

DRV8849 : 38V、1.5A デュアル・ステッピング・ドライバ、電流センス機能内蔵、1/256 マイクロステッピング、STEP/DIR インターフェイスおよびスマート・チューン

1 特長

- デュアル・ステッピング・モーター・ドライバ
 - STEP/DIR インターフェイス
 - 最高 1/256 のマイクロステッピング・インデクサ
- 動作電源電圧範囲: 4.5~38V
- 24V、25°Cで 900mΩ HS + LS $R_{DS(ON)}$
- Hブリッジあたり、フルスケールで 1.5A、実効値で 1.1A の電流
- 電流検出機能内蔵
 - 検出抵抗が不要
 - ±5% のフルスケール電流精度
- スマート・チューン・ディケイ・テクノロジー
- スマート・チューンでオフタイムの PWM チョッピングを構成可能
 - 8μs、16μs、32μs
- 1.8V、3.3V、5.0V のロジック入力をサポート
- 低消費電流のスリープ・モード (1.3μA)
- 各ステップの保護機能
 - VM 低電圧誤動作防止 (UVLO)
 - チャージ・ポンプ低電圧検出 (CPUV)
 - 過電流保護 (OCP)
 - サーマル・シャットダウン (OTSD)
 - フォルト条件出力 (nFAULT)

2 アプリケーション

- IP ネットワーク・カメラ
- プリンタとスキャナ
- ATM と貨幣処理機
- ミシン
- 医療用画像処理、診断、および機器
- 3D プリンタ

3 概要

DRV8849 は、産業用および民生用アプリケーション向けのデュアル・ステッピング・モーター・ドライバです。このデバイスには、4 つの N チャネル・パワー MOSFET Hブリッジ・ドライバ、各ステップに 1 つのマイクロステッピング・インデクサ、および電流検出機能が完全に統合されています。DRV8849 は最大 1.5A フルスケール出力電流を駆動できます (PCB の設計に依存)。

DRV8849 は、4 つの外部電力検出抵抗が不要な内部電流検出アーキテクチャを採用しているため、PCB 面積とシステム・コストを低減できます。本デバイスは、スマート・チューン・ディケイ・モードを使った内部 PWM 電流レギュレーション方式を採用しています。スマート・チューンは、必要な電流レギュレーションを自動的に調整し、モーターの変動と経年変化を補償し、モーターからの可聴ノイズと振動を低減します。

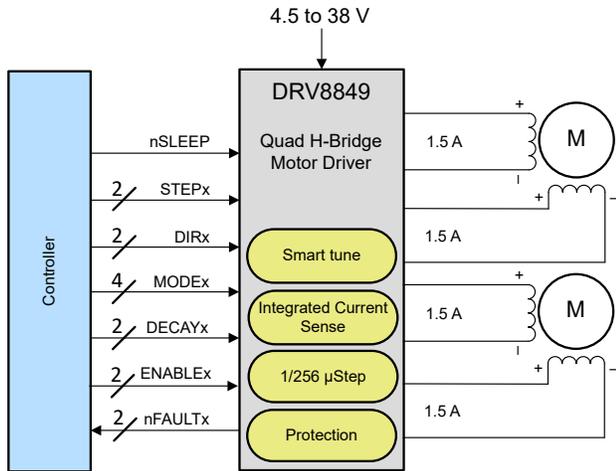
シンプルな STEP/DIR インターフェイスにより、外部コントローラからステッピング・モーターの方向とステップ速度を制御できます。デバイスは、フルステップから 1/256 マイクロステッピングまでのモードに構成可能です。専用の nSLEEP ピンを使用して、低消費電力のスリープ・モードを実現します。電源の低電圧、チャージ・ポンプ障害、過電流、短絡、過熱に対する保護機能が備わっています。フォルト状態は、各ステップに対して 1 つの nFAULT ピンで示されます。

製品情報

部品番号	パッケージ ⁽¹⁾	本体サイズ (公称)
DRV8849RHHR	QFN (36)	6mm × 6mm

(1) 巻末の注文情報を参照してください。





簡略回路図

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4 Revision History

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

DATE	REVISION	NOTES
April 2023	*	Initial Release

5 Device Comparison

表 5-1. Device Comparison Table

Device Name	Drives DC motor	Drives Stepper	Interface	Microstep	Current sensing
DRV8849	No	Yes	STEP/DIR	Up to 1/256	Internal sensing
DRV8845	Yes	Yes	PHASE/Ixx	Up to 1/4, higher microstepping by VREF pin	Sense Resistor

6 Pin Configuration and Functions

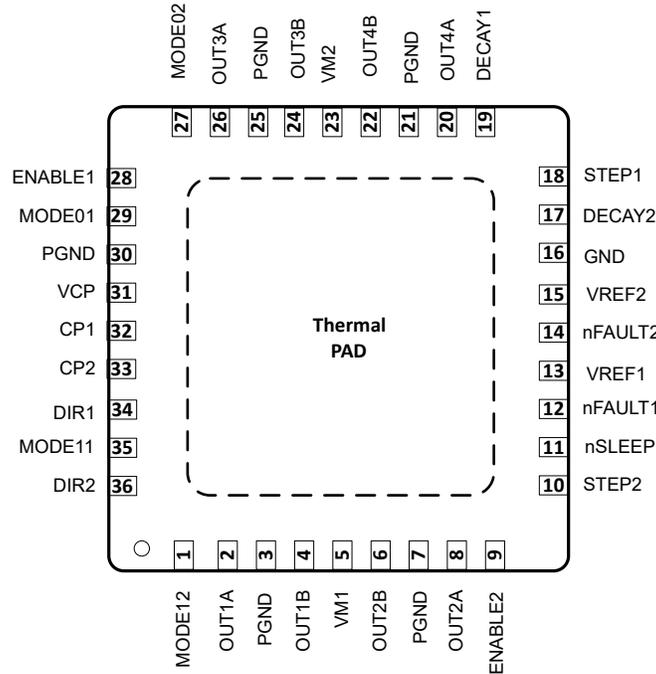


图 6-1. RHH Package, 36-Pin QFN, Top View

表 6-1. Pin Functions

PIN		I/O ⁽¹⁾	DESCRIPTION
NAME	NO.		
OUT1A	2	O	H-Bridge 1 Output A
OUT1B	4	O	H-Bridge 1 Output B
OUT2A	8	O	H-Bridge 2 Output A
OUT2B	6	O	H-Bridge 2 Output B
OUT3A	26	O	H-Bridge 3 Output A
OUT3B	24	O	H-Bridge 3 Output B
OUT4A	20	O	H-Bridge 4 Output A
OUT4B	22	O	H-Bridge 4 Output B
PGND1	3	G	Power ground pin for H-Bridge 1. Connect all ground pins together near the IC.
PGND2	7	G	Power ground pin for H-Bridge 2. Connect all ground pins together near the IC.
PGND3	25	G	Power ground pin for H-Bridge 3. Connect all ground pins together near the IC.
PGND4	21	G	Power ground pin for H-Bridge 4. Connect all ground pins together near the IC.
GND	16, 30	G	Analog ground. Connect all ground pins together near the IC.
VM1	5	P	Supply Voltage. VM1 should be connected to VM2 pin close to the device.
VM2	23	P	Supply Voltage. VM2 should be connected to VM1 pin close to the device.
VCP	31	P	Reservoir Capacitor Terminal
CP1	32	P	Charge Pump Capacitor Terminal
CP2	33	P	Charge Pump Capacitor Terminal

表 6-1. Pin Functions (continued)

PIN		I/O ⁽¹⁾	DESCRIPTION
NAME	NO.		
DECAY1	19	I	Decay mode setting pin for Stepper 1
DECAY2	17	I	Decay mode setting pin for Stepper 2
STEP1	18	I	Step input signal for Stepper 1
STEP2	10	I	Step input signal for Stepper 2
DIR1	34	I	Direction input signal for Stepper 1
DIR2	36	I	Direction input signal for Stepper 2
nSLEEP	11	I	Sleep mode input. Logic high to enable device; logic low to enter low-power sleep mode. An nSLEEP low pulse clears latched faults.
VREF1	13	I	Reference voltage input to set the full scale chopping current for Stepper 1
VREF2	15	I	Reference voltage input to set the full scale chopping current for Stepper 2
ENABLE1	28	I	Enable input for Stepper 1. Logic low on this input disables (Hi-Z) the outputs of Stepper 1.
ENABLE2	9	I	Enable input for Stepper 2. Logic low on this input disables (Hi-Z) the outputs of Stepper 2.
MODE01	29	I	Microstep setting inputs for Stepper 1
MODE11	35	I	
MODE02	27	I	Microstep setting inputs for Stepper 2
MODE12	1	I	
nFAULT1	12	O	Fault diagnostics output for Stepper 1
nFAULT2	14	O	Fault diagnostics output for Stepper 2
PAD	-	-	Exposed pad for enhanced thermal performance. Should be soldered to the PCB.

(1) I = Input, O = Output, I/O = Input or Output, G = Ground, P = Power.

7 Specifications

7.1 Absolute Maximum Ratings

over operating free-air temperature range referenced with respect to GND (unless otherwise noted) ⁽¹⁾

	MIN	MAX	UNIT
Power supply voltage (VMx)	-0.3	40	V
Charge pump voltage (VCP, CP1)	-0.3	V _{VM} + 7	V
Charge pump negative switching pin (CP2)	-0.3	V _{VM}	V
Sleep mode input voltage (nSLEEP)	-0.3	5.75	V
Control input voltage	-0.3	5.75	V
PGND pin voltage	-0.5	0.5	V
PGND pin voltages for < 1 μs	-2.5	2.5	V
Reference input pin voltage (VREFx)	-0.3	5.75	V
Open drain output current (nFAULTx)	0	10	mA
Continuous phase node pin voltage (OUTxA, OUTxB)	-1	V _{VM} + 1	V
Transient 100 ns phase node pin voltage (OUTxA, OUTxB)	-3	V _{VM} + 3	V
Output current	0	1.5	A
Operating ambient temperature, T _A	-40	125	°C
Operating junction temperature, T _J	-40	150	°C
Storage temperature, T _{stg}	-65	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

7.2 ESD Ratings

			VALUE	UNIT
V _(ESD)	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2000	V
		Charged-device model (CDM), per ANSI/ESDA/JEDEC JS-002 ⁽¹⁾	±500	

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process. JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT
V _{VM}	Supply voltage range for normal (DC) operation	4.5	38	V
V _I	Control input voltage	0	5.5	V
V _{REFx}	Reference voltage (VREFx)	0	3.3	V
f _{STEP}	Applied STEP signal ⁽¹⁾	0	500	kHz
I _{RMS}	Motor RMS current (xOUTx) ⁽²⁾	0	1.1	A
T _A	Operating ambient temperature	-40	125	°C
T _J	Operating junction temperature	-40	150	°C

- (1) STEP input can operate up to 500 kHz, but system bandwidth is limited by the motor load
 (2) Power dissipation and thermal limits must be observed

7.4 Thermal Information

THERMAL METRIC		QFN	UNIT
$R_{\theta JA}$	Junction-to-ambient thermal resistance	29.9	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	19.5	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	11.6	°C/W
Ψ_{JT}	Junction-to-top characterization parameter	0.3	°C/W
Ψ_{JB}	Junction-to-board characterization parameter	11.6	°C/W
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	4.1	°C/W

7.5 Electrical Characteristics

Typical values are at $T_A = 25^\circ\text{C}$ and $V_{VM} = 24\text{ V}$. All limits are over recommended operating conditions, unless otherwise noted.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
POWER SUPPLIES (VM)						
I_{VM}	VM operating supply current	ENABLE = 1, nSLEEP = 1, No motor load		6	8	mA
		nSLEEP = 1, Outputs off		5.5	7	mA
		nSLEEP = 0		1.3	3	μA
t_{SLEEP}	Sleep time	nSLEEP = 0 to sleep mode	120			μs
t_{RESET}	nSLEEP reset pulse	nSLEEP low to clear fault	20		40	μs
t_{ON}	Turn-on time	VM > UVLO to output transition		0.62	0.8	ms
t_{WAKE}	Wake-up time	nSLEEP = 1 to output transition		0.62	0.8	ms
t_{EN}	Enable time	ENABLE = 0/1 to output transition			1	μs
CHARGE PUMP (VCP, CP1, CP2)						
V_{VCP}	VCP operating voltage	$6\text{ V} < V_{VM} < 38\text{ V}$		$V_{VM} + 5$		V
$f_{(VCP)}$	Charge pump switching frequency	$V_{VM} > UVLO$, nSLEEP = 1		380		kHz
LOGIC-LEVEL INPUTS (STEP, DIR, nSLEEP)						
V_{IL}	Input logic-low voltage		0		0.8	V
V_{IH}	Input logic-high voltage		2		5.5	V
V_{HYS}	Input logic hysteresis		150	300	500	mV
I_{INL}	Logic input low current	$V_{IN} = 0\text{ V}$	-1		1	μA
I_{INH}	Logic input high current	$V_{IN} = 5\text{ V}$			30	μA
TRI-LEVEL INPUTS (MODE0x, ENABLE)						
V_{I1}	Input logic-low voltage	Tied to GND	0		0.6	V
V_{I2}	Input Hi-Z voltage	Hi-Z	1.8	2	2.2	V
V_{I3}	Input logic-high voltage	Tied to 5 V	2.7		5.5	V
I_O	Input pull-up current			10		μA
QUAD-LEVEL INPUTS (MODE1x, DECAYx)						
V_{I1}	Input logic-low voltage	Tied to GND	0		0.6	V
V_{I2}		$330\text{k}\Omega \pm 5\%$ to GND	1	1.25	1.4	V

Typical values are at $T_A = 25^\circ\text{C}$ and $V_{VM} = 24\text{ V}$. All limits are over recommended operating conditions, unless otherwise noted.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
V_{I3}	Input Hi-Z voltage	Hi-Z	1.8	2	2.2	V
V_{I4}	Input logic-high voltage	Tied to 5 V	2.7		5.5	V
I_O	Input pull-up current			10		μA
CONTROL OUTPUTS (nFAULTx)						
V_{OL}	Output logic-low voltage	$I_O = 5\text{ mA}$			0.2	V
I_{OH}	Output logic-high leakage	$V_{Mx} = 24\text{ V}$	-1		1	μA
MOTOR DRIVER OUTPUTS						
$R_{DS(ONH)}$	High-side FET on resistance	$T_J = 25^\circ\text{C}, I_O = -1.2\text{ A}$		450	550	$\text{m}\Omega$
		$T_J = 125^\circ\text{C}, I_O = -1.2\text{ A}$		700	850	$\text{m}\Omega$
		$T_J = 150^\circ\text{C}, I_O = -1.2\text{ A}$		780	950	$\text{m}\Omega$
$R_{DS(ONL)}$	Low-side FET on resistance	$T_J = 25^\circ\text{C}, I_O = 1.2\text{ A}$		450	550	$\text{m}\Omega$
		$T_J = 125^\circ\text{C}, I_O = 1.2\text{ A}$		700	850	$\text{m}\Omega$
		$T_J = 150^\circ\text{C}, I_O = 1.2\text{ A}$		780	950	$\text{m}\Omega$
$V_{F, \text{Outputs}}$		$I_O = \pm 1.2\text{ A}$			1.2	V
I_{DSS}	Output Leakage	Outputs, $V_{OUT} = 0$ to V_M	-2		7	μA
t_{SR}	Output rise/fall time	$V_M = 24\text{V}, I_O = 1.2\text{ A}$, Between 10% and 90%		100		ns
t_D	Dead time			425		ns
t_{BLANK}	Current sense blanking time ⁽¹⁾			1		μs
PWM CURRENT CONTROL (VREFx)						
K_V	Transimpedance gain	$V_{REF} = 3.3\text{ V}$	2.09	2.2	2.31	V/A
I_{VREFx}	VREFx pin reference input Current		-1		1	μA
t_{OFF}	PWM off-time	DECAYx = 1		16		μs
		DECAYx = Hi-Z		32		
		DECAYx = 330 k Ω to GND		8		
$I_{O,CH}$	AOUT and BOUT current matching	$I_O = 1.5\text{ A}$	-2.5		2.5	%
ΔI_{TRIP}	Current trip accuracy	$I_O = 1.5\text{ A}$, 68% to 100% current setting	-5		5	%
		$I_O = 1.5\text{ A}$, 20% to 67% current setting	-10		10	
		$I_O = 1.5\text{ A}$, 10% to 20% current setting	-15		15	
PROTECTION CIRCUITS						
V_{MUVLO}	VM UVLO threshold	VM falling	4.1	4.25	4.35	V
		VM rising	4.2	4.34	4.45	
$V_{MUVLO,HYS}$	VM UVLO hysteresis	Rising to falling threshold		90		mV
V_{CPIV}	Charge pump undervoltage	VCP falling		$V_{VM} + 2$		V
I_{OCP}	Overcurrent protection	Current through any FET	2.5			A

Typical values are at $T_A = 25^\circ\text{C}$ and $V_{VM} = 24\text{ V}$. All limits are over recommended operating conditions, unless otherwise noted.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
t_{OCP}	Overcurrent deglitch time			2.1		μs
t_{RETRY}	Overcurrent retry time			4		ms
T_{OTSD}	Thermal shutdown	Die temperature T_J	155	165	175	$^\circ\text{C}$
$T_{\text{HYS_OTSD}}$	Thermal shutdown hysteresis	Die temperature T_J		20		$^\circ\text{C}$ Guaranteed by design.

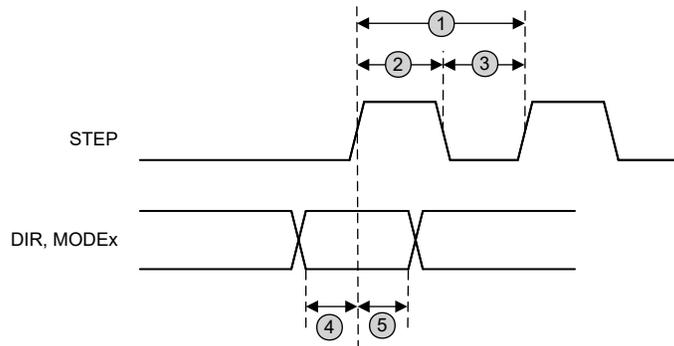
(1) Guaranteed by design.

7.6 Indexer Timing Requirements

Typical limits are at $T_J = 25^\circ\text{C}$ and $V_{VM} = 24\text{ V}$. Over recommended operating conditions unless otherwise noted.

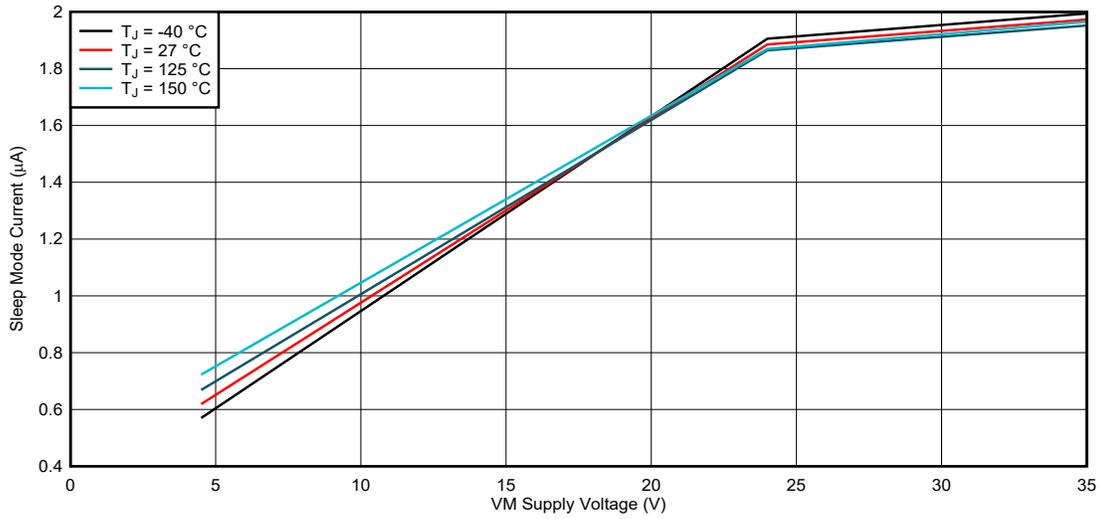
NO.			MIN	MAX	UNIT
1	f_{STEP}	Step frequency		500 ⁽¹⁾	kHz
2	$t_{\text{WH(STEP)}}$	Pulse duration, STEP high	970		ns
3	$t_{\text{WL(STEP)}}$	Pulse duration, STEP low	970		ns
4	$t_{\text{SU(DIR, Mx)}}$	Setup time, DIR or MODEx to STEP rising	200		ns
5	$t_{\text{H(DIR, Mx)}}$	Hold time, STEP rising to DIR or MODEx change	200		ns

(1) STEP input can operate up to 500 kHz, but system bandwidth is limited by the motor load.

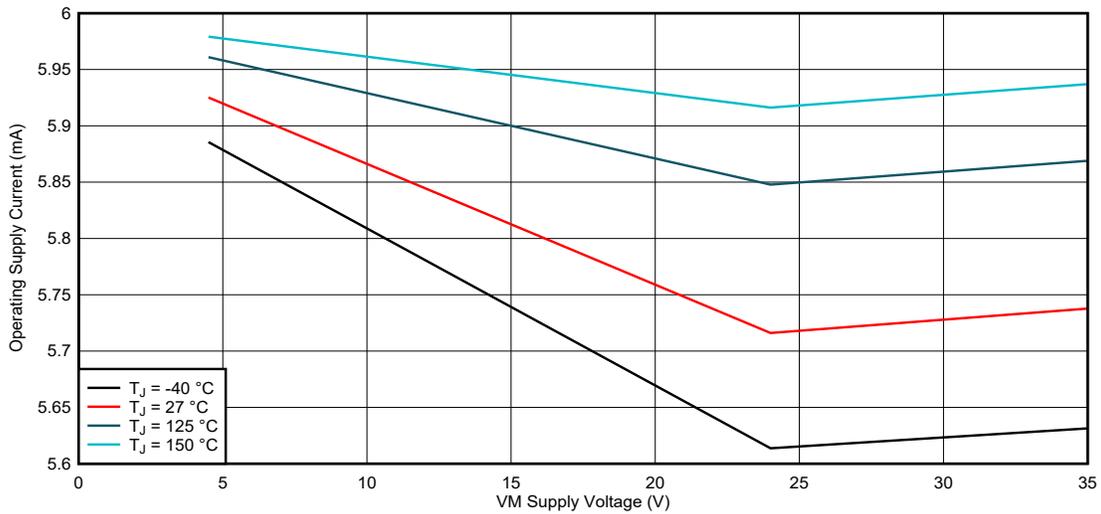


 7-1. STEP and DIR Timing Diagram

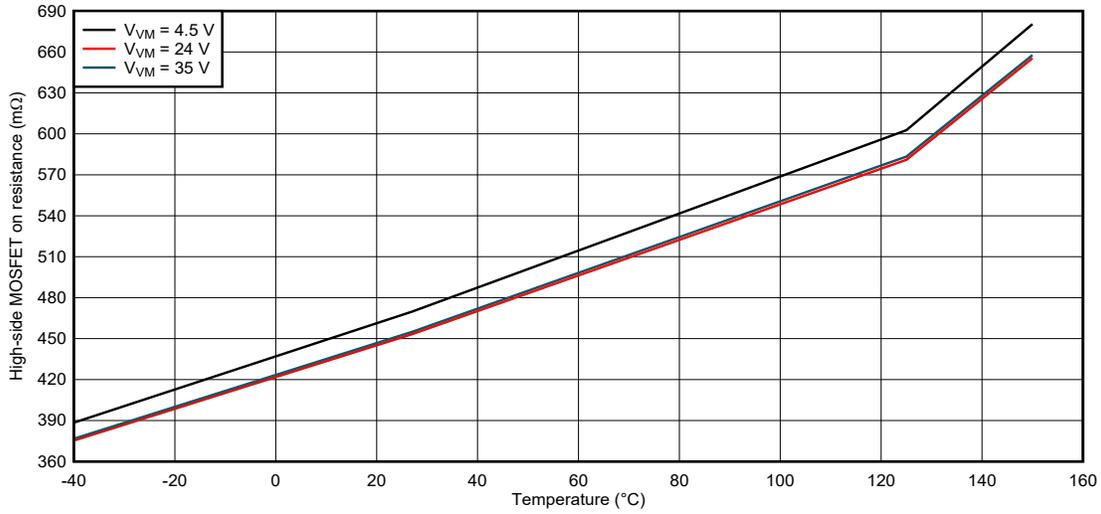
7.7 Typical Operating Characteristics



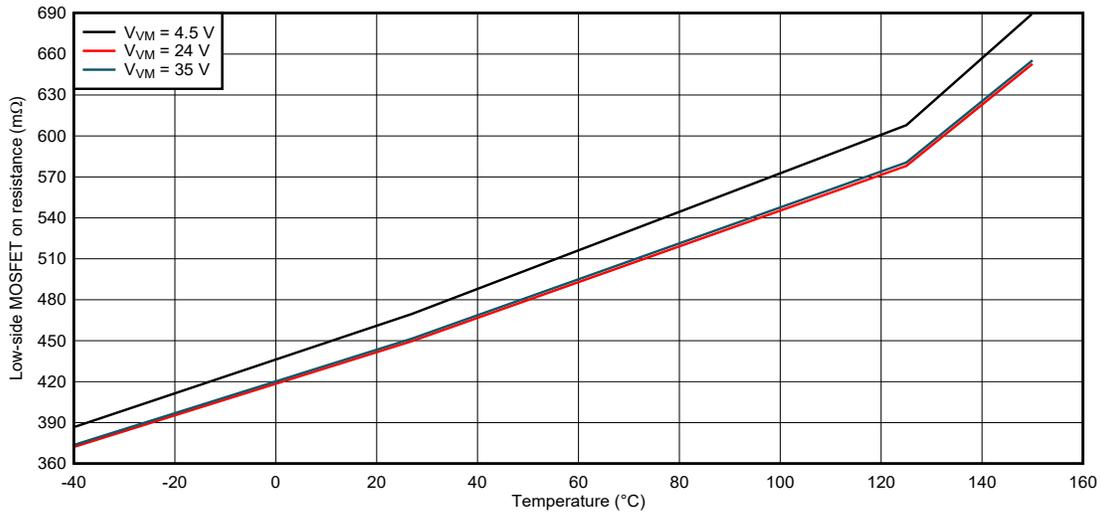
7-2. Sleep Mode Supply Current



7-3. Operating Supply Current with Outputs OFF



7-4. High-side FET on resistance



7-5. Low-side FET on resistance

8 Detailed Description

8.1 Overview

The DRV8849 is an integrated motor-driver solution for driving two bipolar stepper motors. The device provides the maximum integration by integrating four N-channel power MOSFET H-bridges, current sense resistors and regulation circuitry, and one microstepping indexer for each stepper. The DRV8849 is capable of supporting wide supply voltage of 4.5 to 38 V. The device provides an output current up to 2.5-A peak, 1.5-A full-scale, or 1.1-A root mean square (rms) on each output. The actual full-scale and rms current depends on the ambient temperature, supply voltage, and PCB thermal capability.

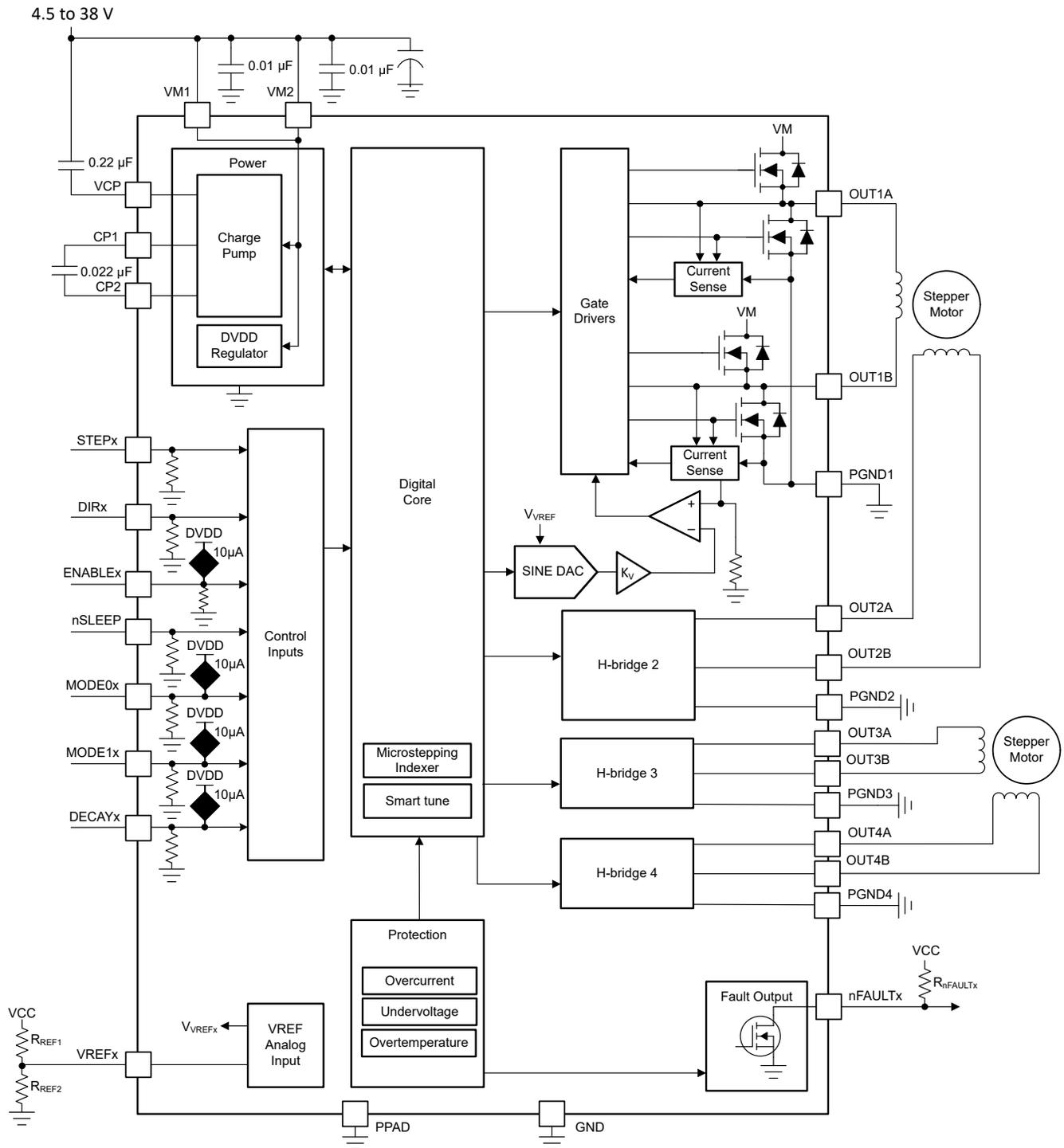
The DRV8849 uses an integrated current-sense architecture which eliminates the need for four external power sense resistors, hence saving significant board space, BOM cost, design efforts and reduces significant power consumption. This architecture removes the power dissipated in the sense resistors by using a current mirror approach and using the internal power MOSFETs for current sensing. The current regulation set point is adjusted by the voltage at the VREF pins.

A simple STEP/DIR interface allows for an external controller to manage the direction and step rate of the stepper motor. The internal microstepping indexer can execute high-accuracy micro-stepping without requiring the external controller to manage the winding current level. The indexer is capable of full step, half step, and 1/4, 1/8, 1/16, 1/32, 1/64, 1/128, and 1/256 microstepping. High microstepping contributes to significant audible noise reduction and smooth motion. In addition to a standard half stepping mode, a noncircular half stepping mode is available for increased torque output at higher motor RPM.

Stepper motor drivers need to re-circulate the winding current by implementing several types of decay modes, like slow decay, mixed decay and fast decay. The DRV8426 comes with smart tune decay modes. The smart tune is an innovative decay mechanism that automatically adjusts for optimal current regulation performance agnostic of voltage, motor speed, variation and aging effects. Smart tune Ripple Control uses a variable off-time, ripple current control scheme to minimize distortion of the motor winding current. Smart tune Dynamic Decay uses a fixed off-time, dynamic fast decay percentage scheme to minimize distortion of the motor winding current while minimizing frequency content and significantly reducing design efforts.

A low-power sleep mode is included which allows the system to save power when not actively driving the motor.

8.2 Functional Block Diagram



8-1. Functional Block Diagram

8.3 Feature Description

The following table shows the recommended values of the external components for the driver.

表 8-1. DRV8849 External Components

COMPONENT	PIN 1	PIN 2	RECOMMENDED
C_{VM1}	VM1	PGND	X7R, 0.01- μ F, VM-rated ceramic capacitor
C_{VM2}	VM2	PGND	X7R, 0.01- μ F, VM-rated ceramic capacitor
C_{VCP}	VCP	VM1	X7R, 0.22- μ F, 16-V ceramic capacitor
C_{SW}	CP1	CP2	X7R, 0.022- μ F, VM-rated ceramic capacitor
$R_{nFAULTx}$	VCC ⁽¹⁾	nFAULTx	>4.7-k Ω resistor
R_{REF1x}	VREFx	VCC	Resistor to limit chopping current.
R_{REF2x}	VREFx	GND	

(1) VCC is not a pin of the DRV8849, but a VCC supply voltage pullup is required for open-drain nFAULT outputs.

8.3.1 Stepper Motor Driver Current Ratings

Stepper motor drivers can be classified using three different numbers to describe the output current: peak, RMS, and full-scale.

8.3.1.1 Peak Current Rating

The peak current in a stepper driver is limited by the overcurrent protection trip threshold I_{OCP} . The peak current describes any transient duration current pulse, for example when charging capacitance, when the overall duty cycle is very low. In general the minimum value of I_{OCP} specifies the peak current rating of the stepper motor driver. For the DRV8849, the peak current rating is 2.5 A per bridge.

8.3.1.2 RMS Current Rating

The RMS (average) current is determined by the thermal considerations of the IC. The RMS current is calculated based on the $R_{DS(ON)}$, rise and fall time, PWM frequency, device quiescent current, and package thermal performance in a typical system at 25°C. The actual operating RMS current may be higher or lower depending on heatsinking and ambient temperature. For the DRV8849, the RMS current rating is 1.1 A per bridge.

8.3.1.3 Full-Scale Current Rating

The full-scale current describes the top of the sinusoid current waveform while microstepping. Because the sinusoid amplitude is related to the RMS current, the full-scale current is also determined by the thermal considerations of the device. The full-scale current rating is approximately $\sqrt{2} \times I_{RMS}$ for a sinusoidal current waveform, and I_{RMS} for a square wave current waveform (full step).

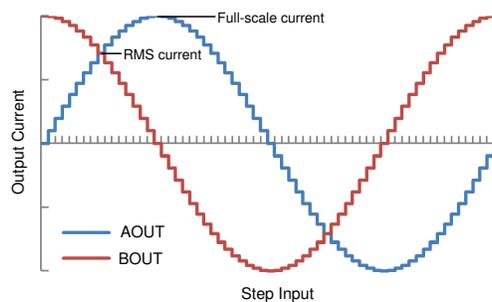


图 8-2. Full-Scale and RMS Current

8.3.2 Microstepping Indexer

Built-in indexer logic in the DRV8849 allows a number of different step modes. The MODE0 and MODE1 pins are used to configure the step mode as shown in 表 8-2. The settings can be changed on the fly.

表 8-2. Microstepping Indexer Settings

MODE0x	MODE1x	STEP MODE
0	0	Full step (2-phase excitation) with 100% current
0	330 kΩ to GND	Full step (2-phase excitation) with 71% current
1	0	Non-circular 1/2 step
Hi-Z	0	1/2 step
0	1	1/4 step
1	1	1/8 step
Hi-Z	1	1/16 step
0	Hi-Z	1/32 step
Hi-Z	330 kΩ to GND	1/64 step
Hi-Z	Hi-Z	1/128 step
1	Hi-Z	1/256 step

表 8-3 shows the relative current and step directions for full-step (71% current), 1/2 step, 1/4 step and 1/8 step operation. Higher microstepping resolutions follow the same pattern. The OUTxA current is the sine of the electrical angle and the OUTxB current is the cosine of the electrical angle. Positive current is defined as current flowing from the OUTxA pin to the OUTxB pin while driving.

At each rising edge of the STEP input the indexer travels to the next state in the table. The direction is shown with the DIR pin logic high. If the DIR pin is logic low, the sequence is reversed.

注

If the step mode is changed on the fly while stepping, the indexer advances to the next valid state for the new step mode setting at the rising edge of STEP.

The initial excitation state is an electrical angle of 45°, corresponding to 71% of full-scale current in both coils. This state is entered after power-up, after exiting logic undervoltage lockout, or after exiting sleep mode.

表 8-3. Relative Current and Step Directions

1/8 STEP	1/4 STEP	1/2 STEP	FULL STEP 71%	OUTxA CURRENT (% FULL-SCALE)	OUTxB CURRENT (% FULL-SCALE)	ELECTRICAL ANGLE (DEGREES)
1	1	1		0%	100%	0.00
2				20%	98%	11.25
3	2			38%	92%	22.50
4				56%	83%	33.75
5	3	2	1	71%	71%	45.00
6				83%	56%	56.25
7	4			92%	38%	67.50
8				98%	20%	78.75
9	5	3		100%	0%	90.00
10				98%	-20%	101.25
11	6			92%	-38%	112.50
12				83%	-56%	123.75
13	7	4	2	71%	-71%	135.00
14				56%	-83%	146.25
15	8			38%	-92%	157.50

表 8-3. Relative Current and Step Directions (continued)

1/8 STEP	1/4 STEP	1/2 STEP	FULL STEP 71%	OUTxA CURRENT (% FULL-SCALE)	OUTxB CURRENT (% FULL-SCALE)	ELECTRICAL ANGLE (DEGREES)
16				20%	-98%	168.75
17	9	5		0%	-100%	180.00
18				-20%	-98%	191.25
19	10			-38%	-92%	202.50
20				-56%	-83%	213.75
21	11	6	3	-71%	-71%	225.00
22				-83%	-56%	236.25
23	12			-92%	-38%	247.50
24				-98%	-20%	258.75
25	13	7		-100%	0%	270.00
26				-98%	20%	281.25
27	14			-92%	38%	292.50
28				-83%	56%	303.75
29	15	8	4	-71%	71%	315.00
30				-56%	83%	326.25
31	16			-38%	92%	337.50
32				-20%	98%	348.75

表 8-4 shows the full step operation with 100% full-scale current. This stepping mode consumes more power than full-step mode with 71% current, but provides a higher torque at high motor RPM.

表 8-4. Full Step with 100% Current

FULL STEP 100%	OUTxA CURRENT (% FULL-SCALE)	OUTxB CURRENT (% FULL-SCALE)	ELECTRICAL ANGLE (DEGREES)
1	100	100	45
2	100	-100	135
3	-100	-100	225
4	-100	100	315

表 8-5 shows the noncircular 1/2–step operation. This stepping mode consumes more power than circular 1/2–step operation, but provides a higher torque at high motor RPM.

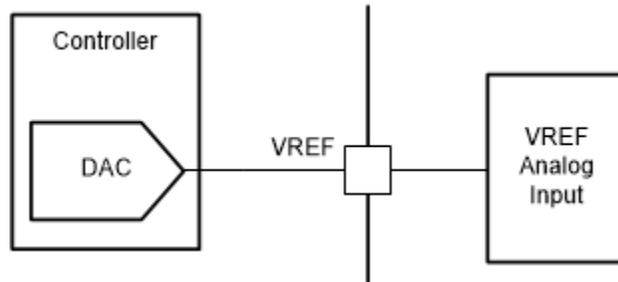
表 8-5. Non-Circular 1/2-Stepping Current

NON-CIRCULAR 1/2-STEP	OUTxA CURRENT (% FULL-SCALE)	OUTxB CURRENT (% FULL-SCALE)	ELECTRICAL ANGLE (DEGREES)
1	0	100	0
2	100	100	45
3	100	0	90
4	100	-100	135
5	0	-100	180
6	-100	-100	225
7	-100	0	270
8	-100	100	315

8.3.3 Controlling VREF with an MCU DAC

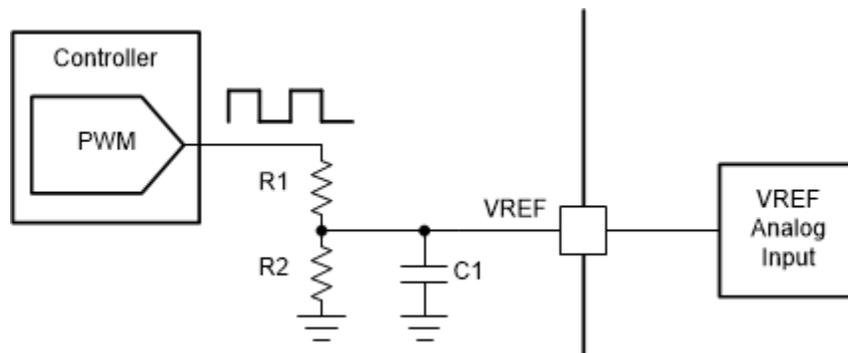
In some cases, the full-scale output current may need to be changed between many different values, depending on motor speed and loading. The voltage of the VREF pin can be adjusted in the system to change the full-scale current.

In this mode of operation, as the DAC voltage increases, the full-scale regulation current increases as well. For proper operation, the output of the DAC should not rise above 3.3 V for DRV8849.



8-3. Controlling VREF with a DAC Resource

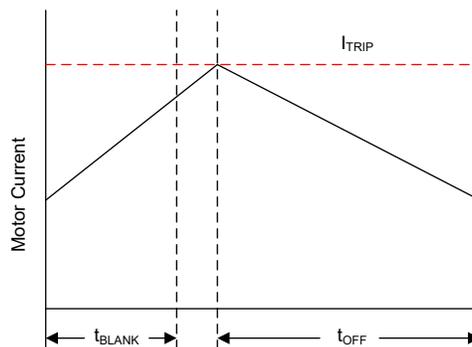
The VREF pin can also be adjusted using a PWM signal and low-pass filter.



8-4. Controlling VREF With a PWM Resource

8.3.4 Current Regulation and Decay Modes

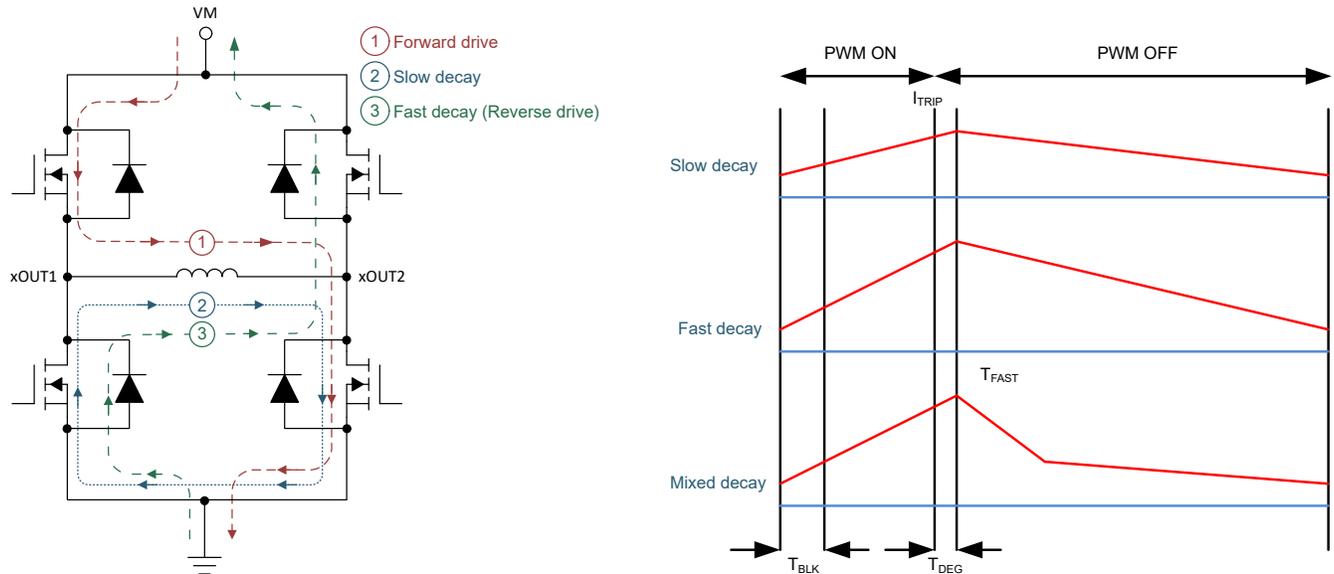
The current through the motor windings is regulated by an adjustable, off-time PWM current-regulation circuit. When an H-bridge is enabled, current rises through the winding at a rate dependent on the DC voltage, inductance of the winding, and the magnitude of the back EMF present. When the current hits the current regulation threshold (as shown in 8-6, Item 1), the bridge enters a decay mode determined by the DECAY pin setting to decrease the current. After the off-time expires, the bridge is re-enabled, starting another PWM cycle.



8-5. Current Chopping Waveform

Once the chopping current threshold is reached, the H-bridge can operate in two different states, fast decay or slow decay.

- In fast decay mode, as soon as the PWM chopping current level is reached, the H-bridge reverses state by switching on the opposite arm MOSFETs to allow the winding current to flow in the opposite direction. As the winding current approaches zero, the H-bridge is disabled to prevent further reverse current flow. Fast decay mode is shown in 8-6, item 2.
- In slow decay mode, the winding current is re-circulated by enabling both low-side MOSFETs in the H-bridge. This is shown in 8-6, Item 3.



8-6. Decay Modes

The PWM regulation current is set by a comparator which monitors the voltage across the current sense MOSFETs in parallel with the low-side power MOSFETs. The current sense MOSFETs are biased with a reference current that is the output of a current-mode sine-weighted DAC whose full-scale reference current is set by the voltage at the VREF pins.

The full-scale regulation current (I_{FS}) can be calculated as -

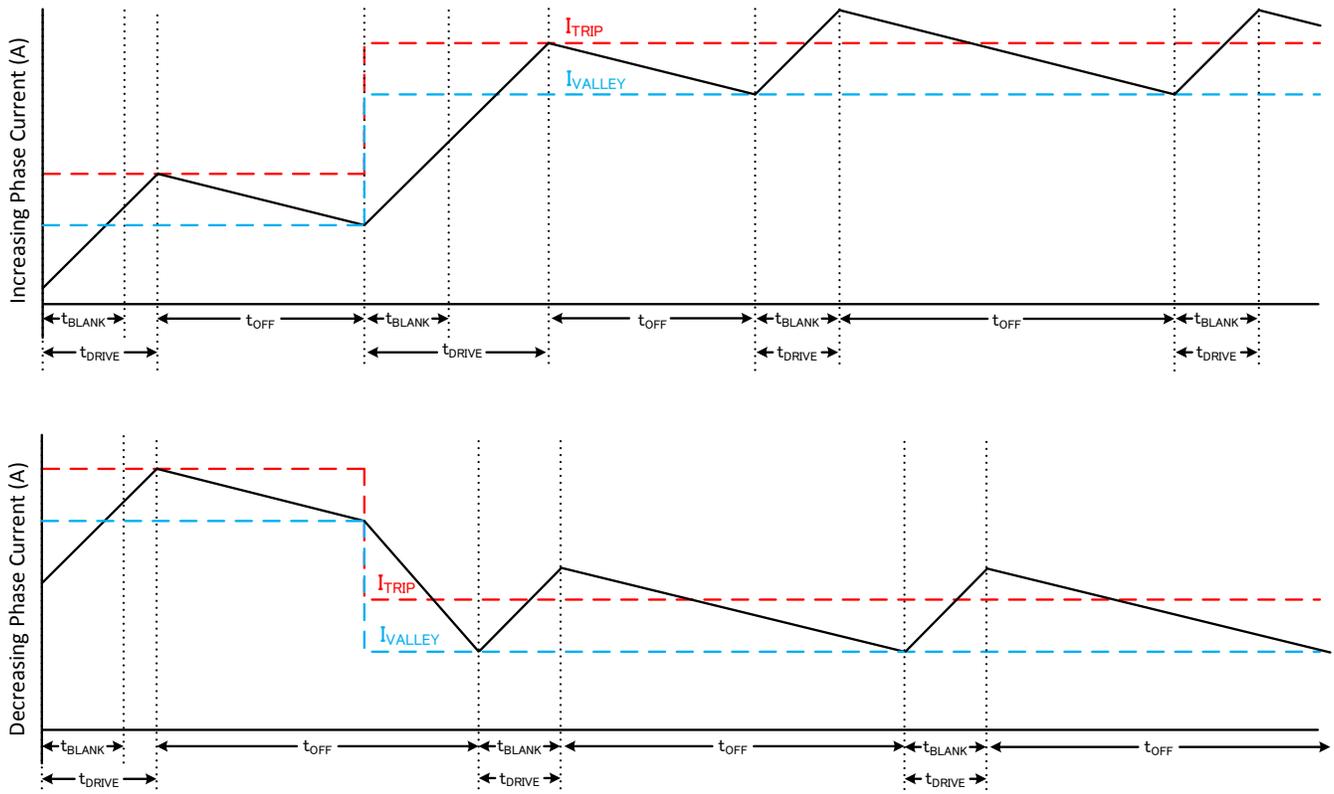
$$I_{FS} (A) = V_{REFx} (V) / K_V (V/A) = V_{REFx} (V) / 2.2 (V/A).$$

The decay mode of the DRV8849 is selected by the DECAY pins as shown in 8-6. The decay modes can be changed on the fly. After a decay mode change, the new decay mode is applied after a 2 μ s de-glitch time.

表 8-6. Decay Mode Settings

DECAYx	DECAY MODE
0	Smart tune Ripple Control
1	Smart tune Dynamic Decay, 16 μ s OFF time
Hi-Z	Smart tune Dynamic Decay, 32 μ s OFF time
330k to GND	Smart tune Dynamic Decay, 8 μ s OFF time

8.3.4.1 Smart tune Ripple Control



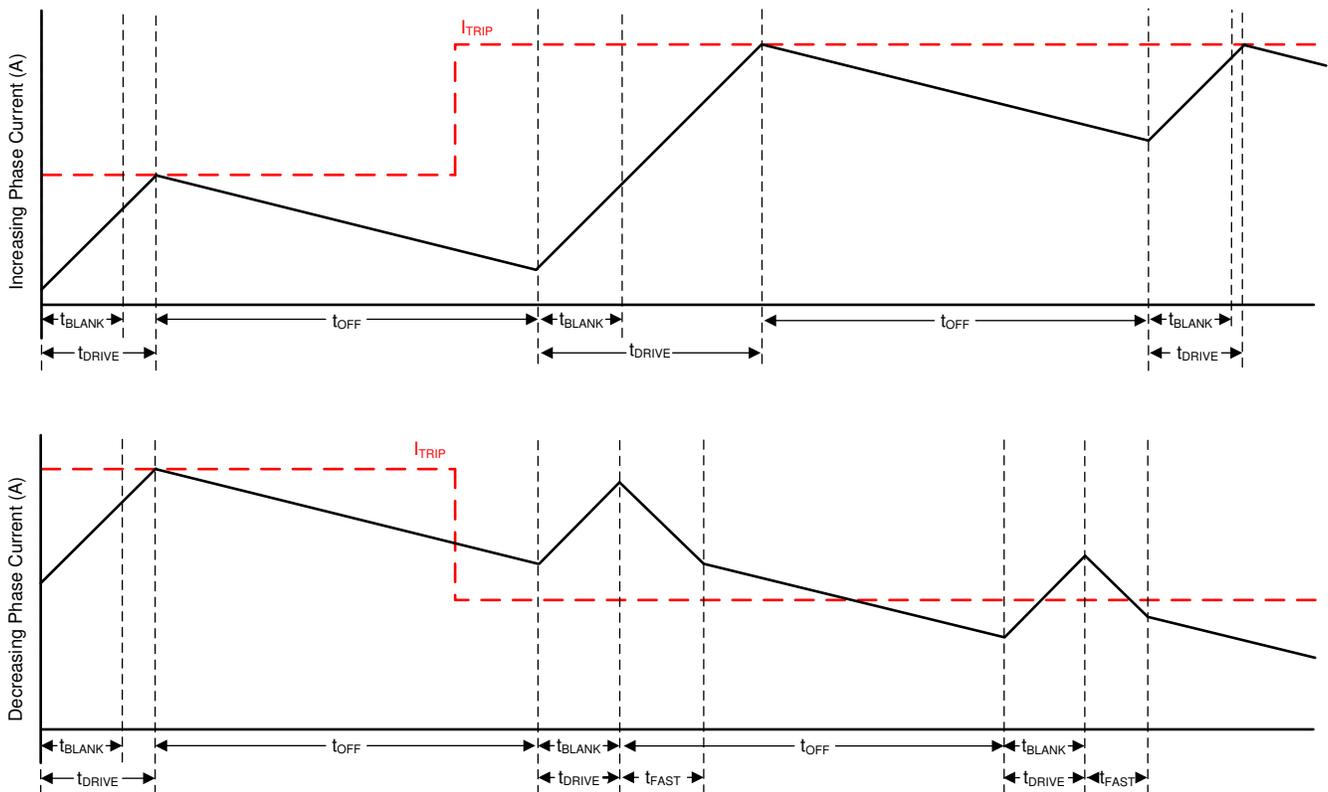
8-7. Smart tune Ripple Control Decay Mode

Smart tune Ripple Control operates by setting an I_{VALLEY} level alongside the I_{TRIP} level. When the current level reaches I_{TRIP} , instead of entering slow decay until the t_{OFF} time expires, the driver enters slow decay until I_{VALLEY} is reached. Slow decay operates by turning on both low-side MOSFETs, allowing the current to recirculate. In this mode, t_{OFF} varies depending on the current level and operating conditions.

The ripple current in this decay mode is $11 \text{ mA} + 1\%$ of I_{TRIP} , where I_{TRIP} is the regulation current of a particular microstep level.

The ripple control method allows much tighter regulation of the current level, thereby increasing motor efficiency and reducing audible noise and vibration. Smart tune Ripple Control can be used in systems that can tolerate a variable off-time regulation scheme to achieve small current ripple in the current regulation.

8.3.4.2 Smart tune Dynamic Decay



8-8. Smart tune Dynamic Decay Mode

Unlike smart tune Ripple Control, smart tune Dynamic Decay operates with fixed OFF time. Smart tune Dynamic Decay dynamically adjusts the fast decay percentage of the total mixed decay time. This eliminates the need for motor decay tuning by automatically determining the best mixed decay setting that results in the lowest ripple and best performance for the motor.

The fast decay percentage is optimized iteratively each PWM cycle. If the motor current overshoots the target I_{TRIP} level, then the mixed decay mode becomes more aggressive (by increasing fast decay percentage) on the next cycle to prevent loss of current regulation. If a long drive time must occur to reach the target I_{TRIP} level, the decay mode becomes less aggressive (by reducing fast decay percentage) on the next cycle to operate with less ripple. On falling steps, smart tune Dynamic Decay automatically switches to fast decay to reach the next step quickly. Smart tune Dynamic Decay operates with fixed 8 μ s, 16 μ s or 32 μ s OFF time.

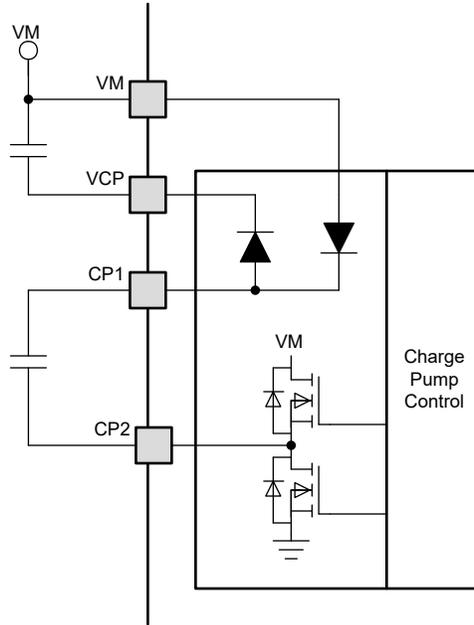
Smart tune Dynamic Decay is optimal for applications that require minimal current ripple but want to maintain a fixed frequency in the current regulation scheme.

8.3.4.3 Blanking time

This function blanks the output of the current sense comparator when the outputs are switched by the internal current control circuitry. The comparator output is blanked to prevent false detections of overcurrent conditions, due to reverse recovery currents, or to switching transients related to the capacitance of the load. The blank time, t_{BLANK} , is approximately 1 μ s.

8.3.5 Charge Pump

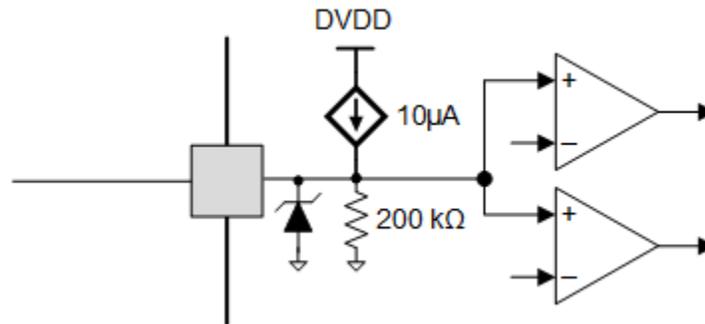
A charge pump is integrated to supply a high-side N-channel MOSFET gate-drive voltage. The charge pump requires a capacitor between the VM and VCP pins to act as the storage capacitor. Additionally a ceramic capacitor is required between the CP1 and CP2 pins to act as the flying capacitor.



8-9. Charge pump

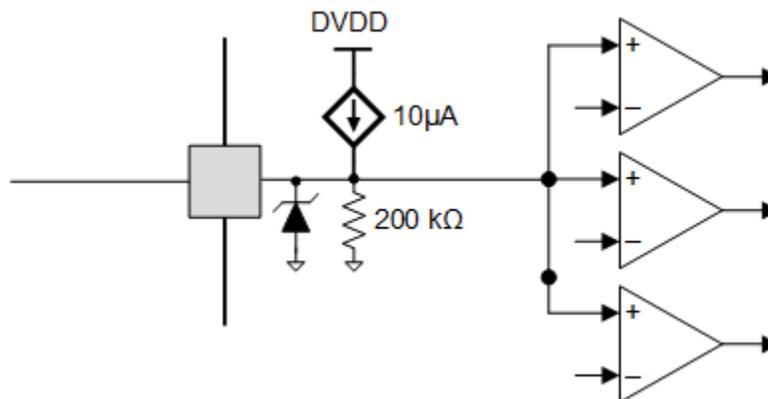
8.3.6 Logic Level, tri-level and quad-level Pin Diagrams

The following diagram shows the input structure for MODE0x, and ENABLE pins.



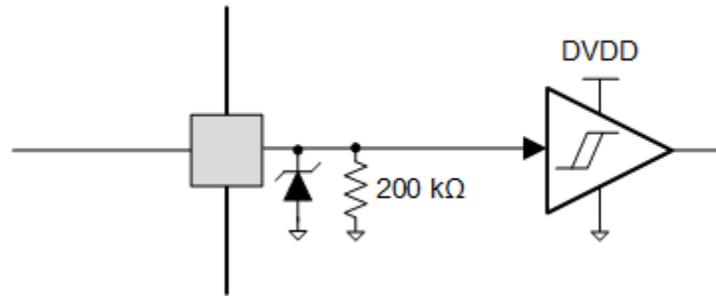
8-10. Tri-Level Input Pin Diagram

8-11 shows the input structure for MODE1x and DECAYx pins.



8-11. Quad-Level Input Pin Diagram

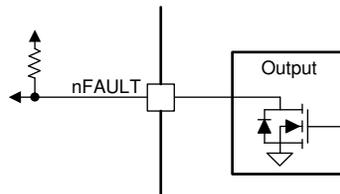
☒ 8-12 shows the input structure for STEP, DIR and nSLEEP pins.



☒ 8-12. Logic-Level Input Pin Diagram

8.3.7 nFAULT Pins

The nFAULT pins have open-drain outputs and should be pulled up to a 5-V, 3.3-V or 1.8-V supply. When a fault is detected, the nFAULT pin of the corresponding stepper will be logic low. nFAULT pin will be high after power-up. An external supply must be used for pulling up the nFAULT pins.



☒ 8-13. nFAULT Pins

8.3.8 Protection Circuits

The DRV8849 is fully protected against supply undervoltage, charge pump undervoltage, output overcurrent, and device overtemperature events.

8.3.8.1 VM Undervoltage Lockout (UVLO)

If at any time the voltage on the VM pins fall below the UVLO-threshold voltage for the voltage supply, all the outputs are disabled, and the nFAULT pins are driven low. The charge pump is disabled in this condition. Normal operation resumes (motor-driver operation and nFAULT released) when the VM undervoltage condition is removed.

8.3.8.2 VCP Undervoltage Lockout (CPUV)

If at any time the voltage on the VCP pin falls below the CPUV voltage, all the outputs are disabled, and the nFAULT pins are driven low. The charge pump remains active during this condition. Normal operation resumes (motor-driver operation and nFAULT released) when the VCP undervoltage condition is removed.

8.3.8.3 Overcurrent Protection (OCP)

An analog current-limit circuit on each FET limits the current through the FET by removing the gate drive. If this current limit persists for longer than the t_{OCP} time, the FETs in both H-bridges for that stepper driver are disabled and the corresponding nFAULT pin is driven low. The charge pump remains active during this condition. The overcurrent protection can operate in two different modes: latched shutdown and automatic retry. The operating modes can be changed on the fly.

The ENABLE pin for a particular stepper driver should be Hi-Z to select latched shutdown mode, and should be HIGH (>2.7 V) to select automatic retry mode. ENABLE1 pin controls the OCP recovery method for Stepper 1, and ENABLE2 pin controls the OCP recovery method for Stepper 2.

8.3.8.3.1 Latched Shutdown

In this mode, after an OCP event, the outputs of the affected stepper driver are disabled and the corresponding nFAULT pin is driven low. Once the OCP condition is removed, normal operation resumes after applying an nSLEEP reset pulse or a power cycling.

8.3.8.3.2 Automatic Retry

In this mode, after an OCP event the outputs of the affected stepper are disabled and the corresponding nFAULT pin is driven low. Normal operation resumes automatically (motor-driver operation and nFAULT released) after the t_{RETRY} time has elapsed and the fault condition is removed.

8.3.8.4 Thermal Shutdown (OTSD)

If the die temperature exceeds the thermal shutdown limit (T_{OTSD}), all MOSFETs are disabled, and the nFAULT pins are driven low. The charge pump is disabled during this condition. The thermal shutdown protection can operate in two different modes: latched shutdown and automatic retry. The operating modes can be changed on the fly.

The ENABLE1 pin should be Hi-Z to select latched shutdown mode, and should be HIGH ($>2.7V$) to select automatic retry mode. ENABLE1 pin controls the OTSD recovery method for both Stepper drivers.

8.3.8.4.1 Latched Shutdown

In this mode, after an OTSD event, all the outputs are disabled and the nFAULT pins are driven low. After the junction temperature falls below the overtemperature threshold limit minus the hysteresis ($T_{OTSD} - T_{HYS_OTSD}$), normal operation resumes after applying an nSLEEP reset pulse or a power cycling.

8.3.8.4.2 Automatic Retry

In this mode, after an OTSD event, all the outputs are disabled and the nFAULT pins are driven low. Normal operation resumes (motor-driver operation and the nFAULT lines released) when the junction temperature falls below the overtemperature threshold limit minus the hysteresis ($T_{OTSD} - T_{HYS_OTSD}$).

8.3.8.5 Fault Condition Summary

表 8-7. Fault Condition Summary

FAULT	CONDITION	CONFIGURATION	ERROR REPORT	H-BRIDGE	CHARGE PUMP	INDEXER	LOGIC	RECOVERY
VM undervoltage (UVLO)	$VM < V_{UVLO}$	—	nFAULT1, nFAULT2	Disabled	Disabled	Disabled	Reset ($VM < 3.9V$)	Automatic: $VM > V_{UVLO}$
VCP undervoltage (CPUV)	$VCP < V_{CPUV}$	—	nFAULT1, nFAULT2	Disabled	Operating	Operating	Operating	$VCP > V_{CPUV}$
Overcurrent (OCP)	$I_{OUT1} > I_{OCP}$	ENABLE1 = Hi-Z	nFAULT1	Disabled (Stepper 1)	Operating	Operating	Operating	Latched (Stepper 1)
		ENABLE1 = 1	nFAULT1	Disabled (Stepper 1)	Operating	Operating	Operating	Automatic retry (Stepper 1) : t_{RETRY}
	$I_{OUT2} > I_{OCP}$	ENABLE2 = Hi-Z	nFAULT2	Disabled (Stepper 2)	Operating	Operating	Operating	Latched (Stepper 2)
		ENABLE2 = 1	nFAULT2	Disabled (Stepper 2)	Operating	Operating	Operating	Automatic retry (Stepper 2) : t_{RETRY}
Thermal Shutdown (OTSD)	$T_J > T_{TSD}$	ENABLE1 = Hi-Z	nFAULT1, nFAULT2	Disabled	Disabled	Operating	Operating	Latched
		ENABLE1 = 1	nFAULT1, nFAULT2	Disabled	Disabled	Operating	Operating	Automatic: $T_J < T_{OTSD} - T_{HYS_OTSD}$

8.4 Device Functional Modes

8.4.1 Sleep Mode (nSLEEP = 0)

The device state is managed by the nSLEEP pin. When the nSLEEP pin is low, the device enters a low-power sleep mode. In sleep mode, all the internal MOSFETs are disabled and the charge pump is disabled. The t_{SLEEP} time must elapse after a falling edge on the nSLEEP pin before the device enters sleep mode. The device is brought out of sleep automatically if the nSLEEP pin is brought high. The t_{WAKE} time must elapse before the device is ready for inputs.

8.4.2 Disable Mode (nSLEEP = 1, ENABLE = 0)

The ENABLE pin is used to enable or disable the device. When the ENABLE pin is low, the corresponding output drivers are disabled in the Hi-Z state.

8.4.3 Operating Mode (nSLEEP = 1, ENABLE = Hi-Z/1)

When the nSLEEP pin is high, the ENABLE pin is Hi-Z or 1, and $V_M > UVLO$, the corresponding stepper enters the active mode. The t_{WAKE} time must elapse before the stepper is ready for inputs.

8.4.4 nSLEEP Reset Pulse

A fault can be cleared through a quick nSLEEP pulse. This pulse width must be greater than $20\ \mu\text{s}$ and shorter than $40\ \mu\text{s}$. If nSLEEP is low for longer than $40\ \mu\text{s}$ but less than $120\ \mu\text{s}$, the faults are cleared and the device may or may not shutdown, as shown in the timing diagram. This reset pulse does not affect the status of the charge pump or other functional blocks.

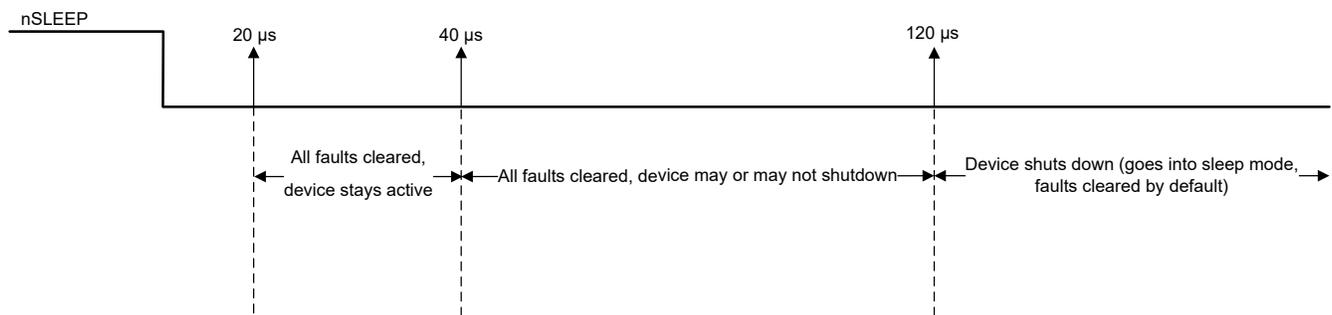


图 8-14. nSLEEP Reset Pulse

8.4.5 Functional Modes Summary

表 8-8 lists a summary of the functional modes.

表 8-8. Functional Modes Summary

	CONDITION	CONFIGURATI ON	H-BRIDGE	CHARGE PUMP	INDEXER	Logic
Sleep mode	$4.5\ \text{V} < V_M < 38\ \text{V}$	nSLEEP pin = 0	Disabled	Disabled	Disabled	Disabled
Operating	$4.5\ \text{V} < V_M < 38\ \text{V}$	nSLEEP pin = 1 ENABLE pin = 1 or Hi-Z	Operating	Operating	Operating	Operating
Disabled	$4.5\ \text{V} < V_M < 38\ \text{V}$	nSLEEP pin = 1 ENABLE pin = 0	Disabled	Operating	Operating	Operating

9 Application and Implementation

注

以下のアプリケーション情報は、TI の製品仕様に含まれるものではなく、TI ではその正確性または完全性を保証いたしません。個々の目的に対する製品の適合性については、お客様の責任で判断していただくこととなります。お客様は自身の設計実装を検証しテストすることで、システムの機能を確認する必要があります。

9.1 Application Information

The DRV8849 is used to control two bipolar stepper motors.

9.2 Typical Application

The following design procedure can be used to configure the DRV8849 to drive two stepper motors.

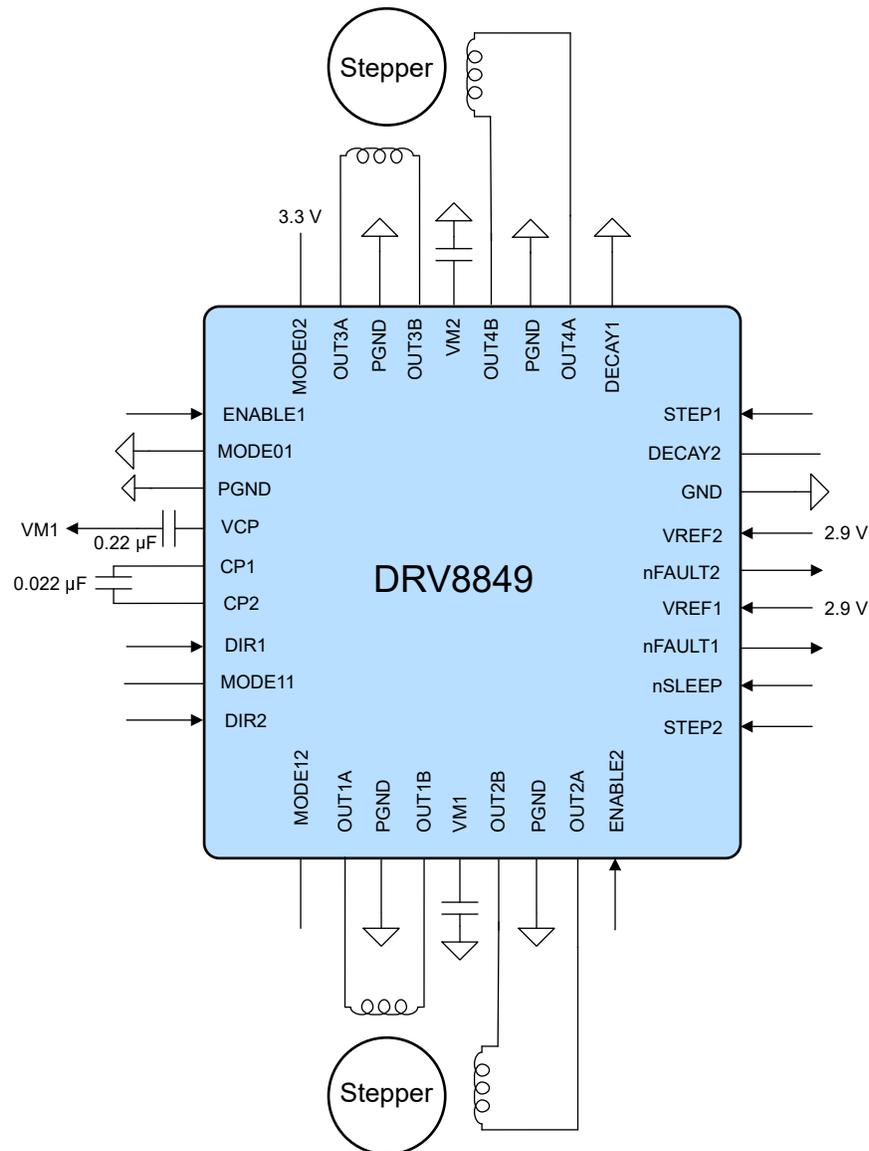


図 9-1. Typical Application Schematic

9.2.1 Design Requirements

表 9-1 lists the design input parameters for a typical application.

表 9-1. Design Parameters

DESIGN PARAMETER	REFERENCE	EXAMPLE VALUE
Supply voltage	VM	24 V
Motor 1 winding resistance	R _{L1}	2.4 Ω/phase
Motor 2 winding resistance	R _{L2}	2 Ω/phase
Motor 1 winding inductance	L _{L1}	5.8 mH/phase
Motor 2 winding inductance	L _{L2}	4.7 mH/phase
Motor 1 full step angle	θ _{step1}	1.8°/step
Motor 2 full step angle	θ _{step2}	1.8°/step
Target microstepping level (motor 1)	n _{m1}	1/32 step
Target microstepping level (motor 2)	n _{m2}	1/256 step
Target motor 1 speed	v ₁	46.8 rpm
Target motor 2 speed	v ₂	23.4 rpm
Target full-scale current (motor 1)	I _{FS1}	1.3 A
Target full-scale current (motor 2)	I _{FS2}	1.3 A

9.2.2 Detailed Design Procedure

9.2.2.1 Stepper Motor Speed

The first step in configuring the DRV8849 requires the desired motor speed and microstepping level. If the target application requires a constant speed, then a square wave with frequency f_{step} must be applied to the corresponding STEP pin. If the target motor speed is too high, the motor does not spin. Make sure that the motor can support the target speed. Use 式 1 to calculate f_{step} for a desired motor speed (v), microstepping level (n_m), and motor full step angle (θ_{step})

$$f_{\text{step}} \text{ (steps / s)} = \frac{v \text{ (rpm)} \times 360 \text{ (}^\circ \text{ / rot)}}{\theta_{\text{step}} \text{ (}^\circ \text{ / step)} \times n_m \text{ (steps / microstep)} \times 60 \text{ (s / min)}} \quad (1)$$

The value of θ_{step} can be found in the stepper motor data sheet, or written on the motor. For example, the motors in this application are required to rotate at 1.8°/step for a target of 46.8 rpm at 1/32 microstep mode (for Motor 1); and for a target of 23.4 rpm at 1/256 microstep mode (for Motor 2). Using 式 1, f_{step} can be calculated as 5 kHz for Motor 1 and 20 kHz for Motor 2.

The microstepping level is set by the MODE0x and MODE1x pins and can be any of the settings listed in 表 8-2. Higher microstepping results in a smoother motor motion and less audible noise, but requires a higher f_{step} to achieve the same motor speed.

9.2.2.2 Current Regulation

In a stepper motor, the full-scale current (I_{FS}) is the maximum current driven through either winding. This quantity depends on the VREF voltage. The maximum allowable voltage on the VREF pin is 3.3 V for DRV8849. During stepping, I_{FS} defines the current chopping threshold (I_{TRIP}) for the maximum current step. $I_{\text{FS}} \text{ (A)} = V_{\text{REF}} \text{ (V)} / 2.2 \text{ (V/A)}$

9.2.2.3 Decay Modes

The DRV8849 supports two different smart tune decay modes, as shown in 表 8-6. In this example, motor 1 is driven with smart tune ripple control decay mode, whereas the motor 2 is driven with smart tune dynamic decay mode with 32 μs OFF time.

9.2.2.4 Application Curves

CH2: STEP2 (5 V/div), CH3: STEP1 (5 V/div), CH7: IOUT_1 (1 A/div), CH8: IOUT_4 (1 A/div)



9-2. DRV8849 driving two Stepper Motors

10 Layout

- A low-ESR ceramic capacitor must be placed in between the CP1 and CP2 pins. A value of 0.022 μF rated for VM is recommended. Place this component as close to the pins as possible.
- A low-ESR ceramic capacitor must be placed in between the VM and VCP pins. A value of 0.22 μF rated for 16 V is recommended. Place this component as close to the pins as possible.
- The device must be soldered directly onto the PCB. The thermal pad should be soldered directly to an exposed surface on the PCB. Thermal vias should be used to transfer heat to other layers of the PCB.
- It is important to have a low impedance single-point ground located very close to the device. Connect the exposed pad and the ground plane directly under the device ground.
- The input capacitors should be placed as close to the device supply pins as possible. The ceramic capacitor should be closer to the pins than the bulk capacitor.

10.1 Layout Guidelines

Follow the layout example of the DRV8849 EVM. The design files can be downloaded from the [DRV8849EVM](#) product folder.

10.2 Bulk Capacitance

Having appropriate local bulk capacitance is an important factor in motor drive system design. It is generally beneficial to have more bulk capacitance, while the disadvantages are increased cost and physical size.

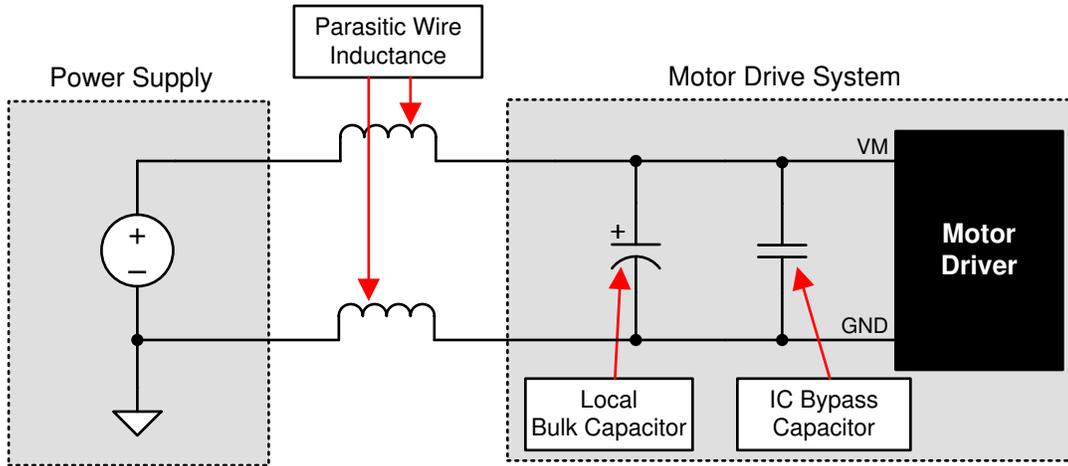
The amount of local capacitance needed depends on a variety of factors, including:

- The highest current required by the motor system
- The power supply's capacitance and ability to source current
- The amount of parasitic inductance between the power supply and motor system
- The acceptable voltage ripple
- The type of motor used (brushed DC, brushless DC, stepper)
- The motor braking method

The inductance between the power supply and motor drive system will limit the rate current can change from the power supply. If the local bulk capacitance is too small, the system will respond to excessive current demands or dumps from the motor with a change in voltage. When adequate bulk capacitance is used, the motor voltage remains stable and high current can be quickly supplied.

The data sheet generally provides a recommended value, but system-level testing is required to determine the appropriate sized bulk capacitor.

The voltage rating for bulk capacitors should be higher than the operating voltage, to provide margin for cases when the motor transfers energy to the supply.



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10-1. Example Setup of Motor Drive System With External Power Supply

11 デバイスおよびドキュメントのサポート

11.1 関連資料

関連資料については、以下を参照してください。

- テキサス・インスツルメンツ、『ステップ・モーターの可聴ノイズを低減する方法』アプリケーション・レポート
- テキサス・インスツルメンツ、『動作の滑らかさと精度を向上させる方法』アプリケーション・レポート
- テキサス・インスツルメンツ、『DRV8xxx によるユニポーラ・ステップ・モーターの駆動方法』アプリケーション・レポート
- テキサス・インスツルメンツ、『モータ・ドライブ消費電力の計算』アプリケーション・レポート (英語)
- テキサス・インスツルメンツ、『電流再循環および減衰モード』アプリケーション・レポート (英語)
- テキサス・インスツルメンツ、『モータ・ドライブの電流定格の理解』アプリケーション・レポート (英語)
- テキサス・インスツルメンツ、『モータ・ドライブのレイアウト・ガイド』アプリケーション・レポート

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package Pins	Package qty Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
DRV8849RHHR	Active	Production	VQFN (RHH) 36	4000 LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	DRV8849
DRV8849RHHR.A	Active	Production	VQFN (RHH) 36	4000 LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	DRV8849

(1) **Status:** For more details on status, see our [product life cycle](#).

(2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

(3) **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

(4) **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

(5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

(6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

Important Information and Disclaimer: The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

GENERIC PACKAGE VIEW

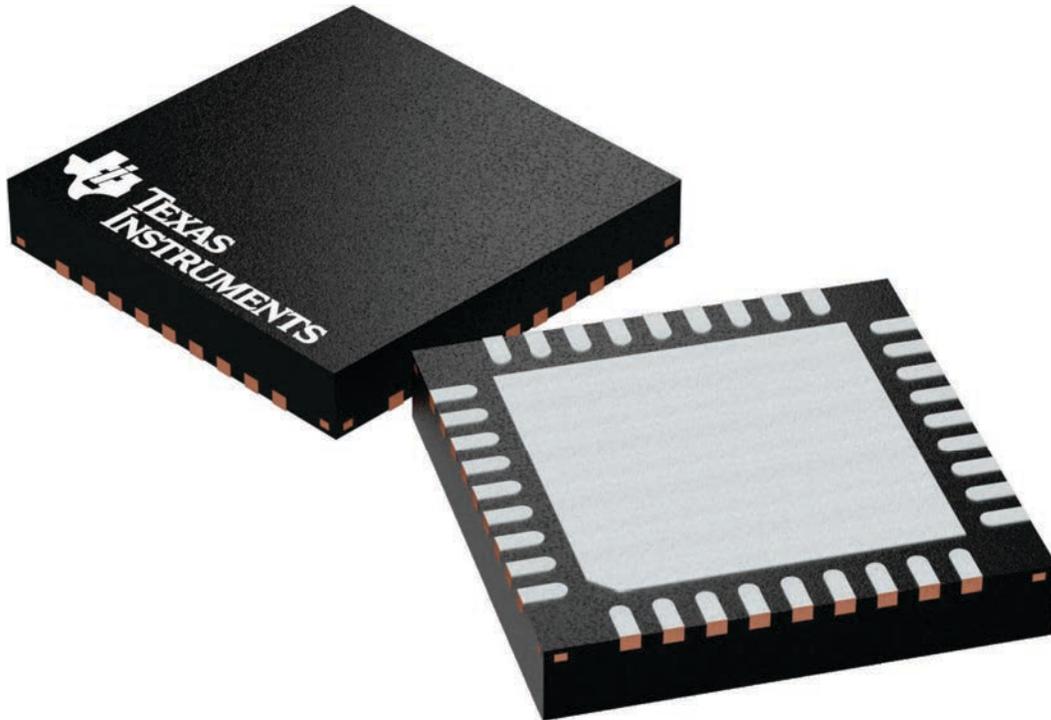
RHH 36

VQFN - 1 mm max height

6 x 6, 0.5 mm pitch

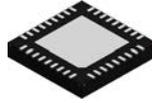
PLASTIC QUAD FLATPACK - NO LEAD

This image is a representation of the package family, actual package may vary.
Refer to the product data sheet for package details.



4225440/A

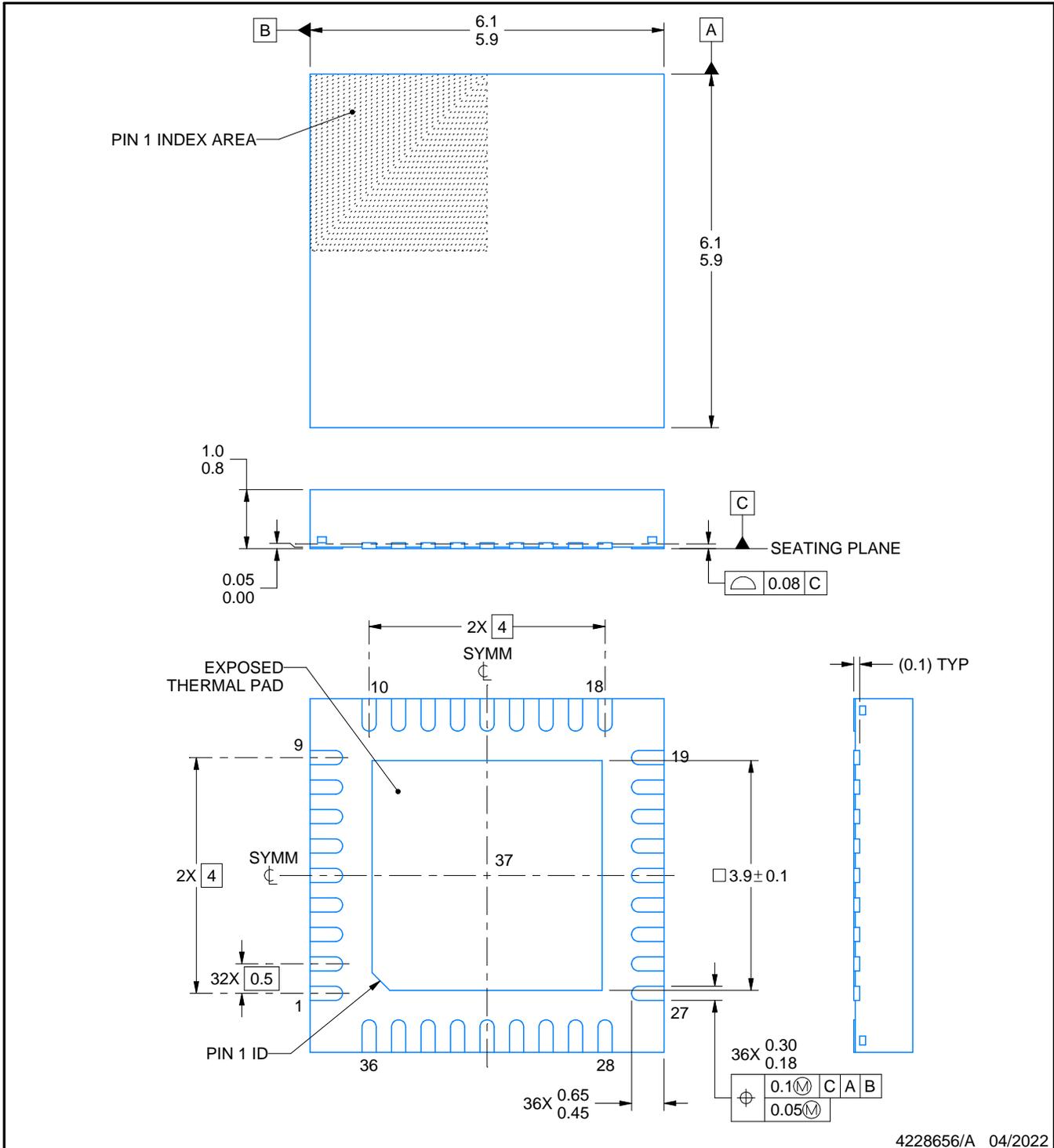
RHH0036H



PACKAGE OUTLINE

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



NOTES:

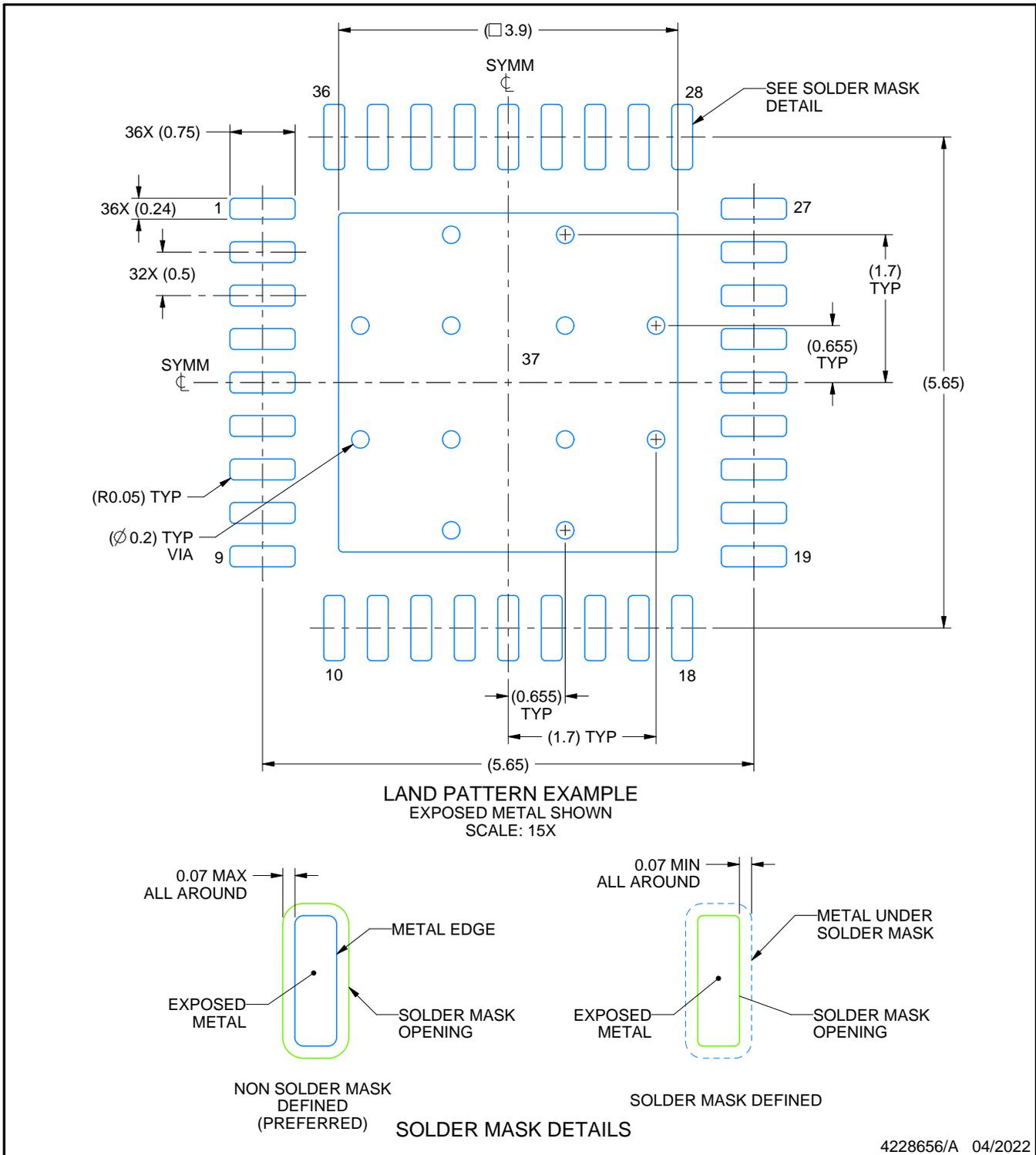
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.

EXAMPLE BOARD LAYOUT

RHH0036H

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



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NOTES: (continued)

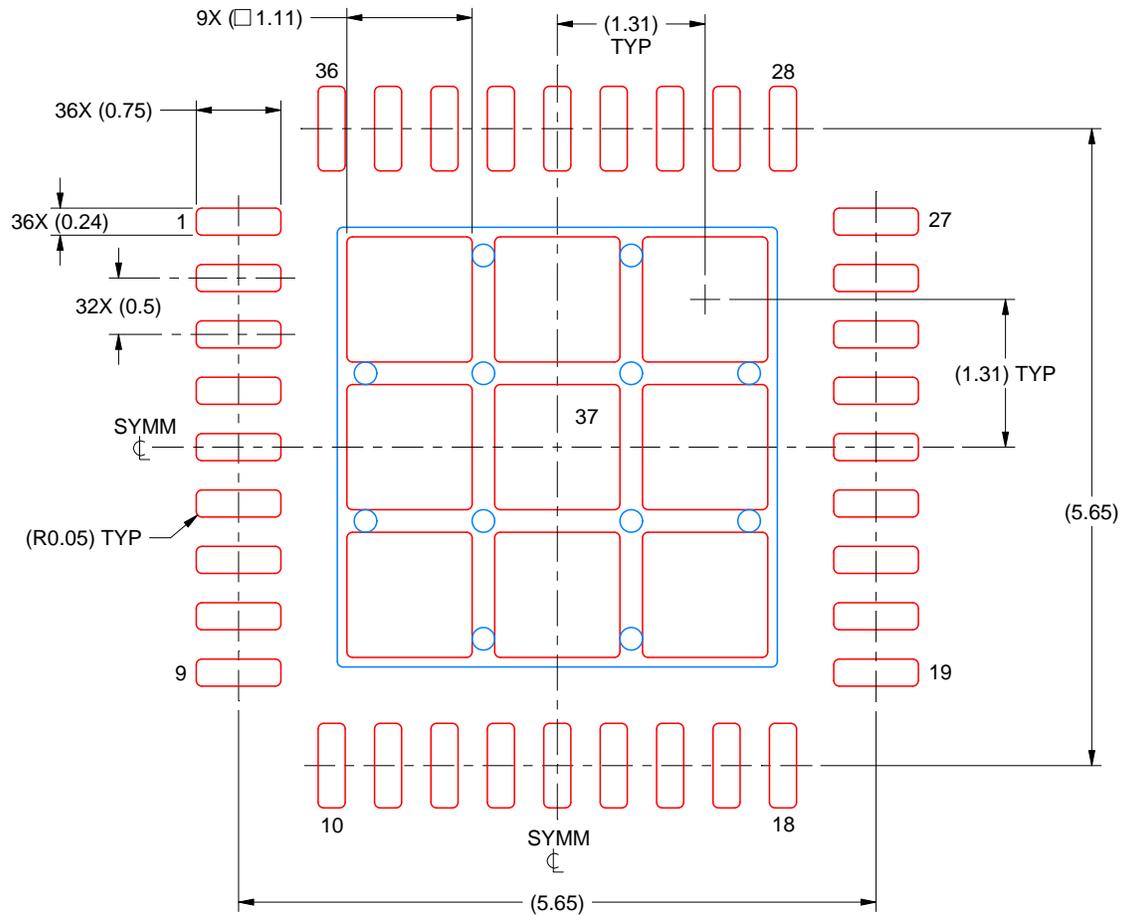
4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/sluea271).
5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.

EXAMPLE STENCIL DESIGN

RHH0036H

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



SOLDER PASTE EXAMPLE
BASED ON 0.125 MM THICK STENCIL
SCALE: 15X

EXPOSED PAD 37
73% PRINTED SOLDER COVERAGE BY AREA UNDER PACKAGE

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NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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