of the internal buck-boost can have a peak of 0.5 A and operates in pulse frequency modulation (PFM) mode without a fixed frequency. In this design, 12-V is chosen to supply the DAC8771 because this voltage is the most efficient for the internal buck-boost converter to generate the required rails.

The average current requirement of the device depends on operating conditions; however, the average is less than 100 mA at 12 V. The target current for the isolated supply design is 150 mA to provide headroom. Both the output capacitance of the flyback converter and the onboard local bypass capacitors supply these peaks. 表 2 lists the power supply design specifications.

表 2. Isolated Power-Supply Design Parameters

PARAMETER	SPECIFICATIONS
Input voltage	12 V to 42 V
Output voltage (secondary)	12.5 V
Output current (secondary)	150 mA
Switching frequency	10-kHz to 350-kHz

### 2.2.2 Flyback Operation

A flyback converter is used to provide galvanic isolation between the input power supply and the onboard circuitry of this reference design. The flyback converter functions as a buck-boost converter with a coupled inductor or transformer to transfer power to the isolated side. During the on time,  $t_{ON}$ , the internal switch between SW and GND is closed. This closed switch allows current to flow through the primary side of the transformer, and thus stores energy in the magnetic field. The flyback diode D1 is reverse biased during  $t_{ON}$  blocking current flow in the secondary side. During the off time,  $t_{OFF}$ , energy stored in the magnetic field during  $T_{ON}$  charges the output capacitance on the secondary side. This process is illustrated in 图 3

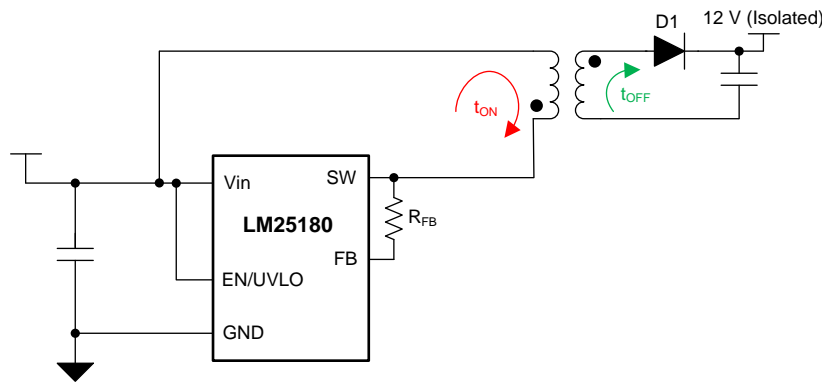


图 3. Flyback Operation

The LM25180 flyback converter uses feedback from the primary side to regulate the secondary-side output voltage, eliminating the need for an optocoupler to provide feedback through the isolation barrier. For efficiency across the load-current range, the LM25180 operates with varying frequency, changing operating modes in order to maximize efficiency at different load conditions.

### 2.2.3 LM25180 Simplified Design Procedure

The first design step is to select the flyback transformer turns ratio, and set the output voltage by selecting  $R_{FB}$ . The turns ratio ( $N_{PS}$ ) at maximum duty cycle and minimum input voltage is given by 公式 1. A turns ratio of 1 is selected based on commonly available coupled inductors. This ratio corresponds to a maximum duty cycle of 51%.

$$N_{PS} = \frac{D_{MAX}}{1 - D_{MAX}} \times \frac{V_{IN(min)}}{V_{OUT} + V_D} = \frac{0.6}{1 - 0.6} \times \frac{12 \text{ V}}{12.5 \text{ V} + 0.5 \text{ V}} = 1.38$$

where

- $D_{MAX}$  is the maximum duty cycle
  - $V_{IN(min)}$  is the minimum input voltage
  - $V_D$  is the forward voltage drop across the flyback diode
  - $V_{OUT}$  is the output voltage
- (1)

公式 2 calculates  $R_{FB}$  in order to set the output voltage.

$$R_{FB} = (V_{OUT} + V_D) \times N_{PS} \times \frac{R_{SET}}{V_{REF}} = (12.5 \text{ V} + 0.5 \text{ V}) \times 1 \times \frac{12.1 \text{ k}\Omega}{1.21 \text{ V}} = 130 \text{ k}\Omega$$

where

- $V_{OUT}$  is the isolated output voltage
  - $V_D$  is the forward voltage drop of the flyback diode
  - $N_{PS}$  is the turns ratio
  - $V_{REF}$  is the internal reference voltage
- (2)

The required minimum inductance is calculated by 公式 3. A 22- $\mu\text{H}$ , 1:1 coupled inductor is chosen with a saturation current of 1.73 A, well above the peak inductor current.

$$L_{MAG} \geq \frac{(V_{OUT} + V_D) \times N_{PS} \times t_{off,min}}{I_{PRI-PK(FFM)}} = \frac{(12 \text{ V} + 0.3 \text{ V}) \times 1 \times 500 \text{ ns}}{0.3 \text{ A}} = 21.6 \mu\text{H}$$

where

- $L_{MAG}$  is the magnetizing inductance
  - $t_{off,min}$  is the minimum off time
  - $I_{PRI-PK(FFM)}$  is the primary-side peak current
- (3)

Choose a flyback diode that can withstand the reverse voltage. 公式 4 shows the calculation for the reverse-diode voltage. A 100-V, 1-A diode is chosen for this design.

$$V_{D-REV} \geq \frac{V_{IN(max)}}{N_{PS}} + V_{OUT} = 42 \text{ V} + 12.5 \text{ V} = 54.5 \text{ V}$$
(4)

Use sufficient input and output capacitance to minimize voltage ripple. Specific calculations are available in the LM25180 data sheet. For this reference design, 20- $\mu\text{F}$  is used for the input capacitance and 44- $\mu\text{F}$  is used for the output capacitance in order to reduce the isolated supply ripple for the DAC8771.

For more information and design examples, see the [LM25180 data sheet](#) and [LM25180 PSR flyback quickstart design tool](#).

#### 2.2.4 DAC8771 External Circuitry

This reference design uses the DAC8771, with the recommended external discrete circuitry for the internal buck-boost converter operation, and protection from IEC61000-4 transients. The DAC8771 internal reference is used to minimize external components and solution size. Two digital isolators are used to isolate the SPI bus, ALARM pin, and hardware reset pin. On the isolated side, the digital isolators are powered from the DAC8771 internal DVDD LDO.

The design includes series resistors, clamp-to-rail diodes, a TVS diode, ferrite bead, and capacitor at the output of DAC8771 in order to provide protection from industrial transients. For more information on this protection circuit for the DAC8771, see [TIPD216, Quad-Channel Industrial Voltage and Current Output Driver Reference Design \(EMC/EMI Tested\)](#).

## 2.3 Highlighted Products

### 2.3.1 DAC8771

The DAC8771 device is chosen for this design because of the high level of integration and the internal buck-boost converter, which simplifies the design process. The DAC8771 includes the digital-to-analog converter (DAC), current and voltage amplifiers, regulated voltages, voltage reference, and all of the switches, transistors, and resistors required to create a configurable integrated solution for industrial voltage and current output drivers. The DAC8771 features a maximum 0.1% FSR TUE specification, which includes the offset error, gain error, and integral non-linearity (INL) baseline for the final system accuracy. This accuracy is maintained across the full  $-24\text{-mA}$  to  $+24\text{-mA}$  and  $\pm 12\text{-V}$  ranges across an ambient operating temperature of  $-40^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$ . The maximum differential non-linearity (DNL) specification of  $\pm 1$  least significant bit (LSB) provides fully-monotonic operation for both  $V_{\text{OUT}}$  and  $I_{\text{OUT}}$ .

The DAC8771 has an internal buck-boost converter which can accept a voltage input range of 12 V to 36 V. The device uses a single inductor multiple output (SIMO) configuration to generate the positive and negative voltages required for operation. In current outputs, the load can be used to vary the voltage across the output transistor to reduce the power dissipation. The recommended inductor value is  $100\ \mu\text{H}$   $\pm 20\%$  with a peak current rating of 500 mA or greater.

图 4 shows the DAC8771 functional block diagram.

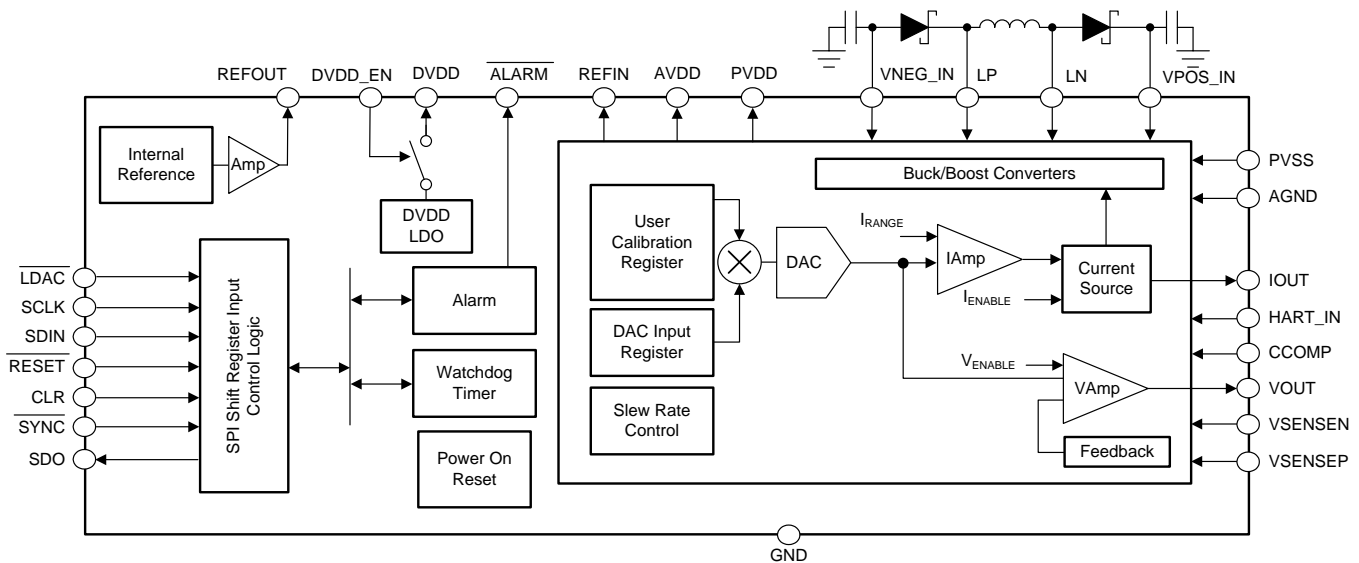


图 4. DAC8771 Functional Block Diagram



### 2.3.2 LM25180

The LM25180 is a primary-side regulated (PSR) flyback converter with high efficiency over a wide input voltage range of 4.5 V to 42 V. The isolated output voltage is sampled from the primary-side flyback voltage, eliminating the need for an optocoupler, voltage reference, or third winding from the transformer output for output voltage regulation. A 1:1 coupled inductor is chosen to minimize the board area and component height. Because of the high efficiency at low output current and design simplicity, the LM25180 is used for this reference design in order to provide an isolated supply for the DAC8771.

图 5 shows the LM25180 functional block diagram.

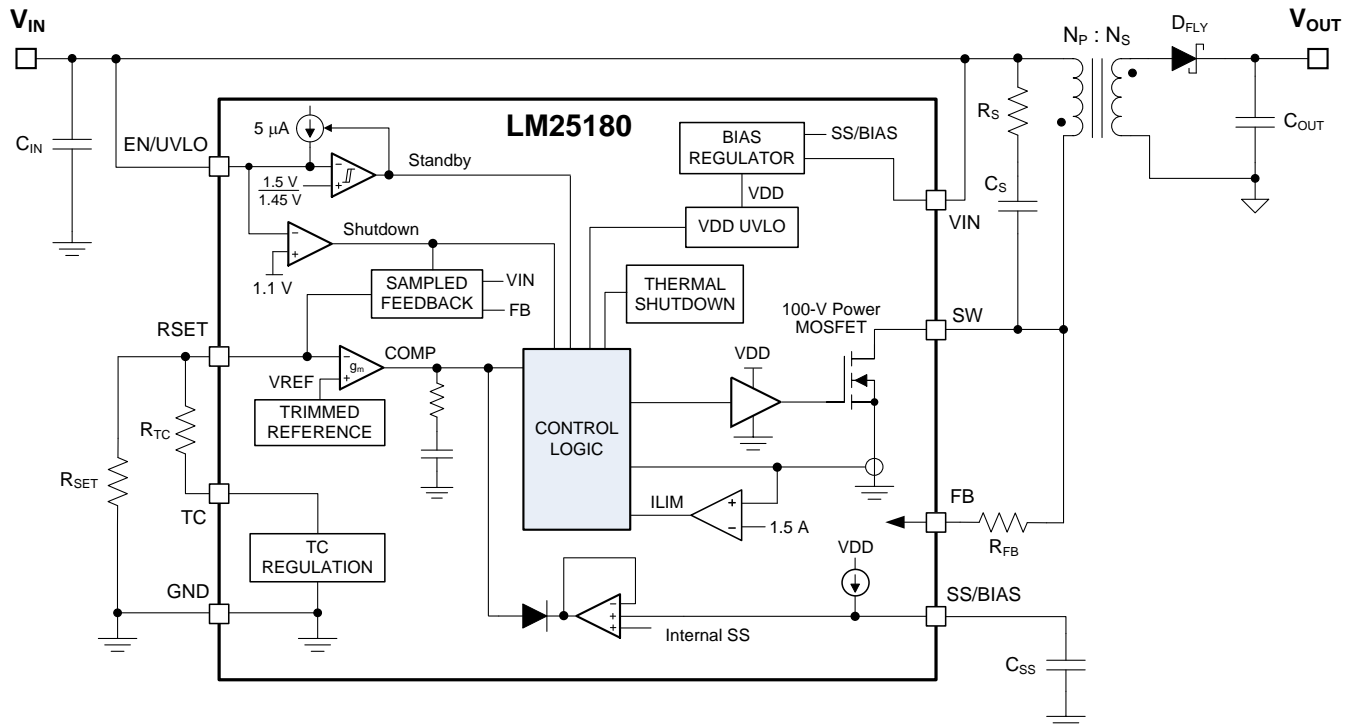
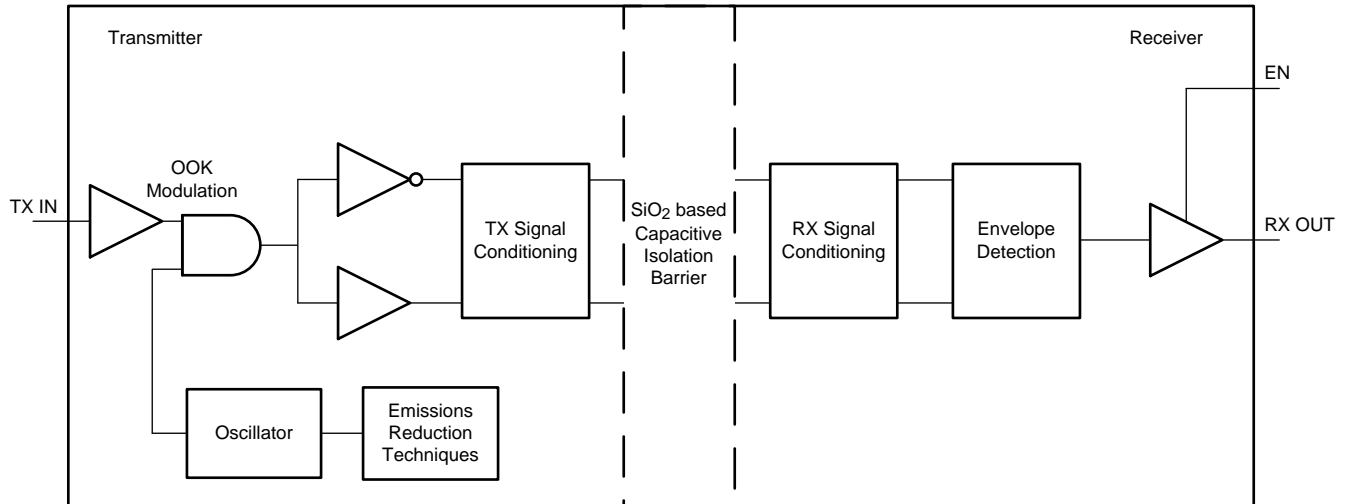


图 5. LM25180 Functional Block Diagram

### 2.3.3 ISO77x1

The ISO774x isolators provide multiple-channel digital isolation that prevents external circuitry interfering with the local ground. These devices feature 100-Mbps signaling, 2500- $V_{RMS}$  isolation, and low power consumption. In this design, the **ISO7741** device is used for SPI isolation and the **ISO7721** device is used to isolate the alarm and reset signals.

图 6 shows the ISO7741 functional block diagram.



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图 6. ISO7741 Functional Block Diagram

### 3 Hardware, Software, Testing Requirements, and Test Results

#### 3.1 Required Hardware and Software

##### 3.1.1 Hardware

For testing, this reference design was connected to a computer USB port through the SM-USB-DIG platform. This connection allows commands to be sent to the DAC from a computer. This process is the same as connecting the DAC8771 evaluation module. 图 7 shows an image of the test setup connections. For more details, see [DAC8771 Evaluation Module User's Guide](#).



图 7. SM-USB-DIG Connected to TIDA-01535

##### 3.1.2 Software

The software used for testing was the evaluation module (EVM) software. 图 8 shows a screenshot of the graphical user interface (GUI).

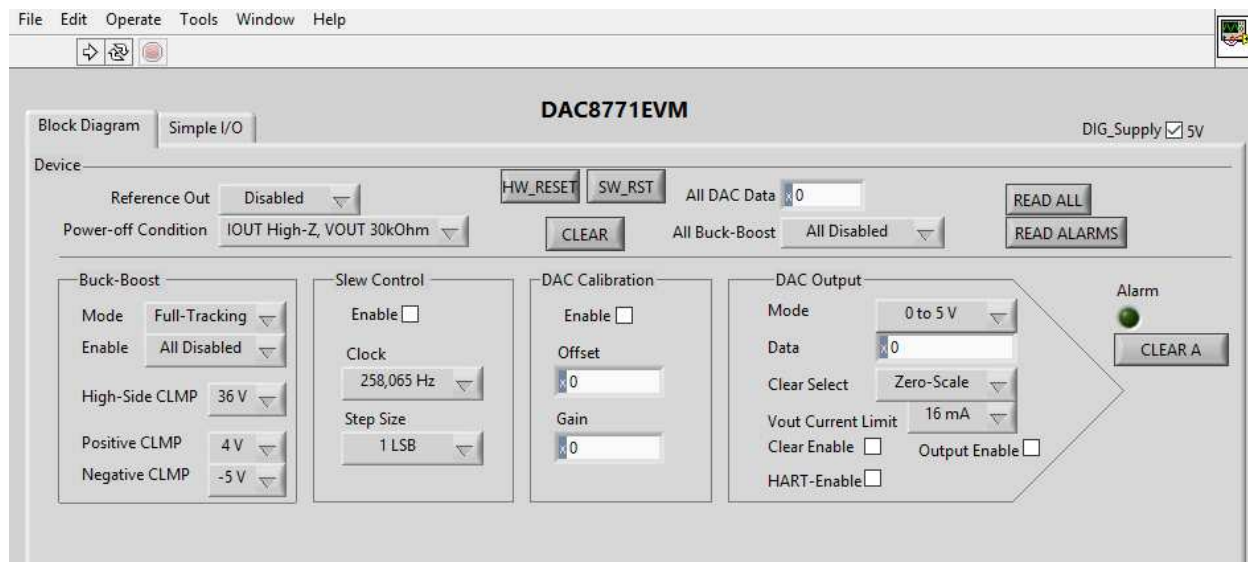
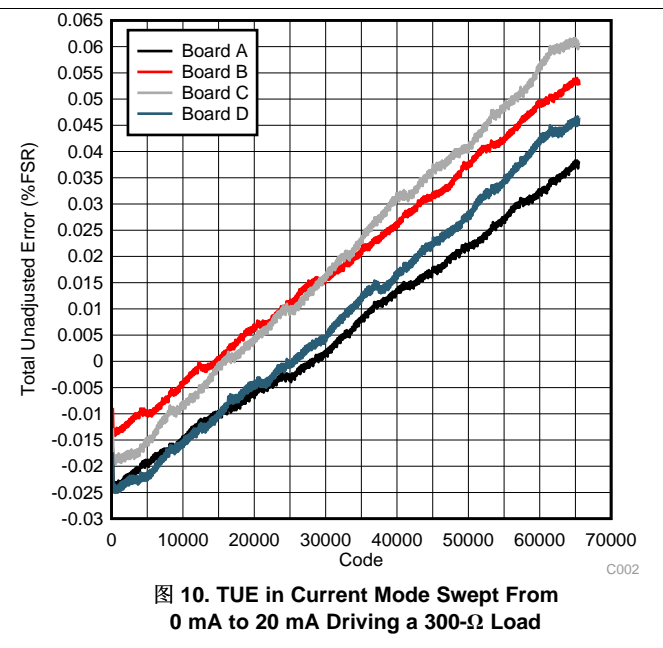
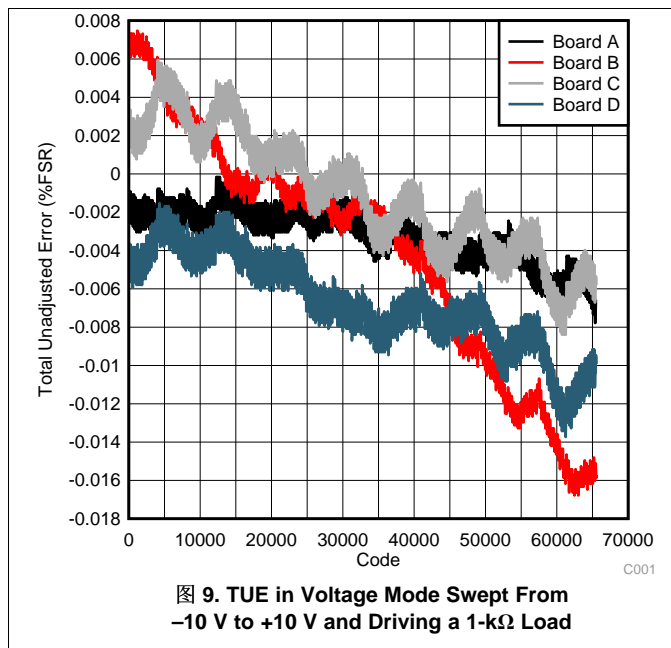


图 8. EVM Software GUI

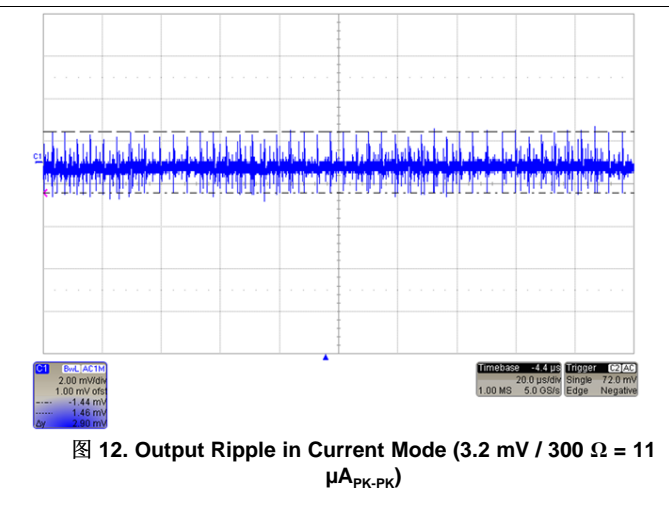
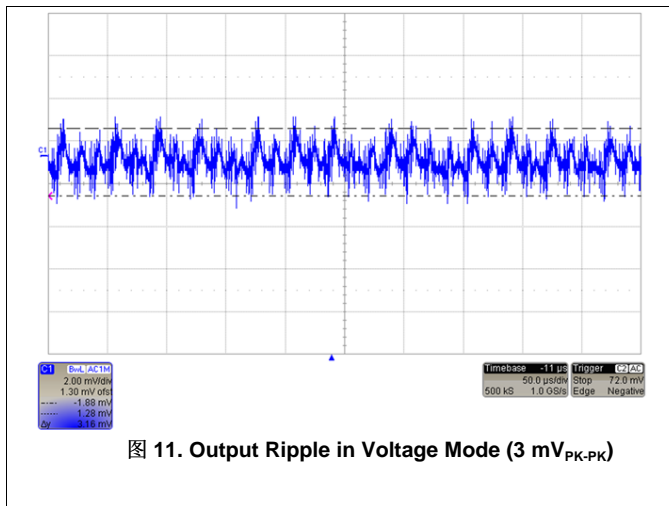
### 3.2 Testing and Results

#### 3.2.1 Test Results

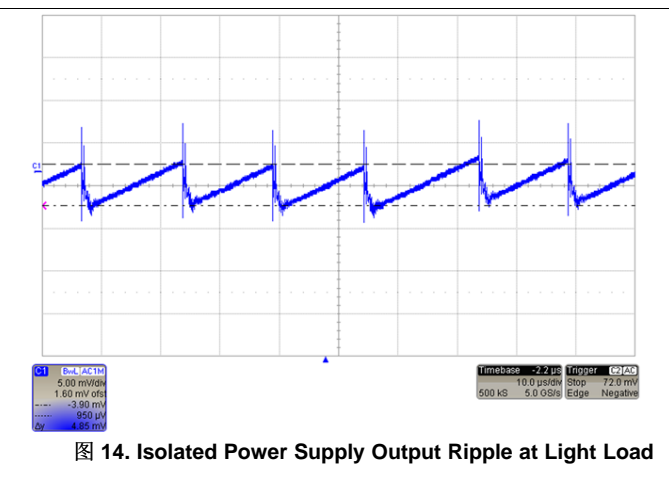
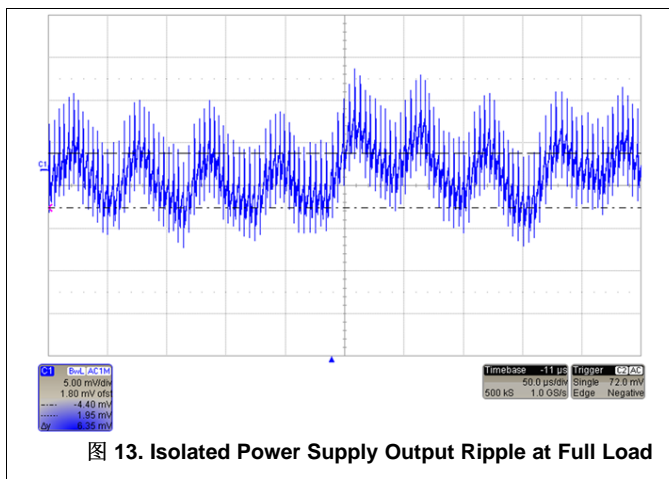
The total unadjusted error (TUE) was measured across the output range of the DAC8771 device. This measurement ensures that the DAC output is accurate across the code range. The TUE was measured in both current and voltage mode outputs across four boards. 图 9 shows the voltage mode TUE. For this measurement, the output was connected to a 1-k $\Omega$  load and swept from -10 V to +10 V. 图 10 shows the TUE measurement across the code range when the DAC8771 device is in current mode. In this measurement, the DAC output was connected to a 300- $\Omega$  load and swept from 0 mA to 20 mA. These TUE plots show that the design has much less than 0.1% TUE across all codes.



The DAC8771 output was also examined for noise that can originate from the isolated switching power supply. The output was directly connected to an oscilloscope through a coaxial cable to prevent environmental noise from coupling. A 200-MHz bandwidth limit was set on the oscilloscope to remove any high frequency. 图 11 shows the output ripple in voltage mode with the voltage set to 10 V to drive a 10-V load. The measured peak-to-peak voltage output ripple was approximately 3 mV. The current output ripple was also measured with the output set to 20 mA driving a 300-Ω load. The voltage was measured and then divided by the load resistance to determine the current ripple. The current ripple was  $3.2 \text{ mV} / 250 \text{ } \Omega = 11 \text{ } \mu\text{A}_{\text{PK-PK}}$ . 图 12 shows the current mode output ripple. These results show that noise on the output is low for both voltage and current modes.



The output ripple of the isolated power supply was also measured. This task was accomplished by measuring directly across the output capacitors of the isolated supplies. This measurement was taken at a full load (24 mA, 1 kΩ) and also at a light load with the output of the DAC8771 disabled. 图 13 and 图 14 show these measurements, respectively. The output ripple increases at a full load. This ripple is not observable at the output of the DAC8771 device.



The onboard power dissipation was measured for three different resistive loads at different current outputs, as 图 15 shows. The power dissipation includes powering the two onboard digital isolators that are responsible for much of the power dissipation at 0-mA load.

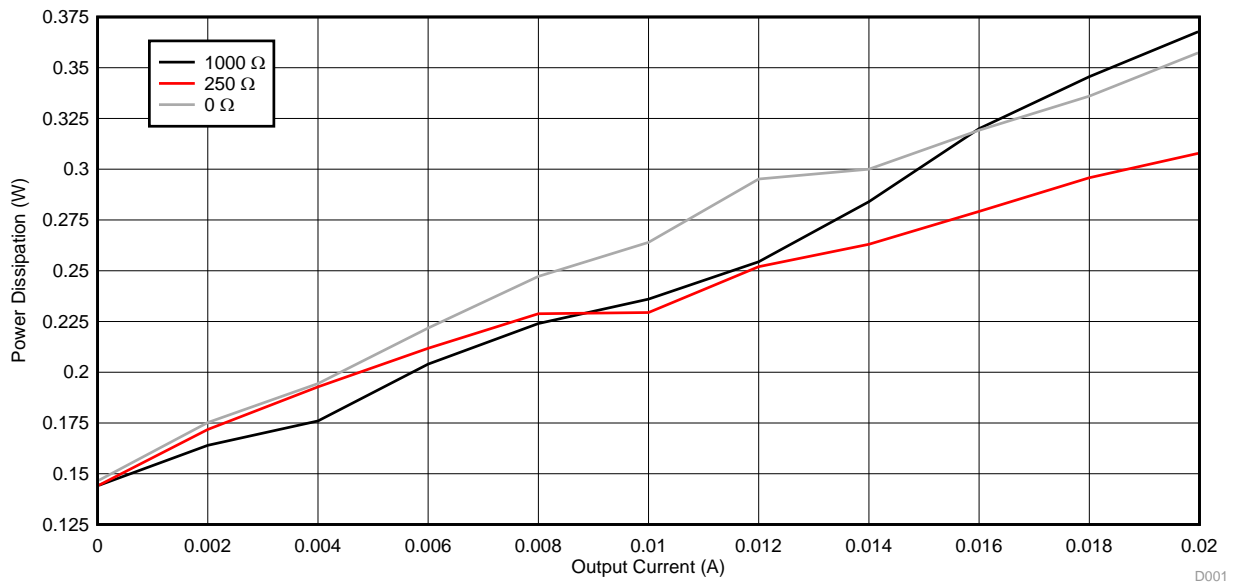


图 15. Onboard Power Dissipation vs Output Current

图 16 shows the power dissipation at the three load conditions without the digital isolators. This power dissipation only includes the DAC8771 and LM25180 circuitry, because not all applications require digital isolation. To make these measurements, the isolators were removed from the board, and the digital communication was interfaced directly with the DAC8771. This plot shows a significant reduction in power dissipation without digital isolation.

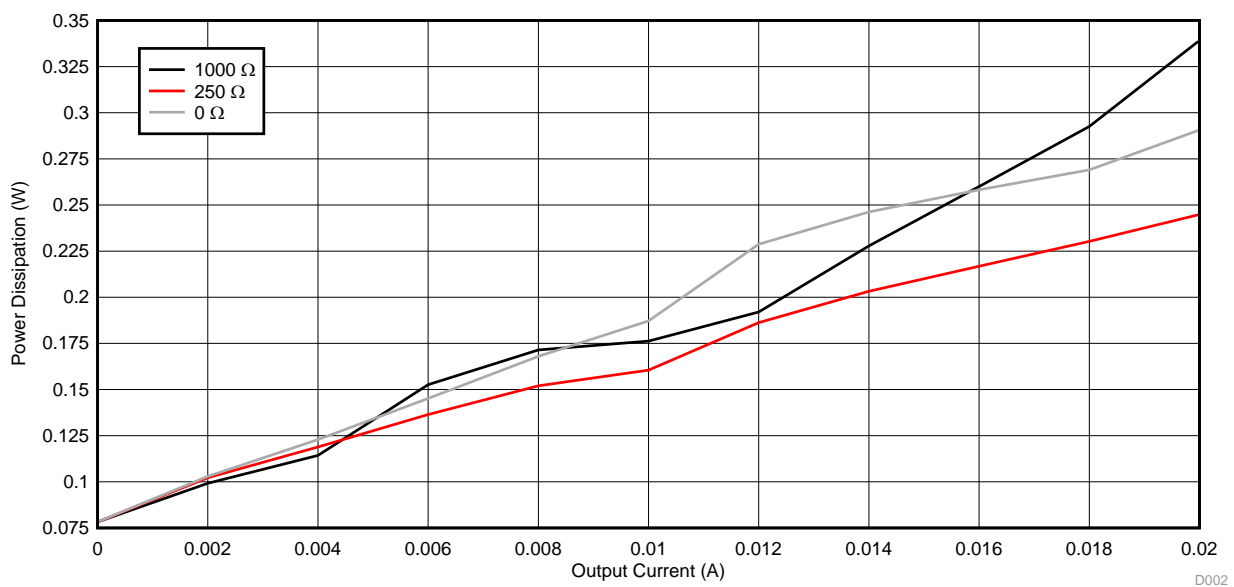


图 16. Onboard Power Dissipation vs Output Current (without digital isolators)

The efficiency of the isolated supply was measured across the designed load range of 0 mA to 150 mA. 图 17 shows the plotted efficiency results for the isolated supply. These efficiency results only include the LM25180 isolated supply design.

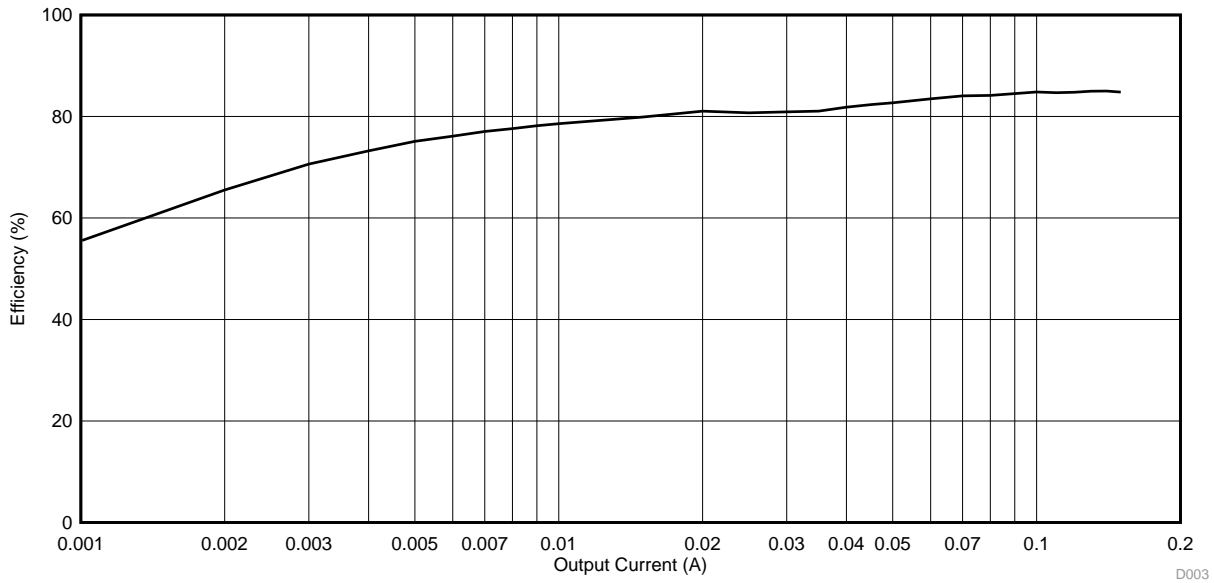


图 17. LM25180 Isolated Supply Efficiency vs Output Current

图 18 shows a thermal image of the board providing 24 mA into a 1-kΩ load.

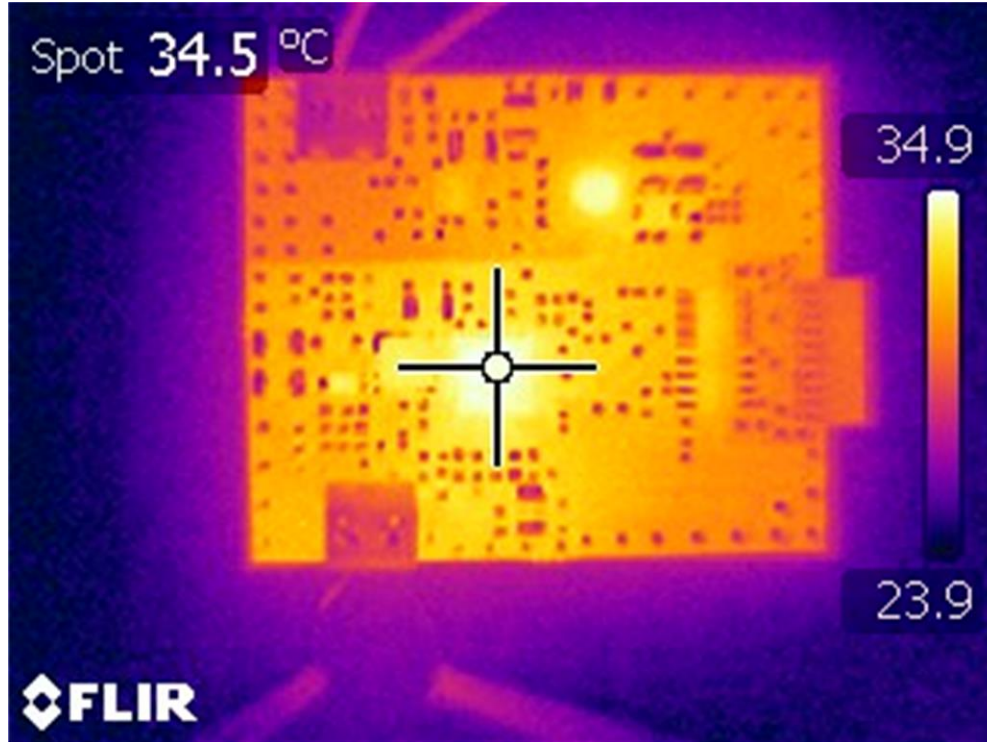


图 18. Board Thermal Image: 24 mA into a 1-kΩ Load



## 4 Design Files

### 4.1 Schematics

To download the schematics, see the design files at [TIDA-01535](#).

### 4.2 Bill of Materials

To download the bill of materials (BOM), see the design files at [TIDA-01535](#).

### 4.3 PCB Layout Recommendations

TI recommends to follow standard printed-circuit board (PCB) layout guidelines such as proper decoupling and ground connections with large copper pours. The EMI and EMC protection circuit elements must be placed as close to the output connectors as possible. Use wide traces along the path of the output signal to provide a low impedance path for the analog signals. Via stitching must be used to tie the ground planes together. When possible, use copper pours instead of traces. The inductor for the integrated power supply of the DAC8771 must be placed as close to the device as possible and wide traces must be used to minimize parasitics.

Note that the isolated power supply circuitry requires a few additional guidelines. Placement of the input bypass capacitor for the LM25180 must be as close as possible to the device pin, which is critical. This capacitor provides switching current and must have a direct path to minimize impedance. Minimizing high di/dt loops in a switch-mode power supply design is also important. The input loop from  $V_{IN}$  to GND through the bypass capacitor must be minimized. The loop from the switch node through the inductor and output capacitors must also be made as short as possible. Be sure to remove the copper layers (GND, PWR) between the input isolated ground planes for isolation. If possible, remove the thermal reliefs on the power components to further reduce impedance in the power path

#### 4.3.1 Layout Prints

To download the layer plots, see the design files at [TIDA-01535](#).

### 4.4 Altium Project

To download the Altium project files, see the design files at [TIDA-01535](#).

### 4.5 Gerber Files

To download the Gerber files, see the design files at [TIDA-01535](#).

### 4.6 Assembly Drawings

To download the assembly drawings, see the design files at [TIDA-01535](#).

## 5 Software Files

To download the software files, see the design files at [TIDA-01535](#).

## 6 Related Documentation

1. Texas Instruments, [LM5180 EVM user's guide](#)
2. Texas Instruments, [DAC8771 evaluation module user's guide](#)
3. Texas Instruments, [Quad-channel industrial voltage and current output driver reference design](#)

(EMC/EMI tested)

4. Texas Instruments, *Less than 1-W, quad-channel, analog output module with adaptive power management reference design*

## 6.1 商标

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## 7 Terminology

**BOM**— Bill of materials

**CCM**— Continuous conduction mode

**COT**— Constant on time

**DAC**— Digital-to-analog converter

**DCIO**— Discrete input/output module

**DNL**— Differential nonlinearity

**EMC**— Electromagnetic compatibility

**EMI**— Electromagnetic interference

**EVM**— Evaluation module

**FET**— Field-effect transistor

**FSR**— Full-scale range

**GUI**— Graphical user interface

**LSB**— Least significant bit

**PFM**— Pulse frequency modulation

**RMS**— Root mean square

**SIMO**— Single inductor multiple output

**SPI**— Serial peripheral interface

**TUE**— Total unadjusted error

**UVLO**— Undervoltage lockout

## 8 About the Author

**GARRETT SATTERFIELD** is an applications engineer in the Precision Digital-to-Analog Converters group at Texas Instruments, where he supports industrial products. Garrett received his BSEE from The Georgia Institute of Technology in 2016.

## 修订历史记录

**Changes from Original (March 2018) to A Revision** **Page**

- 
- 已更改 将设计指南更改成了使用新的 LM25180 器件和相关内容 ..... 1
-

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