

# LPV521 ナノパワー、1.8V、RRIO、CMOS 入力オペアンプ

## 1 特長

- $V_S = 5V$  (特に記載のない限り標準値):
  - 電源電流 ( $V_S = 0.3V$  時): 400nA (最大値)
  - 動作電圧範囲: 1.6V~5.5V
  - 低い  $TCV_{OS}$ : 3.5 $\mu V/^\circ C$  (最大値)
  - $V_{OS}$ : 1mV (最大値)
  - 入力バイアス電流: 40fA
  - PSRR: 109dB
  - CMRR: 102dB
  - 開ループ ゲイン: 132dB
  - ゲイン帯域幅積: 6.2kHz
  - スルーレート: 2.4V/ms
  - 入力電圧ノイズ ( $f = 100Hz$  時): 255nV/ $\sqrt{Hz}$
  - 温度範囲: -40 $^\circ C$ ~+125 $^\circ C$

## 2 アプリケーション

- ワイヤレス環境センサ
- グリッド アセット監視
- 電気メータ
- 煙探知器と熱探知器
- ガス検出器
- ポータブル エレクトロニクス
- サーモスタット
- フィールドトランスミッタとセンサ

## 3 概要

LPV521 は、非常に長いバッテリー寿命を必要とするアプリケーション向けに設計されたシングル ナノパワー 552nW アンプです。1.6V~5.5V の動作電圧範囲と標準 351nA の消費電流の組み合わせにより、RFID リーダーやリモートセンサなどのナノパワー アプリケーションに最適です。入力同相モード電圧はレール全体にわたって 0.1V であり、 $TCV_{OS}$  が保証され、レール ツーレールの電圧出力性能を備えています。LPV521 の CMOS 入力段は注意深く設計され、標準で 40fA という低い  $I_{BIAS}$  電流によって競合製品に差を付けています。この低い入力電流により、メガオーム抵抗や高インピーダンスのフォトダイオード、充電センサなどの状況で生じる、 $I_{BIAS}$  や  $I_{OS}$  の誤差が大きく減少します。LPV521 は PowerWise® ファミリの製品であり、電力対性能比が非常に優れています。

広い入力同相モード電圧範囲、保証された 1mV の  $V_{OS}$  および 3.5 $\mu V/^\circ C$  の  $TCV_{OS}$  により、ハイサイドとローサイド両方の電流センシングで正確で安定した測定を実現します。

また、EMI 保護が組み込まれ、携帯電話や他の RFID リーダーからの不要な RF 信号による影響を低減しています。

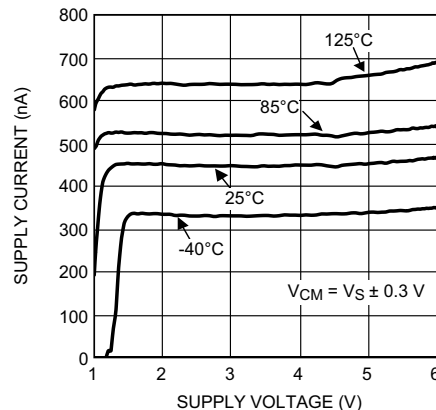
LPV521 は、5 ピン SC70 および 8 ピン PDIP パッケージで供給されます。

### パッケージ情報

部品番号	パッケージ (1)	パッケージ サイズ(2)
LPV521	DCK (SC70, 5)	2mm × 2.1mm
	P (PDIP, 8)	9.81mm × 9.43mm

(1) 詳細については、[セクション 10](#) を参照してください。

(2) パッケージ サイズ (長さ × 幅) は公称値であり、該当する場合はピンも含まれます。



### NanoPower の消費電流



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## 4 Pin Configuration and Functions

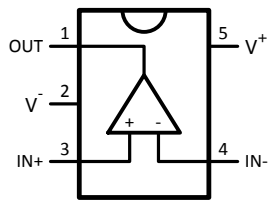


図 4-1. DCK Package, 5-Pin SC70 (Top View)

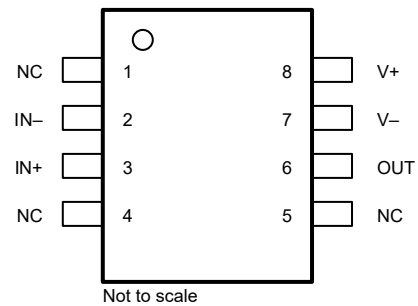


図 4-2. P Package, 8-Pin PDIP (Top View)

表 4-1. Pin Functions

NAME	PIN		TYPE	DESCRIPTION
	NO.			
	DCK (SC70)	P (PDIP)		
IN+	3	3	Input	Noninverting input
IN-	4	2	Input	Inverting input
OUT	1	6	Output	Output
NC	—	1, 4, 5	—	Do not connect
V+	5	8	Power	Positive power supply
V-	2	7	Power	Negative power supply

## 5 Specifications

### 5.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
	Any pin relative to V <sup>-</sup>	-0.3	6	V
	Input voltage, IN <sup>+</sup> , IN <sup>-</sup> , OUT pins	V <sup>-</sup> - 0.3	V <sup>+</sup> + 0.3	V
	Input current, V <sup>+</sup> , V <sup>-</sup> , OUT pins		40	mA
	Differential input voltage (V <sub>IN+</sub> - V <sub>IN-</sub> )	-300	300	mV
T <sub>J</sub>	Junction temperature <sup>(2)</sup>	-40	150	°C
	Mounting temperature	Infrared or convection (30s)	260	°C
		Wave soldering lead temperature (4s)	260	°C
T <sub>stg</sub>	Storage temperature	-65	150	°C

- (1) Operation outside the *Absolute Maximum Ratings* may cause permanent device damage. *Absolute Maximum Ratings* do not imply functional operation of the device at these or any other conditions beyond those listed under *Recommended Operating Conditions*. If used outside the *Recommended Operating Conditions* but within the *Absolute Maximum Ratings*, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.
- (2) The maximum power dissipation is a function of T<sub>J</sub>(MAX), θ<sub>JA</sub>. The maximum allowable power dissipation at any ambient temperature is PD = (T<sub>J</sub>(MAX) - T<sub>A</sub>) / θ<sub>JA</sub>. All numbers apply for packages soldered directly onto a printed circuit board (PCB).

### 5.2 ESD Ratings

			VALUE	UNIT
<b>DCK (SC70) PACKAGE</b>				
V <sub>(ESD)</sub>	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	V
		Charged device model (CDM) per JEDEC specification JESD22-C101 <sup>(2)</sup>	±1000	
		Machine model	±200	
<b>P (PDIP) PACKAGE</b>				
V <sub>(ESD)</sub>	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	V
		Charged device model (CDM) per ANSI/ESDA/JEDEC JS-002 <sup>(2)</sup>	±1000	
		Machine model	±200	

- (1) JEDEC document JEP155 states that 500V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250V CDM allows safe manufacturing with a standard ESD control process.

### 5.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	NOM	MAX	UNIT
V <sub>S</sub>	Supply voltage, V <sub>S</sub> = (V <sup>+</sup> ) - (V <sup>-</sup> )	1.6		5.5	V
T <sub>A</sub>	Temperature <sup>(2)</sup>	-40		125	°C

- (1) *Absolute Maximum Ratings* indicate limits beyond which damage may occur. *Recommended Operating Conditions* indicate conditions for which the device is intended to be functional, but specific performance is not tested. For tested specifications and test conditions, see *Electrical Characteristics*.
- (2) The maximum power dissipation is a function of T<sub>J</sub>(MAX), θ<sub>JA</sub>. The maximum allowable power dissipation at any ambient temperature is PD = (T<sub>J</sub>(MAX) - T<sub>A</sub>) / θ<sub>JA</sub>. All numbers apply for packages soldered directly onto a PCB.

## 5.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		LPV521		UNIT
		DCK (SC70)	P (PDIP)	
		5 PINS	8 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance <sup>(2)</sup>	456	102.3	°C/W
$R_{\theta JC(top)}$	Junction-to-case(top) thermal resistance	53.9	81.2	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	48.9	64.9	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	6.6	47.6	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	48.3	64.1	°C/W
$R_{\theta JC(bot)}$	Junction-to-case(bottom) thermal resistance	N/A	N/A	°C/W

- (1) For information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.  
(2) The maximum power dissipation is a function of  $T_J(MAX)$ ,  $\theta_{JA}$ . The maximum allowable power dissipation at any ambient temperature is  $PD = (T_J(MAX) - T_A) / \theta_{JA}$ . All numbers apply for packages soldered directly onto a PCB.

## 5.5 Electrical Characteristics

at  $T_A = 25^\circ\text{C}$ ,  $V^+ = 1.8\text{V}$ ,  $3.3\text{V}$ , and  $5\text{V}$ ,  $V^- = 0\text{V}$ ,  $V_{CM} = V_O = V_S / 2$ , and  $R_L > 1\text{M}\Omega$  (unless otherwise noted)<sup>(1)</sup>

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
<b>OFFSET VOLTAGE</b>							
$V_{OS}$	Input offset voltage	$V_{CM} = V^- + 0.3\text{V}$		-1	0.1	1	mV
			$T_A = -40^\circ\text{C to } +125^\circ\text{C}$	-1.23		1.23	
		$V_{CM} = V^+ - 0.3\text{V}$		-1	0.1	1	
			$T_A = -40^\circ\text{C to } +125^\circ\text{C}$	-1.23		1.23	
$TCV_{OS}$	Input offset voltage drift <sup>(2)</sup>	$T_A = -40^\circ\text{C to } +125^\circ\text{C}$	$V^+ = 1.8\text{V}, 3.3\text{V}$		$\pm 0.4$		$\mu\text{V}/^\circ\text{C}$
			$V^+ = 5\text{V}$	-3		3	
				-3.5		3.5	
PSRR	Power-supply rejection ratio	$1.6\text{V} \leq V^+ \leq 5.5\text{V}$ , $V_{CM} = 0.3\text{V}$		85	109		dB
			$T_A = -40^\circ\text{C to } +125^\circ\text{C}$	76			
<b>INPUT BIAS CURRENT</b>							
$I_{BIAS}$	Input bias current	$T_A = -40^\circ\text{C to } +125^\circ\text{C}$	$V^+ = 1.8\text{V}, 3.3\text{V}$	-1	0.01	1	pA
			$V^+ = 5\text{V}$	-1	0.04	1	
				-50		+50	
$I_{OS}$	Input offset current	$T_A = -40^\circ\text{C to } +125^\circ\text{C}$	$V^+ = 1.8\text{V}$		10		fA
			$V^+ = 3.3\text{V}$		20		
			$V^+ = 5\text{V}$		60		
<b>NOISE</b>							
	Input-referred voltage noise	$T_A = -40^\circ\text{C to } +125^\circ\text{C}$	$V^+ = 1.8\text{V}$		24		$\mu\text{V}_{PP}$
			$V^+ = 3.3\text{V}, 5\text{V}$		22		
$e_n$	Input-referred voltage noise density	$f = 100\text{Hz}$	$V^+ = 1.8\text{V}$		265		$\text{nV}/\sqrt{\text{Hz}}$
			$V^+ = 3.3\text{V}$		259		
			$V^+ = 5\text{V}$		255		
$i_n$	Input-referred current noise	$f = 100\text{Hz}$			100		$\text{fA}/\sqrt{\text{Hz}}$

## 5.5 Electrical Characteristics (続き)

at  $T_A = 25^\circ\text{C}$ ,  $V^+ = 1.8\text{V}$ ,  $3.3\text{V}$ , and  $5\text{V}$ ,  $V^- = 0\text{V}$ ,  $V_{CM} = V_O = V_S / 2$ , and  $R_L > 1\text{M}\Omega$  (unless otherwise noted)<sup>(1)</sup>

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
<b>INPUT VOLTAGE</b>							
CMRR	Common-mode rejection ratio	$V^- \leq V_{CM} \leq V^+$	$V^+ = 1.8\text{V}$	66	92		dB
			$V^+ = 1.8\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	60			
			$V^+ = 3.3\text{V}$	72	97		
			$V^+ = 3.3\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	70			
			$V^+ = 5\text{V}$	75	102		
			$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	74			
		$V^- \leq V_{CM} \leq V^+ - 1.1\text{V}$	$V^+ = 1.8\text{V}$	75	101		
			$V^+ = 1.8\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	74			
			$V^+ = 3.3\text{V}$	78	106		
			$V^+ = 3.3\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	75			
			$V^+ = 5\text{V}$	84	108		
			$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	80			
		$V^+ - 0.6\text{V} \leq V_{CM} \leq V^+$	$V^+ = 1.8\text{V}$	75	120		
			$V^+ = 1.8\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	53			
			$V^+ = 3.3\text{V}$	77	121		
$V^+ = 3.3\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	76						
$V^+ = 5\text{V}$	77		115				
$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	76						
CMVR	Common-mode voltage range	$V^+ = 1.8\text{V}$ , CMRR $\geq 67\text{dB}$ , $V^+ = 3.3\text{V}$ , CMRR $\geq 72\text{dB}$ , $V^+ = 5\text{V}$ , CMRR $\geq 75\text{dB}$		$(V^-) - 0.1$		$(V^+) + 0.1$	V
		$T_A = -40^\circ\text{C to } +125^\circ\text{C}$ , $V^+ = 1.8\text{V}$ , CMRR $\geq 60\text{dB}$ , $V^+ = 3.3\text{V}$ , CMRR $\geq 70\text{dB}$ , $V^+ = 5\text{V}$ , CMRR $\geq 74\text{dB}$		$(V^-)$		$(V^+)$	V
<b>OPEN-LOOP GAIN</b>							
$A_{VOL}$	Large-signal voltage gain	$V^- + 0.5\text{V} \leq V_O \leq V^+ - 0.5\text{V}$ , $R_L = 100\text{k}\Omega$ to $V^+/2$	$V^+ = 1.8\text{V}$	74	125		dB
			$V^+ = 1.8\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	73			
			$V^+ = 3.3\text{V}$	82	120		
			$V^+ = 3.3\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	76			
			$V^+ = 5\text{V}$	84	132		
			$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	76			
<b>FREQUENCY RESPONSE</b>							
GBW	Gain bandwidth product	$C_L = 20\text{pF}$ , $R_L = 100\text{k}\Omega$	$V^+ = 1.8\text{V}$		6.1		kHz
			$V^+ = 3.3\text{V}, 5\text{V}$		6.2		
SR	Slew rate	Falling edge, $A_V = +1$ , $V_{IN} = V^+$ to $V^-$	$V^+ = 1.8\text{V}$		2.9		V/ms
			$V^+ = 3.3\text{V}$		2.9		
			$V^+ = 5\text{V}$	1.1	2.7		
			$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	1.2			
		Rising edge, $A_V = +1$ , $V_{IN} = V^-$ to $V^+$	$V^+ = 1.8\text{V}$		2.3		
			$V^+ = 3.3\text{V}$		2.5		
			$V^+ = 5\text{V}$	1.1	2.4		
			$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	1.2			
$\theta_m$	Phase margin	$C_L = 20\text{pF}$ , $R_L = 100\text{k}\Omega$	$V^+ = 1.8\text{V}$		72		deg
			$V^+ = 3.3\text{V}, 5\text{V}$		73		
$G_m$	Gain margin	$C_L = 20\text{pF}$ , $R_L = 100\text{k}\Omega$	$V^+ = 1.8\text{V}, 3.3\text{V}$		19		dB
			$V^+ = 5\text{V}$		20		

### 5.5 Electrical Characteristics (続き)

at  $T_A = 25^\circ\text{C}$ ,  $V^+ = 1.8\text{V}, 3.3\text{V}, \text{ and } 5\text{V}$ ,  $V^- = 0\text{V}$ ,  $V_{\text{CM}} = V_O = V_S / 2$ , and  $R_L > 1\text{ M}\Omega$  (unless otherwise noted)<sup>(1)</sup>

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
<b>OUTPUT</b>							
$V_O$	Output voltage	Swing from positive rail, $R_L = 100\text{k}\Omega$ to $V^+/2$ , $V_{\text{IN}}(\text{diff}) = 100\text{mV}$	$V^+ = 1.8\text{V}$		2	50	mV
			$V^+ = 1.8\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$			50	
			$V^+ = 3.3\text{V}$		3	50	
			$V^+ = 3.3\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$			50	
			$V^+ = 5\text{V}$		3	50	
			$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$			50	
		Swing from negative rail, $R_L = 100\text{k}\Omega$ to $V^+/2$ , $V_{\text{IN}}(\text{diff}) = -100\text{mV}$	$V^+ = 1.8\text{V}$		2	50	
			$V^+ = 1.8\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$			50	
			$V^+ = 3.3\text{V}$		2	50	
			$V^+ = 3.3\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$			50	
			$V^+ = 5\text{V}$		3	50	
			$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$			50	
$I_O$	Output current <sup>(3)</sup>	Sourcing, $V_O$ to $V^-$ , $V_{\text{IN}}(\text{diff}) = 100\text{mV}$	$V^+ = 1.8\text{V}$	1	3		mA
			$V^+ = 1.8\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	0.5			
			$V^+ = 3.3\text{V}$	5	11		
			$V^+ = 3.3\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	4			
			$V^+ = 5\text{V}$	15	23		
			$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	8			
		Sinking, $V_O$ to $V^+$ , $V_{\text{IN}}(\text{diff}) = -100\text{mV}$	$V^+ = 1.8\text{V}$	1	3		
			$V^+ = 1.8\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	0.5			
			$V^+ = 3.3\text{V}$	5	12		
			$V^+ = 3.3\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	4			
			$V^+ = 5\text{V}$	15	22		
			$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$	8			

## 5.5 Electrical Characteristics (続き)

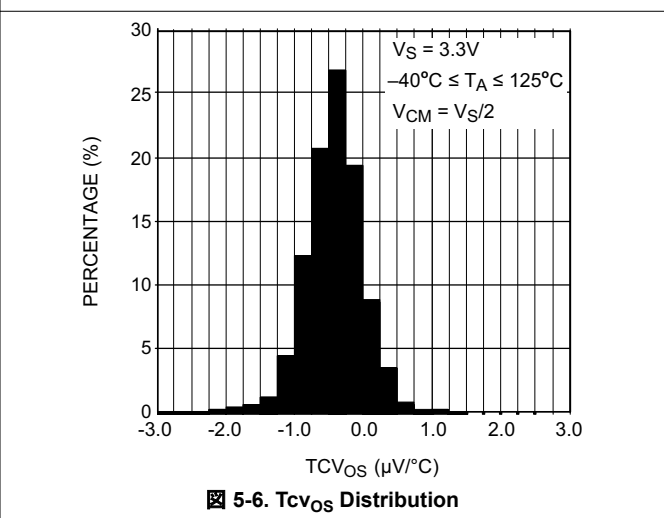
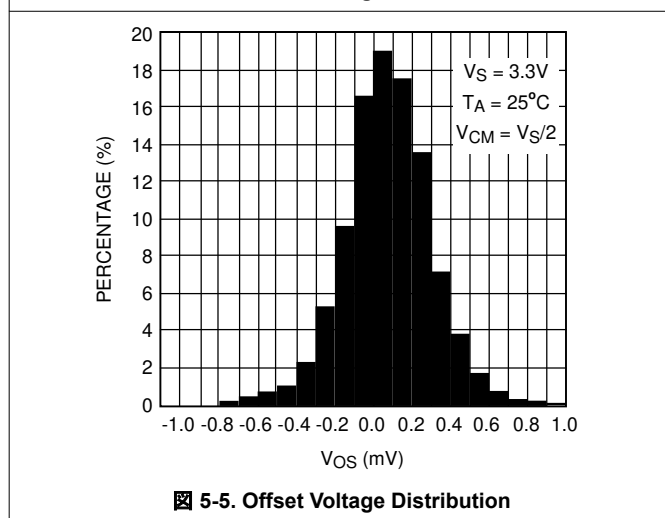
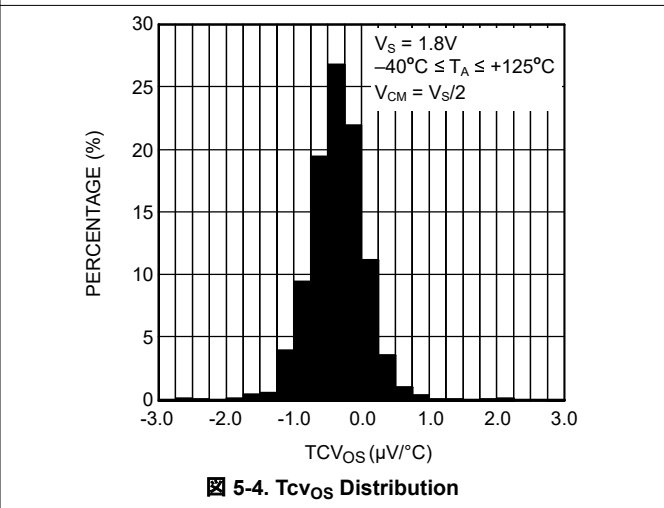
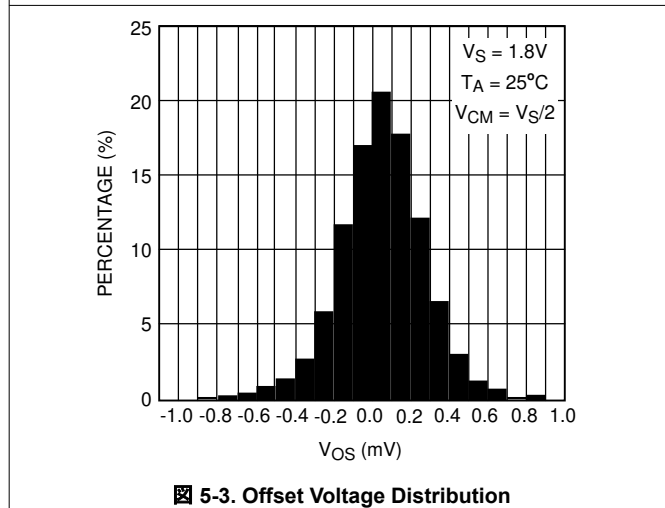
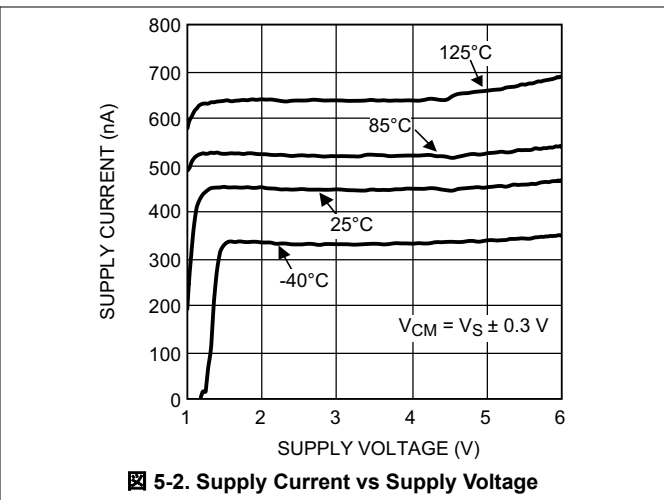
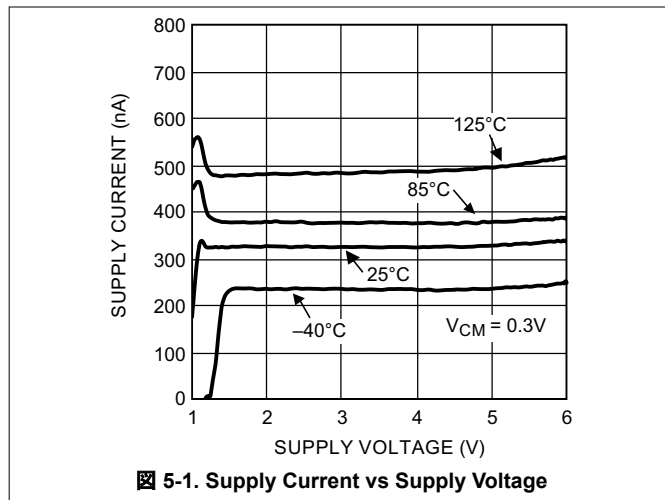
at  $T_A = 25^\circ\text{C}$ ,  $V^+ = 1.8\text{V}$ ,  $3.3\text{V}$ , and  $5\text{V}$ ,  $V^- = 0\text{V}$ ,  $V_{\text{CM}} = V_O = V_S / 2$ , and  $R_L > 1\text{M}\Omega$  (unless otherwise noted)<sup>(1)</sup>

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT	
<b>POWER SUPPLY</b>								
$I_S$	Supply current	$V_{\text{CM}} = V^- + 0.3\text{V}$	$V^+ = 1.8\text{V}$		345	400	nA	
			$V^+ = 1.8\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$				580	nA
			$V^+ = 3.3\text{V}$		346	400	nA	
			$V^+ = 3.3\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$				600	nA
			$V^+ = 5\text{V}$		351	400	nA	
			$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$				620	nA
		$V_{\text{CM}} = V^+ - 0.3\text{V}$	$V^+ = 1.8\text{V}$		472	600	nA	
			$V^+ = 1.8\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$				850	nA
			$V^+ = 3.3\text{V}$		471	600	nA	
			$V^+ = 3.3\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$				860	nA
			$V^+ = 5\text{V}$		475	600	nA	
			$V^+ = 5\text{V}, T_A = -40^\circ\text{C to } +125^\circ\text{C}$				870	nA
<b>NOISE IMMUNITY</b>								
EMIRR	EMI rejection ratio, IN+ and IN- <sup>(4)</sup>	$V^+ = 5\text{V}$ , $V_{\text{RF\_PEAK}} = 100\text{mV}_P (-20\text{dB}_P)$	$f = 400\text{MHz}$		121		dB	
			$f = 900\text{MHz}$		121			
			$f = 1800\text{MHz}$		124			
			$f = 2400\text{MHz}$		142			

- (1) *Electrical Characteristics* values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that  $T_J = T_A$ . No min and max specifications of parametric performance are indicated in the electrical tables under conditions of internal self-heating where  $T_J > T_A$ . *Absolute Maximum Ratings* indicate junction temperature limits beyond which the device may be permanently degraded, either mechanically or electrically.
- (2) The offset voltage average drift is determined by dividing the change in  $V_{\text{OS}}$  at the temperature extremes by the total temperature change.
- (3) The short circuit test is a momentary open-loop test.
- (4) The EMI rejection ratio is defined as  $\text{EMIRR} = 20\log(V_{\text{RF\_PEAK}}/\Delta V_{\text{OS}})$ .

## 5.6 Typical Characteristics

at  $T_J = 25^\circ\text{C}$  (unless otherwise specified)





## 5.6 Typical Characteristics (continued)

at  $T_J = 25^\circ\text{C}$  (unless otherwise specified)

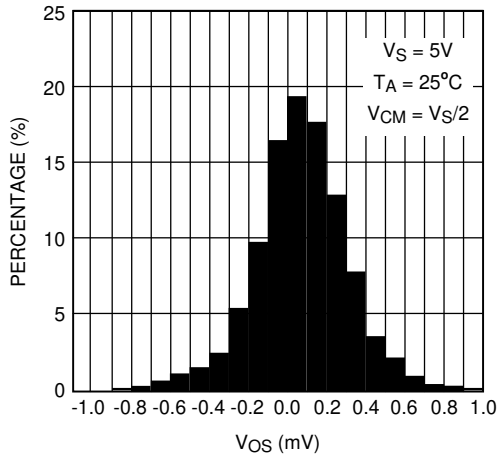


図 5-7. Offset Voltage Distribution

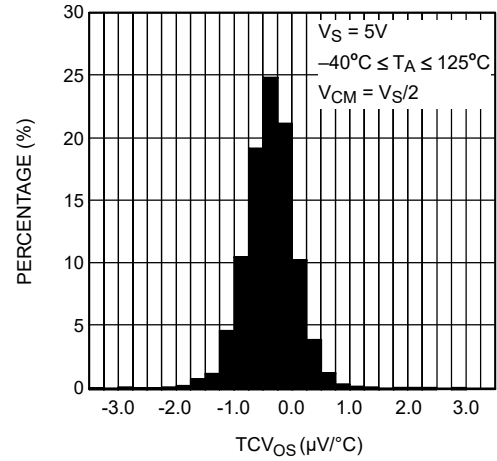


図 5-8. TcvOss Distribution

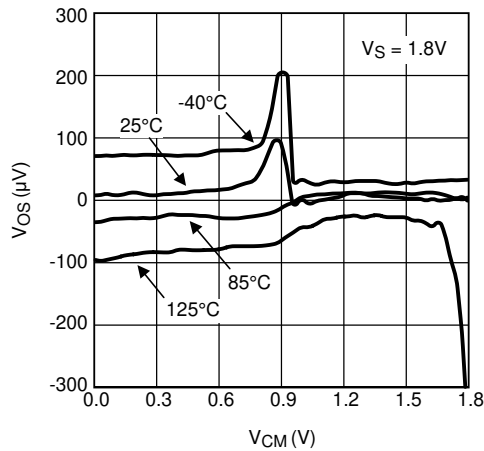


図 5-9. Input Offset Voltage vs Input Common Mode

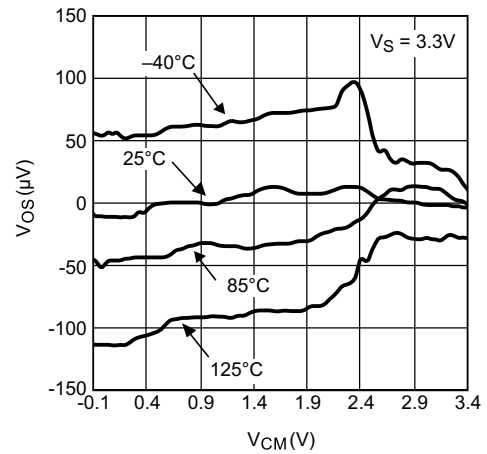


図 5-10. Input Offset Voltage vs Input Common Mode

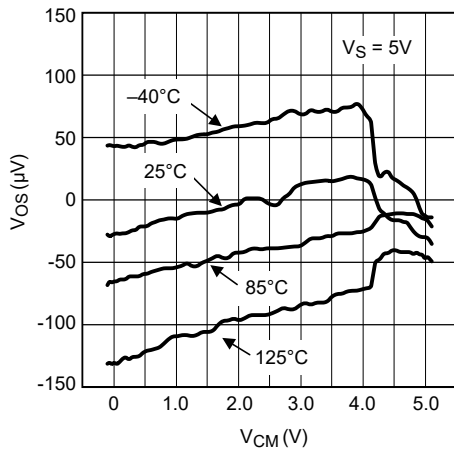


図 5-11. Input Offset Voltage vs Input Common Mode

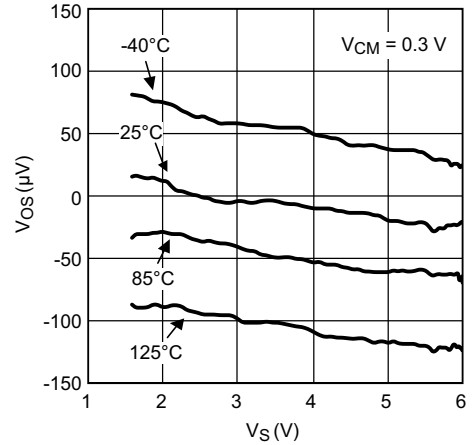


図 5-12. Input Offset Voltage vs Supply Voltage

### 5.6 Typical Characteristics (continued)

at  $T_J = 25^\circ\text{C}$  (unless otherwise specified)

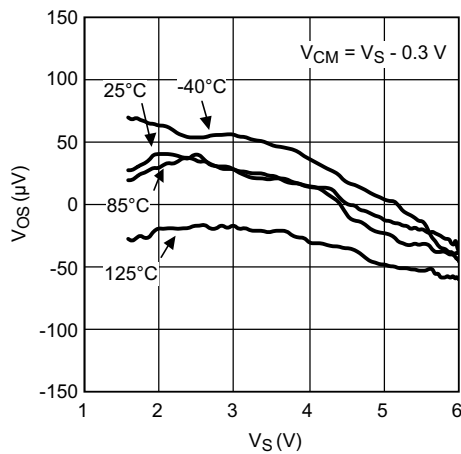


图 5-13. Input Offset Voltage vs Supply Voltage

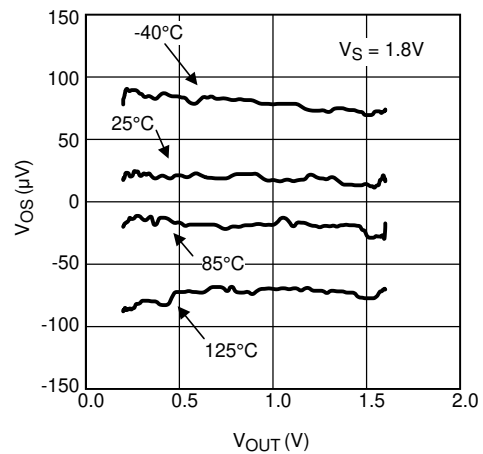


图 5-14. Input Offset Voltage vs Output Voltage

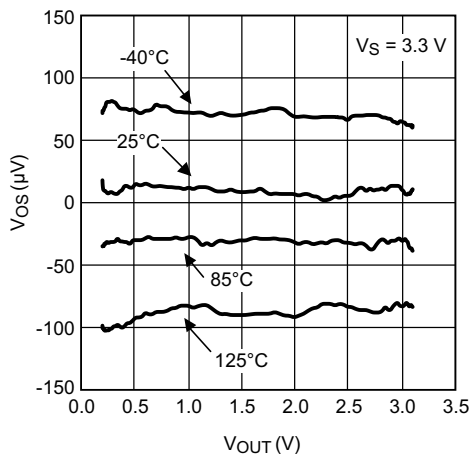


图 5-15. Input Offset Voltage vs Output Voltage

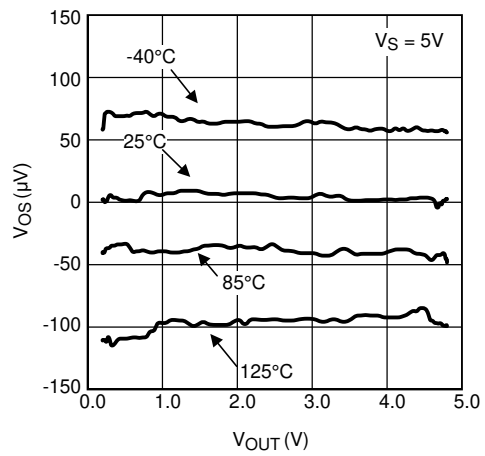


图 5-16. Input Offset Voltage vs Output Voltage

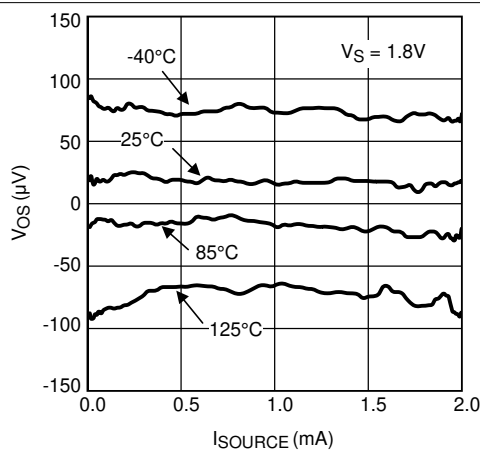


图 5-17. Input Offset Voltage vs Sourcing Current

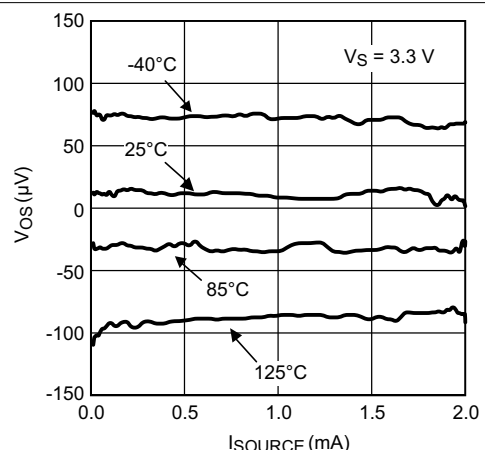


图 5-18. Input Offset Voltage vs Sourcing Current

## 5.6 Typical Characteristics (continued)

at  $T_J = 25^\circ\text{C}$  (unless otherwise specified)

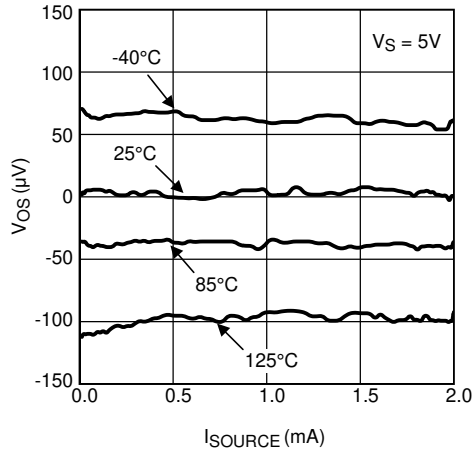


图 5-19. Input Offset Voltage vs Sourcing Current

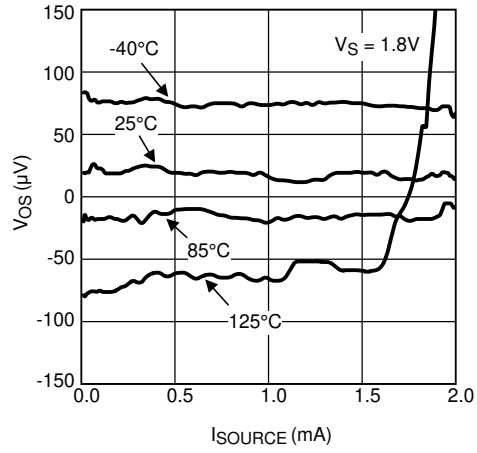


图 5-20. Input Offset Voltage vs Sinking Current

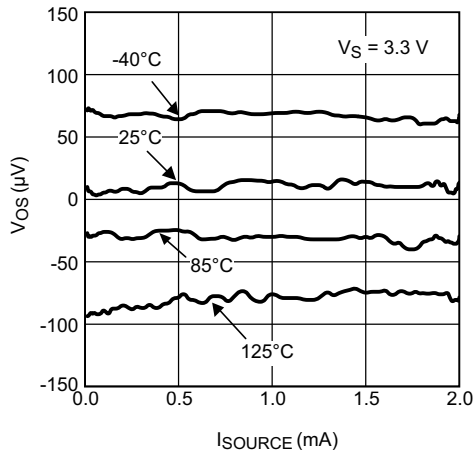


图 5-21. Input Offset Voltage vs Sinking Current

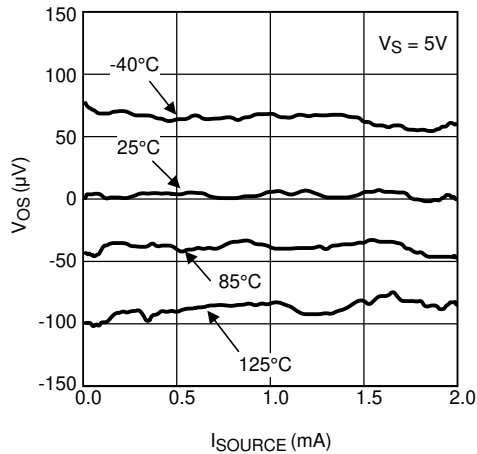


图 5-22. Input Offset Voltage vs Sinking Current

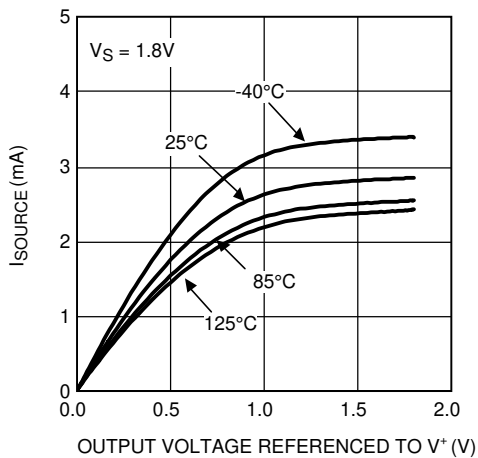


图 5-23. Sourcing Current vs Output Voltage

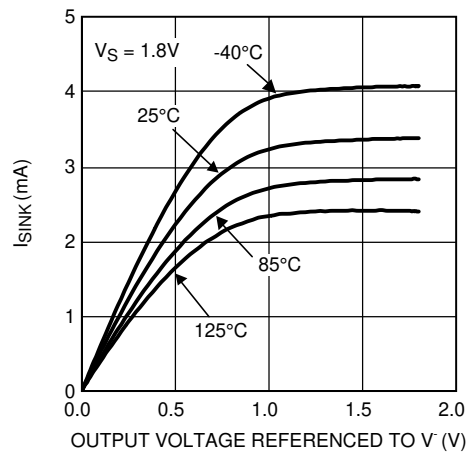
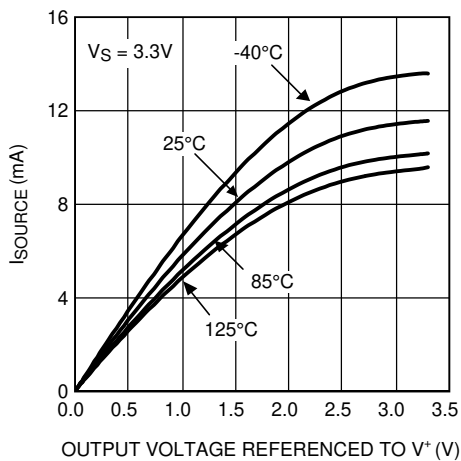


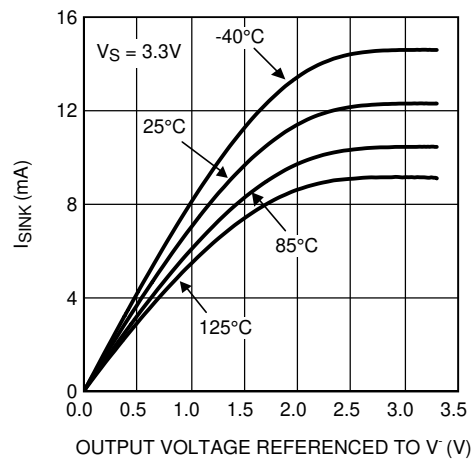
图 5-24. Sinking Current vs Output Voltage

## 5.6 Typical Characteristics (continued)

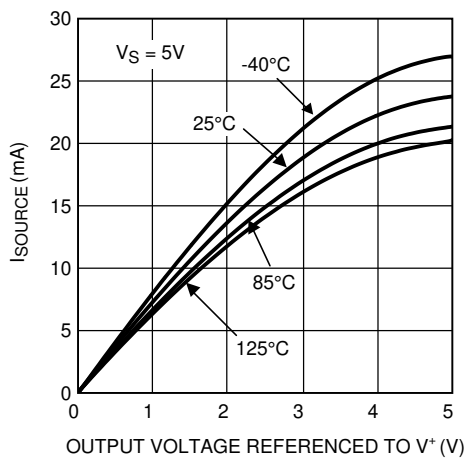
at  $T_J = 25^\circ\text{C}$  (unless otherwise specified)



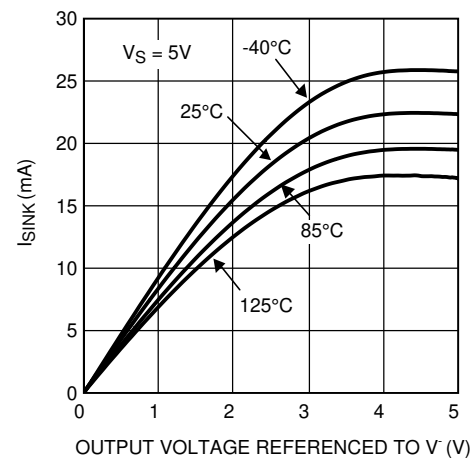
5-25. Sourcing Current vs Output Voltage



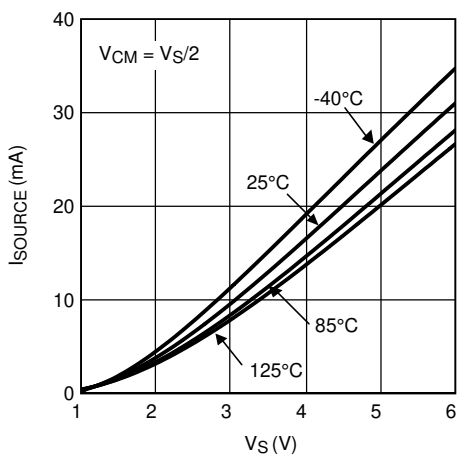
5-26. Sinking Current vs Output Voltage



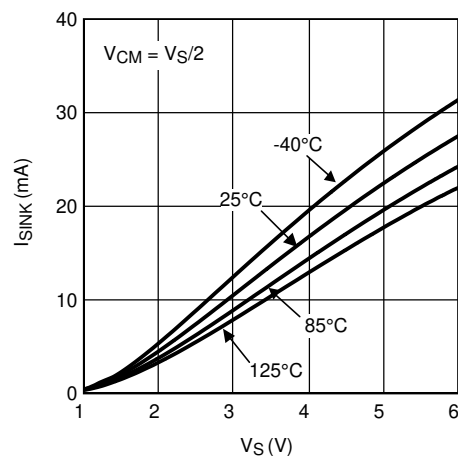
5-27. Sourcing Current vs Output Voltage



5-28. Sinking Current vs Output Voltage



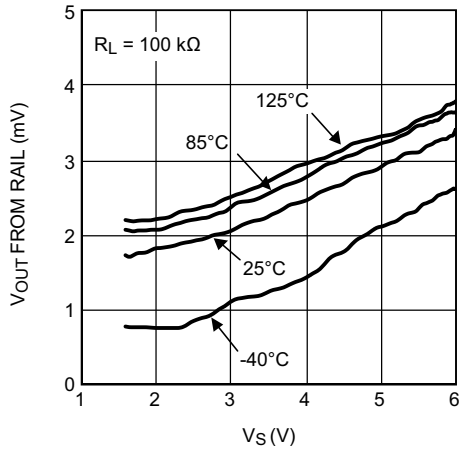
5-29. Sourcing Current vs Supply Voltage



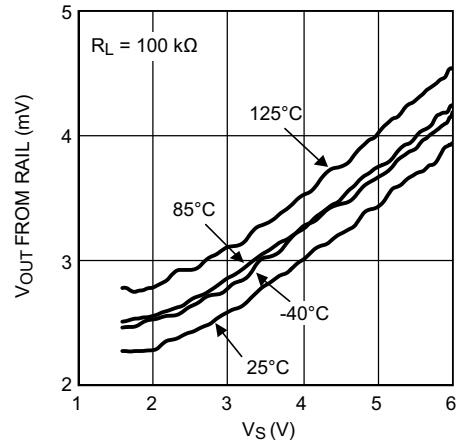
5-30. Sinking Current vs Supply Voltage

## 5.6 Typical Characteristics (continued)

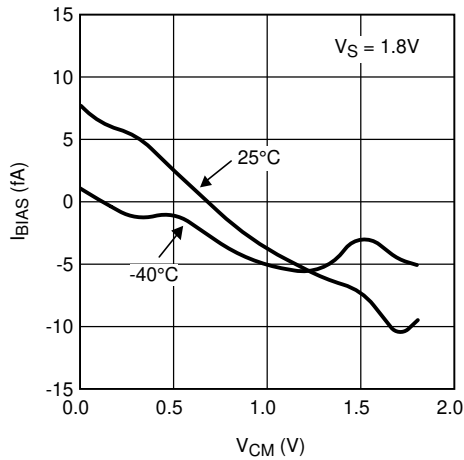
at  $T_J = 25^\circ\text{C}$  (unless otherwise specified)



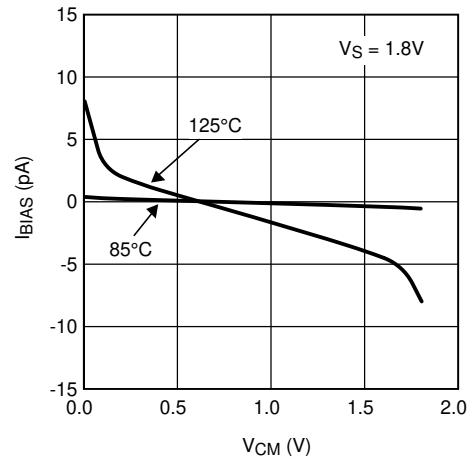
5-31. Output Swing High vs Supply Voltage



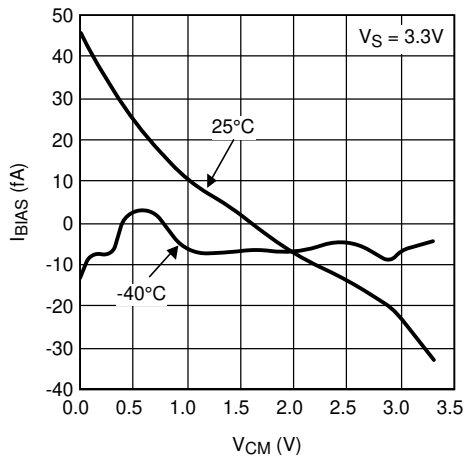
5-32. Output Swing Low vs Supply Voltage



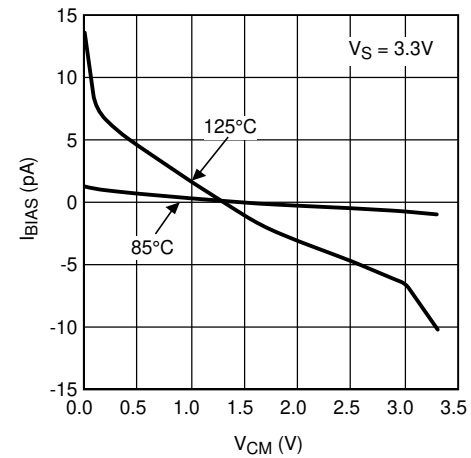
5-33. Input Bias Current vs Common Mode Voltage



5-34. Input Bias Current vs Common Mode Voltage



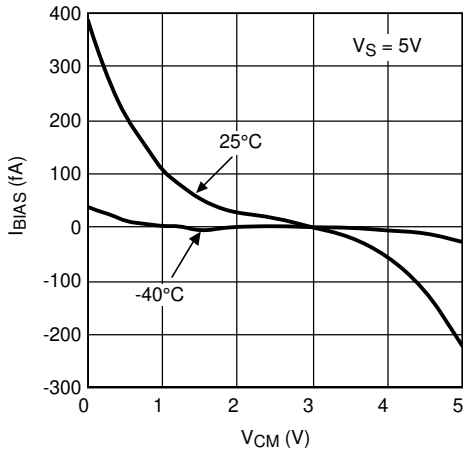
5-35. Input Bias Current vs Common Mode Voltage



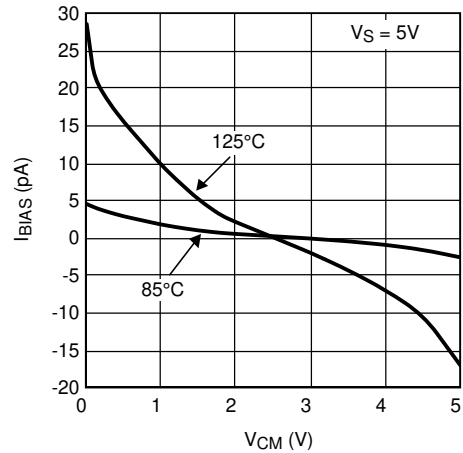
5-36. Input Bias Current vs Common Mode Voltage

### 5.6 Typical Characteristics (continued)

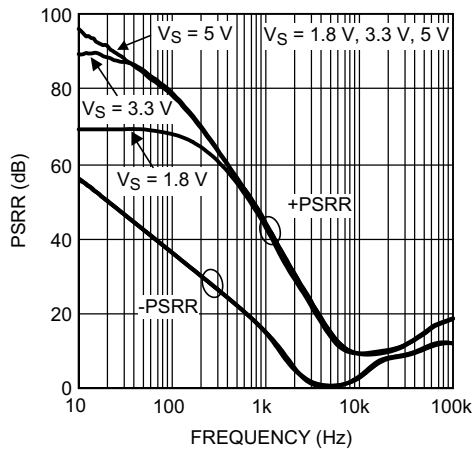
at  $T_J = 25^\circ\text{C}$  (unless otherwise specified)



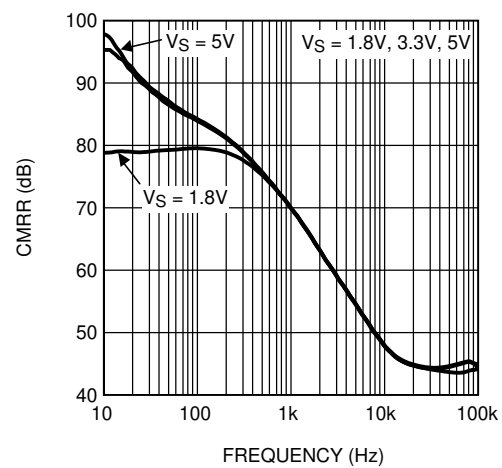
5-37. Input Bias Current vs Common Mode Voltage



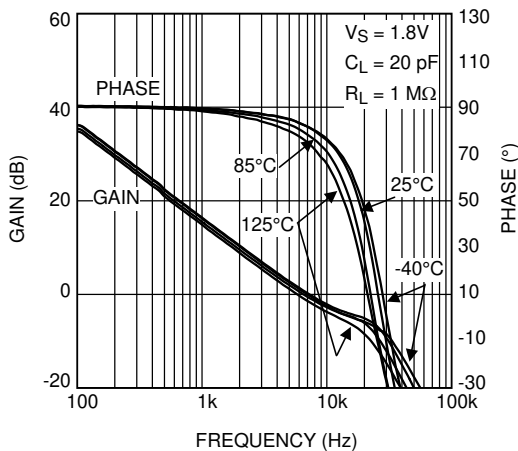
5-38. Input Bias Current vs Common Mode Voltage



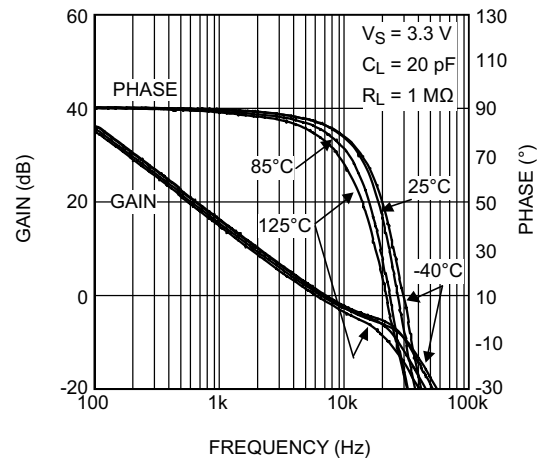
5-39. PSRR vs Frequency



5-40. CMRR vs Frequency



5-41. Frequency Response vs Temperature



5-42. Frequency Response vs Temperature

### 5.6 Typical Characteristics (continued)

at  $T_J = 25^\circ\text{C}$  (unless otherwise specified)

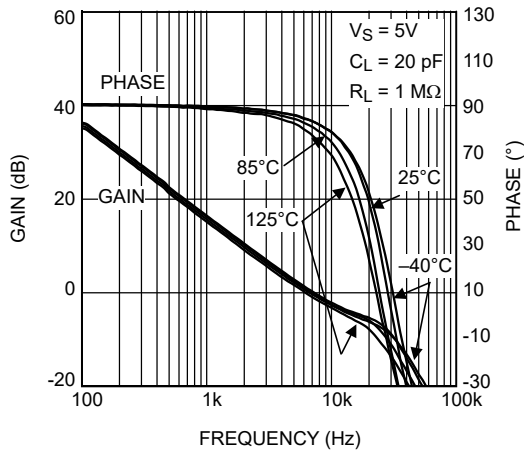


図 5-43. Frequency Response vs Temperature

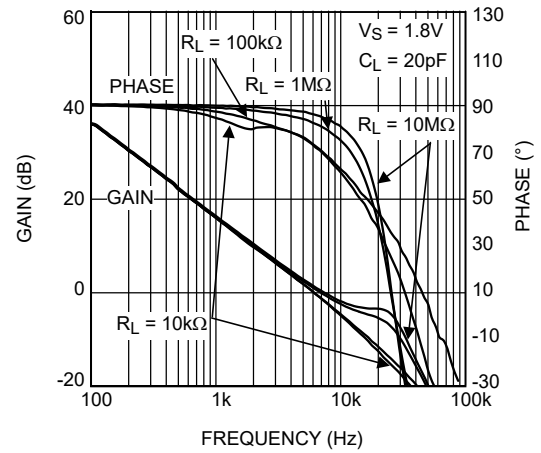


図 5-44. Frequency Response vs  $R_L$

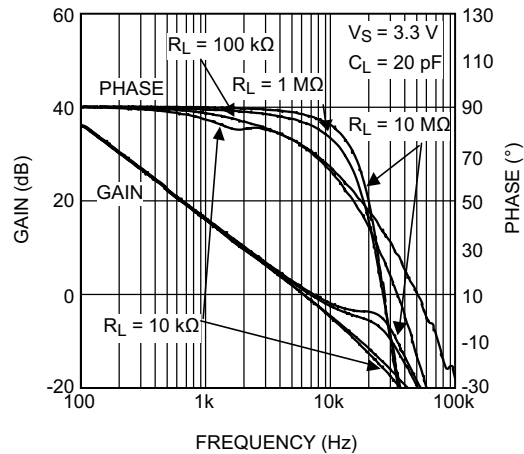


図 5-45. Frequency Response vs  $R_L$

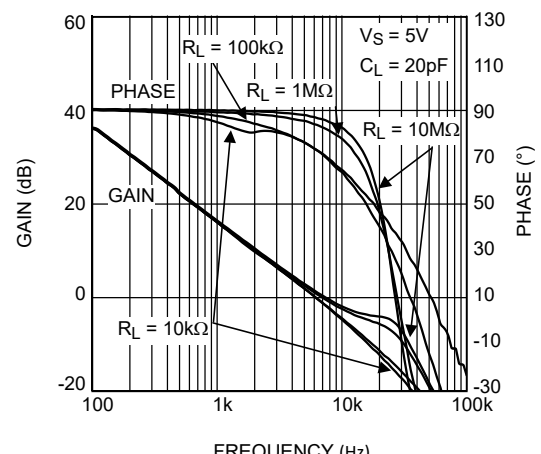


図 5-46. Frequency Response vs  $R_L$

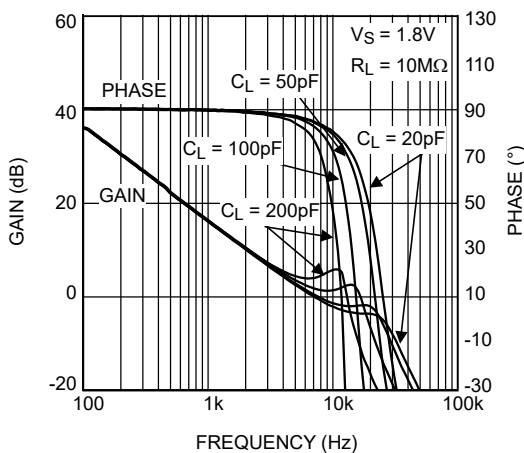


図 5-47. Frequency Response vs  $C_L$

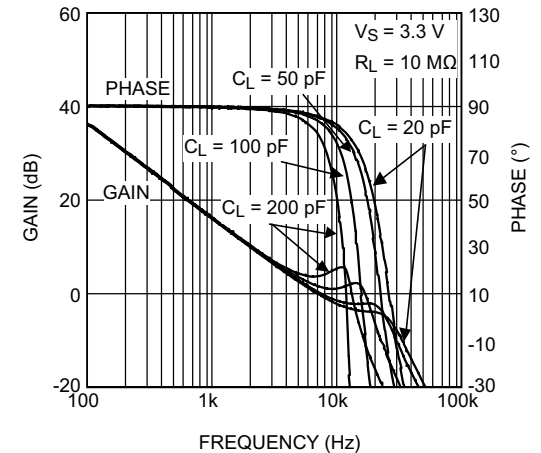


図 5-48. Frequency Response vs  $C_L$

### 5.6 Typical Characteristics (continued)

at  $T_J = 25^\circ\text{C}$  (unless otherwise specified)

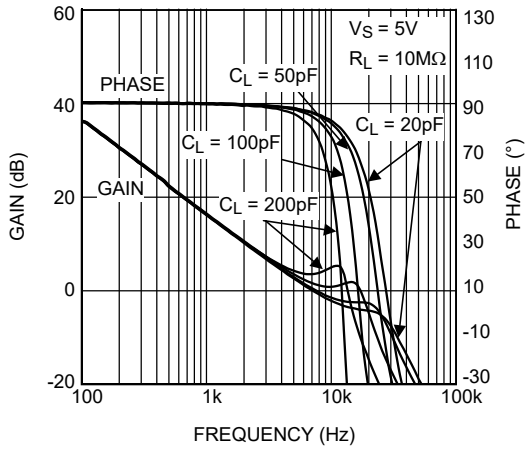


Figure 5-49. Frequency Response vs  $C_L$

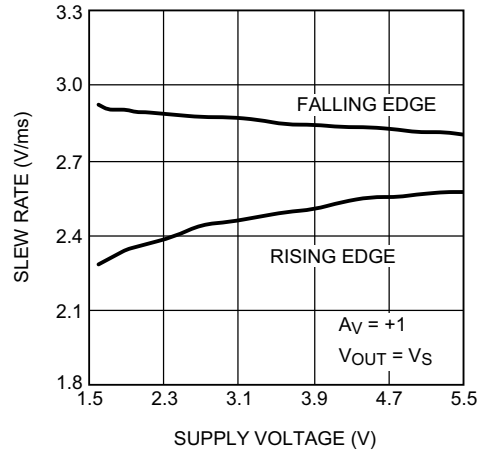


Figure 5-50. Slew Rate vs Supply Voltage

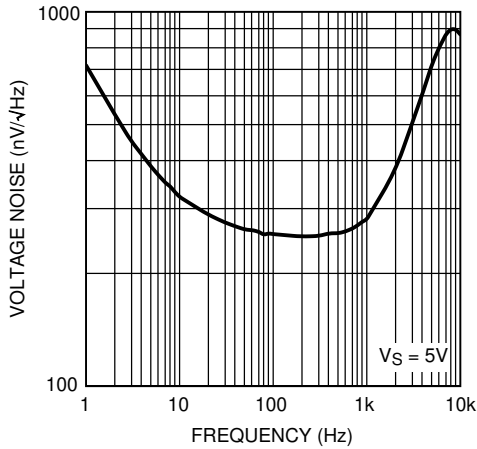


Figure 5-51. Voltage Noise vs Frequency

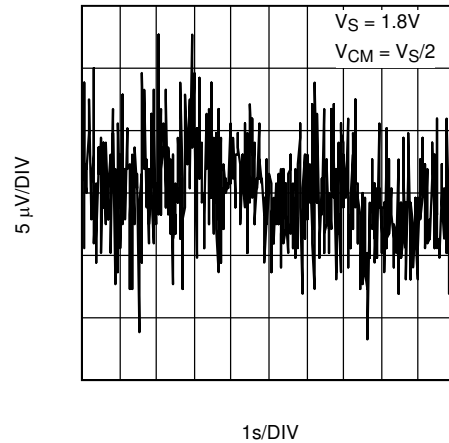


Figure 5-52. 0.1-Hz to 10-Hz Time Domain Voltage Noise

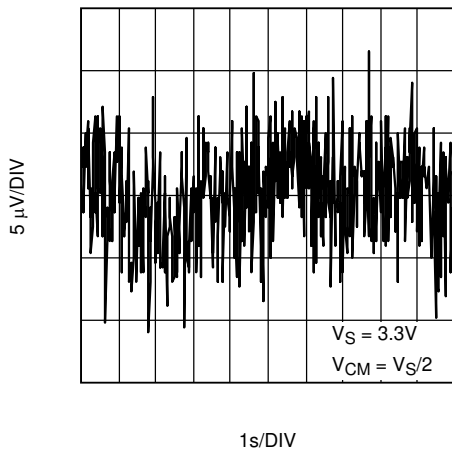


Figure 5-53. 0.1-Hz to 10-Hz Time Domain Voltage Noise

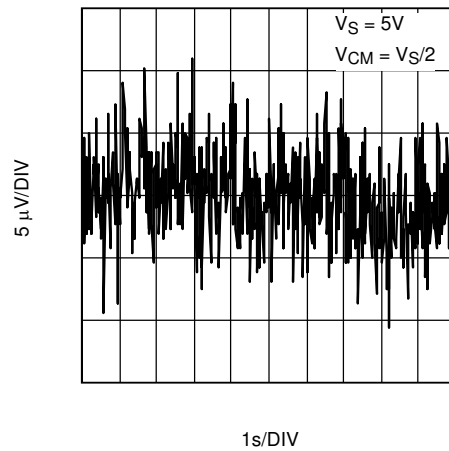
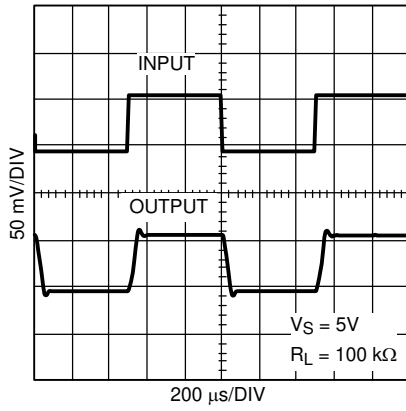


Figure 5-54. 0.1-Hz to 10-Hz Time Domain Voltage Noise

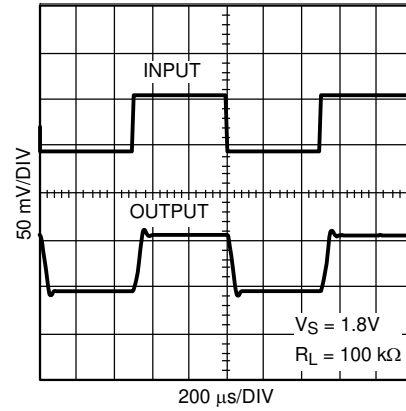


## 5.6 Typical Characteristics (continued)

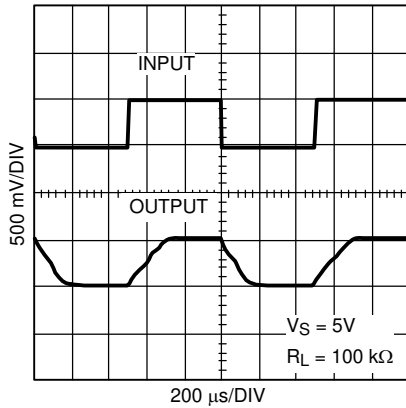
at  $T_J = 25^\circ\text{C}$  (unless otherwise specified)



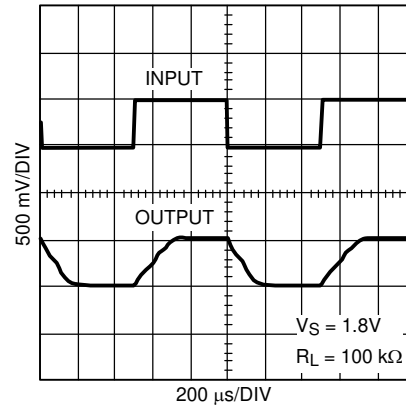
5-55. Small-Signal Pulse Response



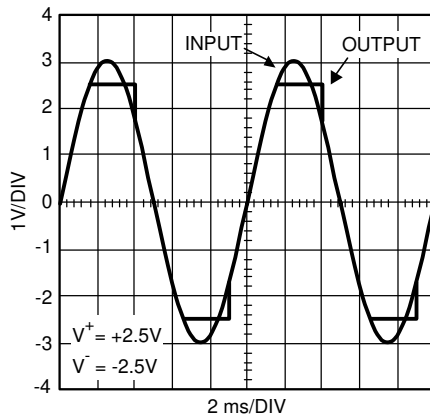
5-56. Small-Signal Pulse Response



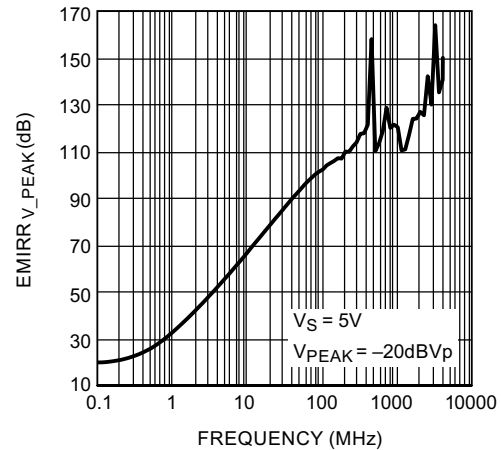
5-57. Large-Signal Pulse Response



5-58. Large-Signal Pulse Response



5-59. Overload Recovery Waveform



5-60. EMIRR vs Frequency

## 6 Detailed Description

### 6.1 Overview

The LPV521 is fabricated with Texas Instruments' state-of-the-art VIP50 process. This proprietary process dramatically improves the performance of Texas Instruments' low-power and low-voltage operational amplifiers. The following sections showcase the advantages of the VIP50 process and highlight circuits that enable ultra-low power consumption.

### 6.2 Functional Block Diagram

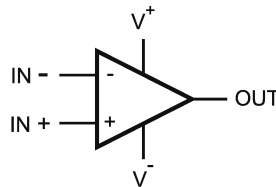


図 6-1. Block Diagram

### 6.3 Feature Description

The amplifier differential inputs consist of a noninverting input (+IN) and an inverting input (–IN). The amplifier amplifies only the difference in voltage between the two inputs, which is called the differential input voltage. The output voltage of the op-amp  $V_{OUT}$  is given by 式 1:

$$V_{OUT} = A_{OL} (IN^+ - IN^-) \quad (1)$$

where  $A_{OL}$  is the open-loop gain of the amplifier, typically around 132dB (4,000,000 ×, or 0.25μV/V).

### 6.4 Device Functional Modes

#### 6.4.1 Input Stage

The LPV521 has a rail-to-rail input that provides more flexibility for the system designer. Rail-to-rail input is achieved by using in parallel, one PMOS differential pair and one NMOS differential pair. When the common mode input voltage ( $V_{CM}$ ) is near  $V^+$ , the NMOS pair is on and the PMOS pair is off. When  $V_{CM}$  is near  $V^-$ , the NMOS pair is off and the PMOS pair is on. When  $V_{CM}$  is between  $V^+$  and  $V^-$ , internal logic decides how much current each differential pair get. This special logic maintains stable and low-distortion amplifier operation within the entire common-mode voltage range.

Both input stages have an offset voltage ( $V_{OS}$ ) characteristic; therefore, the offset voltage of the LPV521 becomes a function of  $V_{CM}$ .  $V_{OS}$  has a crossover point at 1.0V less than  $V^+$ . See the *Input Offset Voltage vs Input Common Mode* curves in the *Typical Characteristics*. Take care in situations where the input signal amplitude is comparable to the  $V_{OS}$  value or the design requires high accuracy. In these situations, the input signal must avoid the crossover point. In addition, parameters such as PSRR and CMRR that involve the input offset voltage are also affected by changes in  $V_{CM}$  across the differential-pair transition region.

#### 6.4.2 Output Stage

The LPV521 output voltage swings 3mV from rails at a 3.3V supply, which provides the maximum possible dynamic range at the output. This feature is particularly important when operating on low supply voltages.

The LPV521 maximum output voltage swing defines the maximum swing possible under a particular output load. The LPV521 output swings 50mV from the rail at a 5V supply with an output load of 100kΩ.

## 7 Applications and Implementation

### 注

以下のアプリケーション情報は、TI の製品仕様に含まれるものではなく、TI ではその正確性または完全性を保証いたしません。個々の目的に対する製品の適合性については、お客様の責任で判断していただくこととなります。お客様は自身の設計実装を検証しテストすることで、システムの機能を確認する必要があります。

### 7.1 Application Information

The LPV521 is specified for operation from 1.6V to 5.5V ( $\pm 0.8V$  to  $\pm 2.25V$ ). Many of the specifications apply from  $-40^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$ . The LMV521 features rail-to-rail input and rail-to-rail output swings while consuming only nanowatts of power. Parameters that exhibit significant variance with regard to operating voltage or temperature are presented in [セクション 5.6](#).

#### 7.1.1 Driving Capacitive Load

The LPV521 is internally compensated for stable unity gain operation, with a 6.2kHz, typical gain bandwidth. However, the unity gain follower is the most sensitive configuration to capacitive load. The combination of a capacitive load placed at the output of an amplifier along with the amplifier output impedance creates a phase lag, which reduces the phase margin of the amplifier. If the phase margin is significantly reduced, the response is underdamped, and causes peaking in the transfer. When there is too much peaking, the op amp can start oscillating.

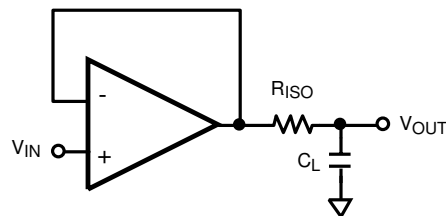


図 7-1. Resistive Isolation of Capacitive Load

To drive heavy capacitive loads, use an isolation resistor,  $R_{ISO}$ , as in [図 7-1](#). By using this isolation resistor, the capacitive load is isolated from the amplifier output. The larger the value of  $R_{ISO}$ , the more stable the amplifier. If the value of  $R_{ISO}$  is sufficiently large, the feedback loop is stable, independent of the value of  $C_L$ . However, larger values of  $R_{ISO}$  result in reduced output swing and reduced output current drive.

[表 7-1](#) shows the recommended minimum  $R_{ISO}$  values for a 5V supply. [図 7-2](#) shows the typical response obtained with the  $C_L = 50\text{pF}$  and  $R_{ISO} = 154\text{k}\Omega$ . The other values of  $R_{ISO}$  in [Table 7-1](#) are chosen to achieve similar dampening at the respective capacitive loads. Notice that for the LPV521 with larger a  $C_L$ , a smaller  $R_{ISO}$  can be used for stability. However, for a given  $C_L$ , a larger  $R_{ISO}$  provides a more damped response. For capacitive loads of 20pF and less, no isolation resistor is needed.

表 7-1. Recommended Minimum  $R_{ISO}$  Values for a 5V Supply

$C_L$	$R_{ISO}$
0pF to 20pF	Not needed
50pF	154k $\Omega$
100pF	118k $\Omega$
500pF	52.3k $\Omega$
1nF	33.2k $\Omega$
5nF	17.4k $\Omega$
10nF	13.3k $\Omega$

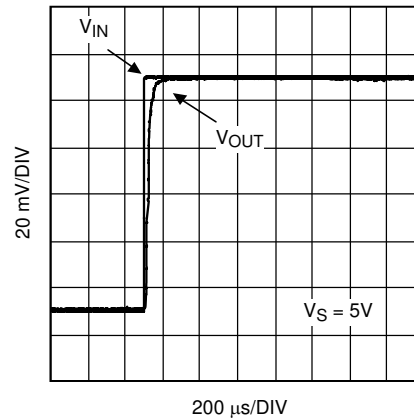


図 7-2. Step Response

### 7.1.2 EMI Suppression

The near-ubiquity of cellular, Bluetooth®, and Wi-Fi® signals and the rapid rise of sensing systems incorporating wireless radios make electromagnetic interference (EMI) an evermore important design consideration for precision signal paths. Though RF signals lie outside the op-amp band, RF carrier switching can modulate the dc offset of the op amp. Also some common RF modulation schemes can induce down-converted components. The added dc offset and the induced signals are amplified with the signal of interest and thus corrupt the measurement. The LPV521 uses on-chip filters to reject these unwanted RF signals at the inputs and power supply pins, thereby preserving the integrity of the precision signal path.

Twisted pair cabling and the active front-end common-mode rejection provide immunity against low-frequency noise (for example, 60Hz or 50Hz mains) but are ineffective against RF interference. Even a few centimeters of printed circuit board (PCB) trace and wiring for sensors located close to the amplifier can pick up significant 1GHz RF. The integrated EMI filters of the LPV521 reduce or eliminate external shielding and filtering requirements, thus increasing system robustness. A larger EMIRR means more rejection of the RF interference. For more information on EMIRR, see the [AN-1698 A Specification for EMI Hardened Operational Amplifiers application report](#).

## 7.2 Typical Applications

### 7.2.1 60Hz Twin T-Notch Filter

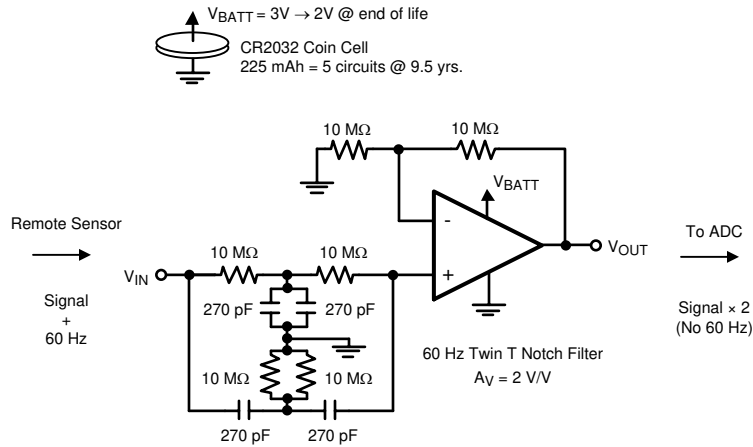


図 7-3. 60Hz Notch Filter

#### 7.2.1.1 Design Requirements

Small signals from transducers in remote and distributed sensing applications commonly suffer strong 60Hz interference from ac power lines. The circuit of 図 7-3 notches out the 60Hz and provides a gain  $A_V = 2$  for the sensor signal represented by a 1kHz sine wave. Similar stages can be cascaded to remove 2nd and 3rd harmonics of 60Hz. Thanks to the nA power consumption of the LPV521, even five such circuits can run for 9.5 years from a small CR2032 lithium cell. These batteries have a nominal voltage of 3V and an end of life voltage of 2V. With an operating voltage from 1.6V to 5.5V, the LPV521 can function over this voltage range.

#### 7.2.1.2 Detailed Design Procedure

The notch frequency is set by  $F_0 = 1 / 2\pi RC$ . To achieve a 60Hz notch, use  $R = 10\text{M}\Omega$  and  $C = 270\text{pF}$ . If eliminating 50Hz noise, which is common in European systems, use  $R = 11.8\text{M}\Omega$  and  $C = 270\text{pF}$ .

The twin T notch filter works by having two separate paths from  $V_{IN}$  to the amplifier input. A low-frequency path through resistors R-R and another separate high-frequency path through capacitors C-C. However, at frequencies around the notch frequency, the two paths have opposing phase angles and the two signals tend to cancel at the amplifier input.

To ensure that the target center frequency is achieved, and to maximize the notch depth (Q factor), balance the filter as much as possible. To obtain circuit balance, while overcoming limitations of available standard resistor and capacitor values, use passives in parallel to achieve the  $2C$  and  $R/2$  circuit requirements for the filter components that connect to ground.

To ensure that passive component values stay as expected, clean the board with alcohol, rinse with deionized water, and air dry. Ensure that the board remains in a relatively low humidity environment to minimize moisture that can increase the conductivity of board components. Also large resistors come with considerable parasitic stray capacitance; the effects can be reduced by cutting out the ground plane below components of concern.

Use Large resistors in the feedback network to minimize battery drain. When designing with large resistors, consider the resistor thermal noise, op-amp current noise, as well as op-amp voltage noise in the noise analysis of the circuit. The noise analysis for the circuit in 図 7-3 can be done over a bandwidth of 5kHz, which takes the conservative approach of overestimating the bandwidth (LPV521 typical  $GBW/A_V$  is less). The total noise at the output is approximately  $800\mu\text{V}_{PP}$ , which is excellent considering the total consumption of the circuit is only 540nA. The dominant noise terms are op-amp voltage noise ( $550\mu\text{V}_{PP}$ ), current noise through the feedback network ( $430\mu\text{V}_{PP}$ ), and current noise through the notch filter network ( $280\mu\text{V}_{PP}$ ). Thus, the total circuit noise is less than  $\frac{1}{2}$  LSB of a 10-bit system with a 2V reference, which is 1mV.

### 7.2.1.3 Application Curve

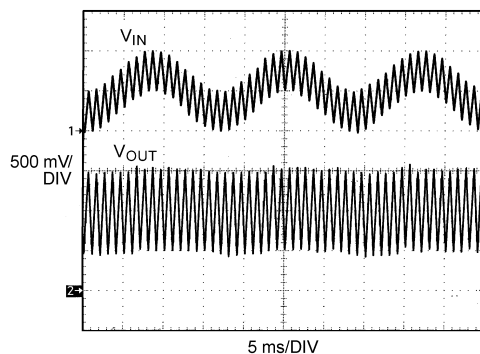


図 7-4. 60Hz Notch Filter Waveform

## 7.2.2 Portable Gas Detection Sensor

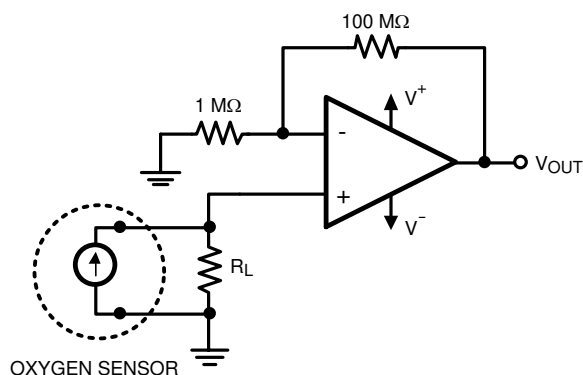


図 7-5. Precision Oxygen Sensor

### 7.2.2.1 Design Requirements

Gas sensors are used in many different industrial and medical applications. Gas sensors generate a current that is proportional to the percentage of a particular gas sensed in an air sample. This current goes through a load resistor and the resulting voltage drop is measured. The LPV521 is an excellent choice for this application because the device draws only 345nA of current and operates on supply voltages down to 1.6V. Depending on the sensed gas and sensitivity of the sensor, the output current can be in the order of tens of microamperes to a few milliamperes. Gas sensor data sheets often specify a recommended load resistor value or suggest a range of load resistors from which to choose.

Oxygen sensors are used when air quality or oxygen delivered to a patient needs to be monitored. Fresh air contains 20.9% oxygen. Air samples containing less than 18% oxygen are considered dangerous. This application detects oxygen in air. Oxygen sensors are also used in industrial applications where the environment must lack oxygen. An example is when food is vacuum packed. There are two main categories: oxygen sensors that sense oxygen when oxygen is abundantly present (for example, in air or near an oxygen tank), and oxygen sensors that detect traces of oxygen in ppm.

### 7.2.2.2 Detailed Design Procedure

Figure 7-5 shows a typical circuit used to amplify the output of an oxygen detector. The oxygen sensor outputs a known current through the load resistor. This value changes with the amount of oxygen present in the air sample. Oxygen sensors usually recommend a particular load resistor value or specify a range of acceptable values for the load resistor. The use of the nanopower LPV521 means minimal power usage by the op amp, and enhanced battery life. With the components shown in Figure 7-5, the circuit consumes less than 0.5µA of current, so that even batteries used in compact portable electronics, with low mAh charge ratings, can last beyond the life of the oxygen sensor. The precision specifications of the LPV521, such as the very low offset voltage, low  $TCV_{OS}$ , low input bias current, high CMRR, and high PSRR are other factors that make the LPV521 a great choice for this application.

### 7.2.2.3 Application Curve

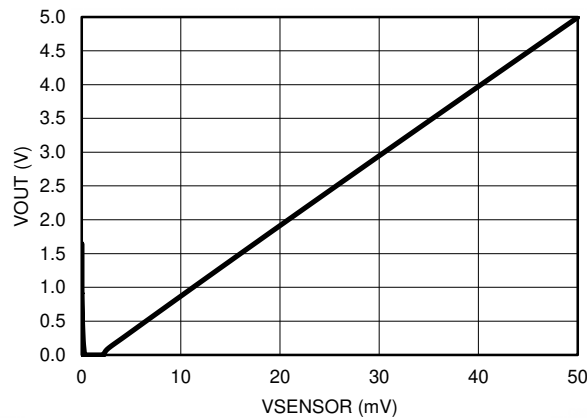


Figure 7-6. Calculated Oxygen Sensor Circuit Output (Single 5V Supply)

### 7.2.3 High-Side Battery Current Sensing

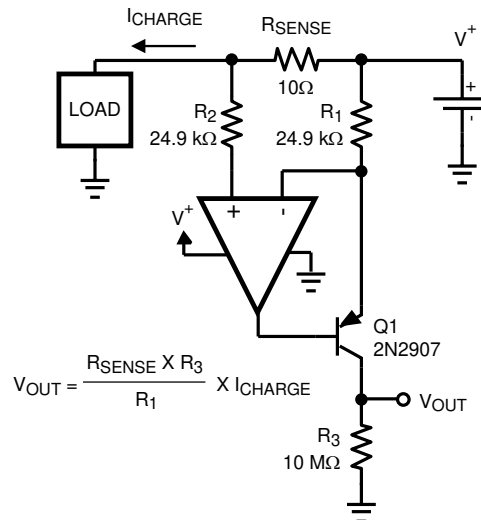


Figure 7-7. High-Side Current Sensing

#### 7.2.3.1 Design Requirements

The rail-to-rail common-mode input range and the very low quiescent current make the LPV521 an excellent choice for use in high-side and low-side battery current-sensing applications. The high-side current-sensing

circuit in [Figure 7-7](#) is commonly used in a battery charger to monitor the charging current to prevent overcharging. A sense resistor  $R_{\text{SENSE}}$  is connected in series with the battery.

### 7.2.3.2 Detailed Design Procedure

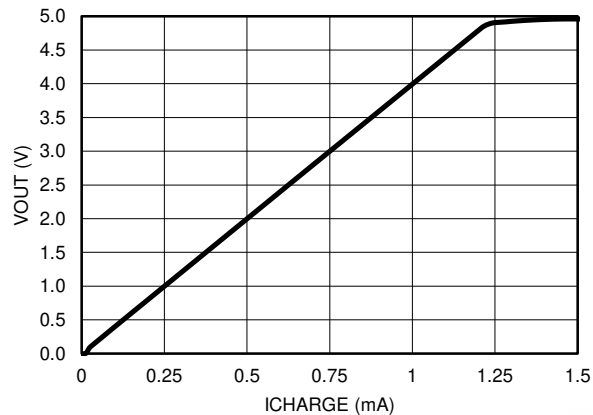
The theoretical output voltage of the circuit is  $V_{\text{OUT}} = [(R_{\text{SENSE}} \times R_3) / R_1] \times I_{\text{CHARGE}}$ . In reality, however, as a result of the finite current gain of the transistor ( $\beta$ ), the current that travels through  $R_3$  is not  $I_{\text{CHARGE}}$ . Instead,  $R_3$  is  $\alpha \times I_{\text{CHARGE}}$  or  $\beta / (\beta + 1) \times I_{\text{CHARGE}}$ . A Darlington pair can be used to increase the  $\beta$  and performance of the measuring circuit.

Using the components shown in [Figure 7-7](#) results in  $V_{\text{OUT}} \approx 4000\Omega \times I_{\text{CHARGE}}$ . This result is needed to amplify a 1mA  $I_{\text{CHARGE}}$  to near full-scale of an analog-to-digital converter (ADC) with  $V_{\text{REF}}$  at 4.1V. A resistor,  $R_2$  is used at the noninverting input of the amplifier, with the same value as  $R_1$  to minimize offset voltage.

Selecting values per [Figure 7-7](#) limits the current traveling through the  $R_1 - Q1 - R_3$  leg of the circuit to under 1 $\mu$ A, which is on the same order as the LPV521 supply current. Increasing resistors  $R_1$ ,  $R_2$ , and  $R_3$  decreases the measuring circuit supply current and extends battery life.

Decreasing  $R_{\text{SENSE}}$  minimizes error due to resistor tolerance; however, this decrease also decreases  $V_{\text{SENSE}} = I_{\text{CHARGE}} \times R_{\text{SENSE}}$ , and in turn, the amplifier offset voltage has a more significant contribution to the total error of the circuit. With the components shown in [Figure 7-7](#), the measurement circuit supply current can be kept below 1.5 $\mu$ A and measure 100 $\mu$ A to 1mA.

### 7.2.3.3 Application Curve



**Figure 7-8. Calculated High-Side Current Sense Circuit Output**

## 7.3 Power Supply Recommendations

The LPV521 is specified for operation from 1.6V to 5.5V ( $\pm 0.8V$  to  $\pm 2.75V$ ) over a  $-40^\circ\text{C}$  to  $+125^\circ\text{C}$  temperature range. Parameters that can exhibit significant variance with regard to operating voltage or temperature are presented in the [Section 5.6](#).

### 注意

Supply voltages greater than 6 V can permanently damage the device.

Low bandwidth nanopower devices do not have good high frequency ( $> 1\text{kHz}$ ) ac PSRR rejection against high-frequency switching supplies and other kHz and greater noise sources; therefore, extra supply filtering is recommended if kHz-range noise is expected on the power-supply lines.



## 7.4 Layout

### 7.4.1 Layout Guidelines

For best operational performance of the device, use good printed circuit board (PCB) layout practices, including:

- Noise can propagate into analog circuitry through the power pins of the circuit as a whole and the op amp. Use bypass capacitors to reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
- Connect low-ESR, 0.1 $\mu$ F ceramic bypass capacitors between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable for single-supply applications.
- Separate grounding for analog and digital portions of circuitry is one of the simplest and most-effective methods of noise suppression. One or more layers on multilayer PCBs are usually devoted to ground planes. A ground plane helps distribute heat and reduces EMI noise pickup. Physically separate digital and analog grounds paying attention to the flow of the ground current.
- To reduce parasitic coupling, run the input traces as far away from the supply or output traces as possible. If not possible, cross the sensitive trace perpendicular as opposed to in parallel with the noisy trace.
- Place the external components as close to the device as possible. [セクション 7.4.2](#) shows how keeping RF and RG close to the inverting input minimizes parasitic capacitance.
- Keep the length of input traces as short as possible. Always remember that the input traces are the most sensitive part of the circuit.
- Consider a driven, low-impedance guard ring around the critical traces. A guard ring can significantly reduce leakage currents from nearby traces that are at different potentials.

### 7.4.2 Layout Example

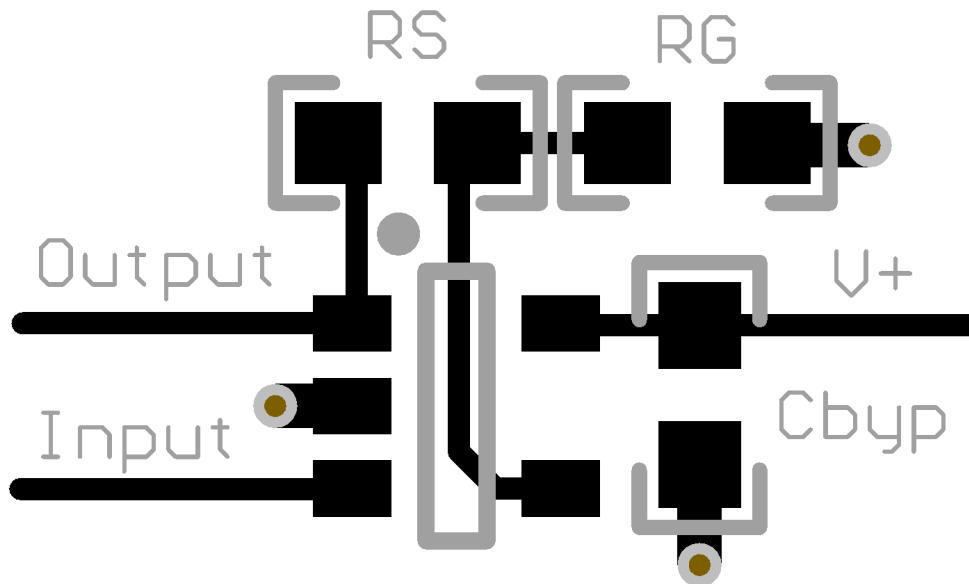


図 7-9. Noninverting Layout Example

## 8 Device and Documentation Support

### 8.1 Device Support

#### 8.1.1 Development Support

- [LPV521 PSPICE Model](#)
- TINA-TI SPICE-Based Analog Simulation Program, <http://www.ti.com/tool/tina-ti>
- [Capacitive Load Drive Solution Using an Isolation Resistor](#) reference design
- DIP Adapter Evaluation Module, <http://www.ti.com/tool/dip-adapter-evm>
- Evaluation board for 5-pin, north-facing amplifiers in the SC70 package, [SNOA487](#).
- Manual for LMH730268 Evaluation board [551012922-001](#)

### 8.2 Documentation Support

#### 8.2.1 Related Documentation

For related documentation, see the following:

- Texas Instruments, [Feedback Plots Define Op Amp AC Performance](#) application bulletin
- Texas Instruments, [AN-1698 A Specification for EMI Hardened Operational Amplifiers](#) application report
- Texas Instruments, [EMI Rejection Ratio of Operational Amplifiers](#) application report
- Texas Instruments, [Handbook of Operational Amplifier Applications](#) application report

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### 8.7 用語集

[テキサス・インスツルメンツ用語集](#)

この用語集には、用語や略語の一覧および定義が記載されています。

## 9 Revision History

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

<b>Changes from Revision D (December 2014) to Revision E (July 2024)</b>	<b>Page</b>
ドキュメント全体にわたって表、図、相互参照の採番方法を更新.....	1
P (PDIP、8) パッケージと関連する内容をドキュメントに追加.....	1
「アプリケーション」を更新.....	1
「パッケージ情報」表を更新.....	1
Added missing thermal information for DCK (SC70) package.....	4
Moved all <i>Electrical Characteristics</i> tables into one table.....	4
Updated <i>Electrical Characteristics</i> note 1.....	4
Added missing CMRR test condition for V+ = 5V.....	4
Updated common mode voltage range to fix the incorrect conditions.....	4
Updated Figure 5-4 and Figure 5-6, <i>TcvOS Distribution</i> , to fix test condition typos.....	8
Changed A <sub>OL</sub> typical value from "100 dB (100,000 ×, or 10 μV/V)" to "132dB (4000,000 ×, or 0.25μV/V)" in <i>Feature Description</i> .....	18

<b>Changes from Revision C (February 2013) to Revision D (December 2014)</b>	<b>Page</b>
「ピン構成および機能」セクション、「ESD 定格」表、「機能説明」セクション、「デバイスの機能モード」セクション、「アプリケーションと実装」セクション、「電源に関する推奨事項」セクション、「レイアウト」セクション、「デバイスおよびドキュメントのサポート」セクション、「メカニカル、パッケージ、および注文情報」セクションを追加.....	1

## 10 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
LPV521MG/NOPB	ACTIVE	SC70	DCK	5	1000	RoHS & Green	Call TI   SN	Level-1-260C-UNLIM	-40 to 125	AHA	<a href="#">Samples</a>
LPV521MGE/NOPB	ACTIVE	SC70	DCK	5	250	RoHS & Green	Call TI   SN	Level-1-260C-UNLIM	-40 to 125	AHA	<a href="#">Samples</a>
LPV521MGX/NOPB	ACTIVE	SC70	DCK	5	3000	RoHS & Green	Call TI   SN	Level-1-260C-UNLIM	-40 to 125	AHA	<a href="#">Samples</a>
LPV521P	ACTIVE	PDIP	P	8	50	RoHS & Green	NIPDAU	N / A for Pkg Type	-40 to 125	LPV521	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

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**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSELETE:** TI has discontinued the production of the device.

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(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "-" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

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**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LPV521MG/NOPB	SC70	DCK	5	1000	178.0	8.4	2.25	2.45	1.2	4.0	8.0	Q3
LPV521MGE/NOPB	SC70	DCK	5	250	178.0	8.4	2.25	2.45	1.2	4.0	8.0	Q3
LPV521MGX/NOPB	SC70	DCK	5	3000	178.0	8.4	2.25	2.45	1.2	4.0	8.0	Q3

## TAPE AND REEL BOX DIMENSIONS



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LPV521MG/NOPB	SC70	DCK	5	1000	208.0	191.0	35.0
LPV521MGE/NOPB	SC70	DCK	5	250	208.0	191.0	35.0
LPV521MGX/NOPB	SC70	DCK	5	3000	208.0	191.0	35.0



**TUBE**


\*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (μm)	B (mm)
LPV521P	P	PDIP	8	50	506	13.97	11230	4.32

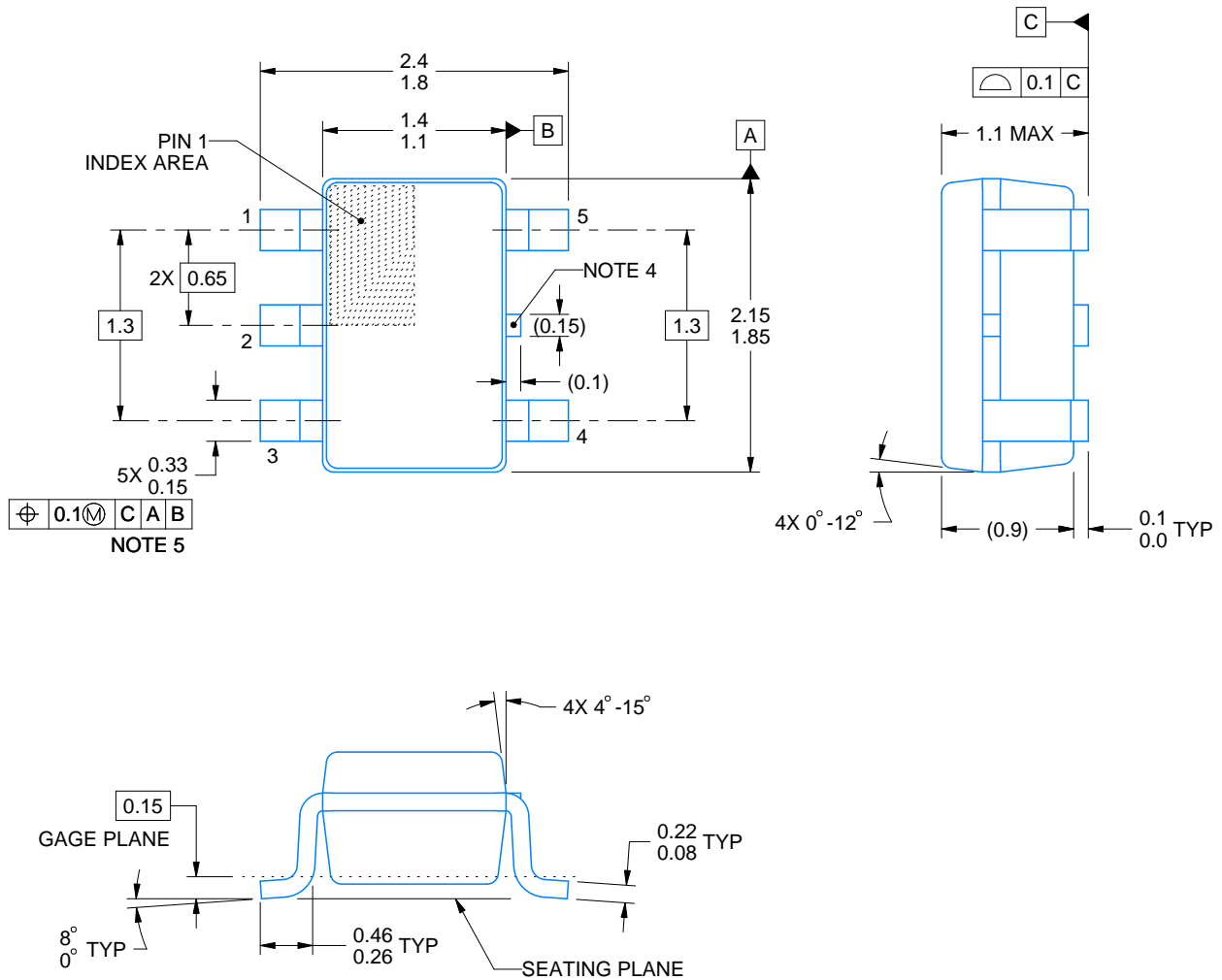
# DCK0005A



## PACKAGE OUTLINE

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



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### NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Reference JEDEC MO-203.
4. Support pin may differ or may not be present.
5. Lead width does not comply with JEDEC.
6. Body dimensions do not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.25mm per side

# EXAMPLE BOARD LAYOUT

DCK0005A

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:18X



SOLDER MASK DETAILS

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NOTES: (continued)

- 7. Publication IPC-7351 may have alternate designs.
- 8. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DCK0005A

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 THICK STENCIL  
SCALE:18X

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NOTES: (continued)

9. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
10. Board assembly site may have different recommendations for stencil design.

P (R-PDIP-T8)

PLASTIC DUAL-IN-LINE PACKAGE



- NOTES:
- A. All linear dimensions are in inches (millimeters).
  - B. This drawing is subject to change without notice.
  - C. Falls within JEDEC MS-001 variation BA.

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