

TPS70245, TPS70248 TPS70251, TPS70258 TPS70202

SLVS286E – JUNE 2000 – REVISED DECEMBER 2009

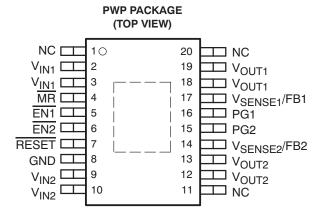
# DUAL-OUTPUT, LOW DROPOUT VOLTAGE REGULATORS WITH INTEGRATED SVS FOR SPLIT VOLTAGE SYSTEMS

# FEATURES

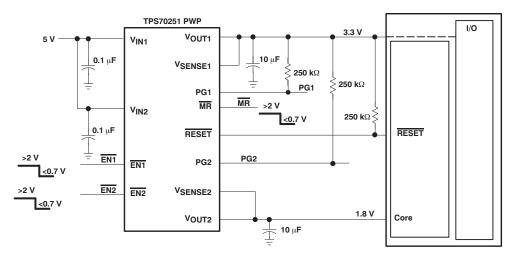
- Dual Output Voltages for Split-Supply Applications
- Independent Enable Functions (See Part Number TPS701xx for Sequenced Outputs)
- Output Current Range of 500mA on Regulator 1 and 250mA on Regulator 2
- Fast Transient Response
- Voltage Options: 3.3V/2.5V, 3.3V/1.8V, 3.3V/1.5V, 3.3V/1.2V, and Dual Adjustable Outputs
- Open Drain Power-On Reset with 120ms Delay
- Open Drain Power Good for Regulator 1 and Regulator 2
- Ultralow 190µA (typ) Quiescent Current
- 1µA Input Current During Standby
- Low Noise: 65µV<sub>RMS</sub> Without Bypass Capacitor
- Quick Output Capacitor Discharge Feature
- One Manual Reset Input
- 2% Accuracy Over Load and Temperature
- Undervoltage Lockout (UVLO) Feature
- 20-Pin PowerPAD<sup>™</sup> TSSOP Package
- Thermal Shutdown Protection

# DESCRIPTION

The TPS702xx is <u>a low dropout</u> voltage regulator with integrated SVS (RESET, POR, or power on reset) and power good (PG) functions. These devices are capable of supplying 500mA and 250mA by regulator 1 and regulator 2 respectively. Quiescent current is typically 190µA at full load. Differentiated features, such as accuracy, fast transient response, SVS supervisory circuit (power on reset), manual reset input, and independent enable functions provide a complete system solution.







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The TPS702xx family of voltage regulators offers very low dropout voltage and dual outputs. These devices have extremely low noise output performance without using any added filter bypass capacitors and are designed to have a fast transient response and be stable with 10µF low ESR capacitors.

These devices have fixed 3.3V/2.5V, 3.3V/1.8V, 3.3V/1.5V, 3.3V/1.2V, and adjustable voltage options. Regulator 1 can support up to 500mA, and regulator 2 can support up to 250mA. Separate voltage inputs allow the designer to configure the source power.

Because the PMOS device behaves as a low-value resistor, the dropout voltage is very low (typically 170mV on regulator 1) and is directly proportional to the output current. Additionally, since the PMOS pass element is a voltage-driven device, the quiescent current is very low and independent of output loading (maximum of 230µA over the full range of output current and full range of temperature). This LDO family also features a sleep mode; applying a high signal to EN1 or EN2 (enable) shuts down regulator 1 or regulator 2, respectively. When a high signal is applied to both EN1 and EN2, both regulators enter sleep mode, thereby reducing the input current to  $2\mu$ A at  $T_J = +25^{\circ}$ C.

For each regulator, there is an internal discharge transistor to discharge the output capacitor when the regulator is turned off (disabled).

The PG1 pin reports the voltage condition at  $V_{OUT1}$ . The PG1 pin can be used to implement a SVS (RESET, POR, or power on reset) for the circuitry supplied by regulator 1. The PG2 pin reports the voltage conditions at  $V_{OUT2}$ . The PG2 pin can be used to implement a SVS (power on reset) for the circuitry supplied by regulator 2.

The TPS702xx features a RESET (SVS, POR, or power on reset). RESET output initiates a reset in the event of an undervoltage condition. RESET also indicates the status of the manual reset pin (MR). When MR is in the logic high state, RESET goes to a high impedance state after a 120ms delay. To monitor  $V_{OUT1}$ , the PG1 output pin can be connected to MR. To monitor  $V_{OUT2}$ , the PG2 output pin can be connected to MR.

The device has an undervoltage lockout UVLO circuit that prevents the internal regulators from turning on until  $V_{IN1}$  reaches 2.5V.

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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

	VOLTA	GE (V) <sup>(2)</sup>	PACKAGE- LEAD	SPECIFIED TEMPERATURE	ORDERING	TRANSPORT
PRODUCT	V <sub>OUT1</sub>	V <sub>OUT2</sub>	(DESIGNATOR)	RANGE (T <sub>J</sub> )	NUMBER	MEDIA, QUANTITY
TPS70202	Adjustable	Adjustable	HTSSOP-20 (PWP)	-40°C to +125°C	TPS70202PWP	Tube, 70
1F370202	Aujustable	Aujustable	H1330F-20 (FWF)	-40 C 10 +125 C	TPS70202PWPR	Tape and Reel, 2000
TPS70245	3.3V	1.2V	HTSSOP-20 (PWP)	-40°C to +125°C	TPS70245PWP	Tube, 70
1F370245	3.3V	1.2 V	П1330F-20 (FWF)	-40 C 10 +125 C	TPS70245PWPR	Tape and Reel, 2000
TPS70248	2.21/	1.5V	HTSSOP-20 (PWP)	-40°C to +125°C	TPS70248PWP	Tube, 70
1P570246	3.3V			-40 °C 10 +125 °C	TPS70248PWPR	Tape and Reel, 2000
TPS70251	3.3V	1.8V	HTSSOP-20 (PWP)	-40°C to +125°C	TPS70251PWP	Tube, 70
1P570251	3.3V	1.0V	H1330P-20 (PWP)	-40 °C 10 +125 °C	TPS70251PWPR	Tape and Reel, 2000
TPS70258	3.3V	2.5V	HTSSOP-20 (PWP)	-40°C to +125°C	TPS70258PWP	Tube, 70
1F370256	3.3V	2.3V	птээог-20 (PWP)	-40 C 10 +125 C	TPS70258PWPR	Tape and Reel, 2000

## ORDERING INFORMATION<sup>(1)</sup>

(1) For the most current package and ordering information see the Package Option Addendum located at the end of this document, or see the TI web site at www.ti.com.

(2) For fixed 1.20V operation, tie FB to OUT.

# ABSOLUTE MAXIMUM RATINGS<sup>(1)</sup>

Over operating free-air temperature range (unless otherwise noted).

	TPS702xx	UNIT
Input voltage range: V <sub>IN1</sub> , V <sub>IN2</sub> <sup>(2)</sup>	-0.3 to +7	V
Voltage range at EN1, EN2	-0.3 to +7	V
Output voltage range (V <sub>OUT1</sub> , V <sub>SENSE1</sub> )	5.5	V
Output voltage range (V <sub>OUT2</sub> , V <sub>SENSE2</sub> )	5.5	V
Maximum RESET, PG1, PG2 voltage	7	V
Maximum MR voltage	V <sub>IN1</sub>	V
Peak output current	Internally limited	—
Continuous total power dissipation	See Dissipation Ratings Table	—
Operating virtual junction temperature range, T <sub>J</sub>	-40 to +150	°C
Storage temperature range, T <sub>stg</sub>	-65 to +150	°C
ESD rating, HBM	2	kV

(1) Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltages are tied to network ground.

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### **DISSIPATION RATINGS**

PACKAGE	AIR FLOW (CFM)	T <sub>A</sub> ≤ +25°C	DERATING FACTOR	T <sub>A</sub> = +70°C	T <sub>A</sub> = +85°C
PWP <sup>(1)</sup>	0	3.067W	30.67mW/°C	1.687W	1.227W
PVVP	250	4.115W	41.15mW/°C	2.265W	1.646W

(1) This parameter is measured with the recommended copper heat sink pattern on a 4-layer PCB, 1 oz. copper on a 4-in by 4-in ground layer. For more information, refer to TI technical brief SLMA002.

# **RECOMMENDED OPERATING CONDITIONS**

Over operating temperature range (unless otherwise noted).

	MIN	MAX	UNIT
Input voltage, V <sub>I</sub> <sup>(1)</sup> (regulator 1 and 2)	2.7	6	V
Output current, I <sub>O</sub> (regulator 1)	0	500	mA
Output current, I <sub>O</sub> (regulator 2)	0	250	mA
Output voltage range (for adjustable option)	1.22	5.5	V
Operating virtual junction temperature, T <sub>J</sub>	-40	+125	°C

(1) To calculate the minimum input voltage for maximum output current, use the following equation:  $V_{I(min)} = V_{O(max)} + V_{DO(max load)}$ .

# **ELECTRICAL CHARACTERISTICS**

Over recommended operating junction temperature range ( $T_J = -40^{\circ}C$  to  $+125^{\circ}C$ ),  $V_{IN1}$  or  $V_{IN2} = V_{OUT(nom)} + 1V$ ,  $I_O = 1mA$ , EN1 = 0V, EN2 = 0V, and  $C_O = 33\mu$ F (unless otherwise noted).

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT		
		Reference	2.7V < V <sub>IN</sub> < 6V, T <sub>J</sub> = +25°C	FB connected to $V_{O}$		1.22			
		voltage	2.7V < V <sub>IN</sub> < 6V,	FB connected to V <sub>O</sub>	1.196		1.244	l	
Output Vo voltage <sup>(1) ,</sup>		2.7V < V <sub>IN</sub> < 6V,	$T_J = +25^{\circ}C$		1.2				
	1.2V Output	2.7V < V <sub>IN</sub> < 6V,		1.176		1.224			
		2.7V < V <sub>IN</sub> < 6V,	$T_J = +25^{\circ}C$		1.5				
	1.5V Output	2.7V < V <sub>IN</sub> < 6V,		1.47		1.53	V		
Ū	(2)		2.8V < V <sub>IN</sub> < 6V,	$T_J = +25^{\circ}C$		1.8			
		1.8V Output	2.8V < V <sub>IN</sub> < 6V,		1.764		1.836		
			3.5V < V <sub>IN</sub> < 6V,	$T_J = +25^{\circ}C$		2.5			
		2.5V Output	3.5V < V <sub>IN</sub> < 6V,		2.45		2.55		
			4.3V < V <sub>IN</sub> < 6V,	$T_J = +25^{\circ}C$		3.3			
	3.3V Output	4.3V < V <sub>IN</sub> < 6V,		3.234		3.366			
Quiescent current (GND current) for		See (2)	$T_J = +25^{\circ}C$		190				
regulator 1 and regulator 2, $\overline{EN1} = \overline{EN2}$ = 0V <sup>(1)</sup>		2, EN1 = EN2	See <sup>(2)</sup>				230	μA	
Output voltage line regulation ( $\Delta V_O/V_O)$ for regulator 1 and regulator 2 $^{(3)}$		$V_{\rm O}+1V < V_{\rm IN} \le 6V,$	$T_J = +25^{\circ}C^{(1)}$		0.01		- %V		
		$V_{O} + 1V < V_{IN} \le 6V$	(1)			0.1			
Load regu	lation for V <sub>OUT</sub>	<sub>1</sub> and V <sub>OUT2</sub>	T <sub>J</sub> = +25°C			1		mV	
	Output noise	Regulator 1		С <sub>О</sub> = 33µF, Т <sub>Ј</sub> = +25°С		65		$\mu V_{RMS}$	
Vn	voltage	Regulator 2	BW = 300Hz  to  50kHz,	$C_0 = 33\mu r$ , $T_1 = +25 C$		65			
Output out	rrant limit	Regulator 1	V <sub>OUT</sub> = 0V			1.6	1.9	A	
Output cu	ment innit	Regulator 2				0.750	1		
Thermal s	hutdown junctio	on temperature				+150		°C	
l <sub>i</sub>	Standby	Regulator 1	$\overline{\text{EN1}} = \text{V}_{\text{IN}}, \ \overline{\text{EN2}} = \text{V}_{\text{I}}$	$T_J = +25^{\circ}C$			2		
(standby)	current	Regulator 2	$\overline{\text{EN1}} = \text{V}_{\text{IN}}, \ \overline{\text{EN2}} = \text{V}_{\text{I}}$				6	μA	
	Power-		Regulator 1	f = 1kHz, C <sub>O</sub> = 33µF, I <sub>OUT1</sub> = 500mA	$T_{J} = +25^{\circ}C^{(1)}$		60		JD
PSRR supply ripple rejection		Regulator 2	$f = 1kHz, C_O = 33\mu F,$ $I_{OUT2} = 250mA$	$T_{J} = +25^{\circ}C^{(1)}$		50		dB	
UVLO threshold				2.4		2.65	V		
RESET Te	erminal						1		
Minimum i	input voltage fo	r valid RESET	I <sub>RESET</sub> = 300μA,	V <sub>(RESET)</sub> ≤ 0.8V		1.0	1.3	V	
t (RESET)			RESET pulse duration		80	120	160	ms	
Output lov	v voltage		V <sub>IN</sub> = 3.5V,	I <sub>(RESET)</sub> = 1mA		0.15	0.4	V	
Leakage d	current		$V_{(RESET)} = 6V$				1	μA	

Minimum input operating voltage is 2.7V or V<sub>O(typ)</sub> + 1V, whichever is greater. Maximum input voltage = 6V, minimum output current = 1mA.

(2)  $I_0 = 1$ mA to 500mA for Regulator 1 and 1mA to 250mA for Regulator 2.

(3) If 
$$V_0 < 1.8V$$
 then  $V_{\text{Imax}} = 6V$ ,  $V_{\text{Imin}} = 2.7V$ : Line regulation (mV) = (%/V) x  $V_0 \frac{(V_{\text{Imax}} - 2.7)}{100}$  x 1000  
If  $V_0 > 2.5V$  then  $V_{\text{Imax}} = 6V$ ,  $V_{\text{Imin}} = V_0 + 1V$ : Line regulation (mV) = (%/V) x  $V_0 \frac{[V_{\text{Imax}} - (V_0 + 1)]}{100}$  x 1000

**EXAS INSTRUMENTS** 

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# **ELECTRICAL CHARACTERISTICS (continued)**

Over recommended operating junction temperature range ( $T_J = -40^{\circ}C$  to  $+125^{\circ}C$ ),  $V_{IN1}$  or  $V_{IN2} = V_{OUT(nom)} + 1V$ ,  $I_O = 1mA$ , EN1 = 0V, EN2 = 0V, and  $C_O = 33\mu$ F (unless otherwise noted).

PARAMETER	TEST CONDITIONS		MIN	TYP	MAX	UNIT
PG1/PG2 Terminal	·					
Minimum input voltage for valid PGx	$I_{(PGx)} = 300 \mu A,$	V <sub>(PGx)</sub> ≤ 0.8V		1.0	1.3	V
Trip threshold voltage	V <sub>O</sub> decreasing		92	95	98	%V <sub>OUT</sub>
Hysteresis voltage	Measured at V <sub>O</sub>			0.5		%V <sub>OUT</sub>
t <sub>r(PGx)</sub>	Rising edge deglitch			30		μs
Output low voltage	V <sub>IN</sub> = 2.7V,	$I_{(PGx)} = 1mA$		0.15	0.4	V
Leakage current	$V_{(PGx)} = 6V$				1	μA
EN1/EN2 Terminal						
High-level ENx input voltage			2			V
Low-level ENx input voltage					0.7	V
Input current (ENx)			-1		1	μA
MR Terminal						
High-level input voltage			2			V
Low-level input voltage					0.7	V
Pull-up current source				6		μA
V <sub>OUT1</sub> Terminal						
Dropout voltage <sup>(4)</sup>	I <sub>O</sub> = 500mA, V <sub>IN1</sub> = 3	$T_{\rm J} = +25^{\circ}{\rm C}$	170			
Dropout voltage.	I <sub>O</sub> = 500mA, V <sub>IN1</sub> = 3	3.2V			275	mV
Peak output current	2ms pulse width			750		mA
Discharge transistor current	V <sub>OUT1</sub> = 1.5V			7.5		mA
V <sub>OUT2</sub> Terminal						
Peak output current	2ms pulse width			375		mA
Discharge transistor current	V <sub>OUT2</sub> = 1.5V			7.5		mA
FB Terminal	·					
Input current: TPS70202	FB = 1.8V			1		μA

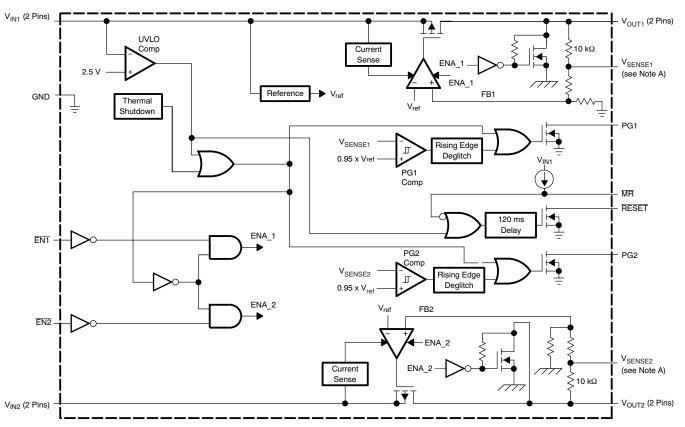
Input voltage ( $V_{IN1}$  or  $V_{IN2}$ ) =  $V_{O(typ)}$  – 100mV. For 1.5V, 1.8V and 2.5V regulators, the dropout voltage is limited by input voltage range. The 3.3V regulator input is set to 3.2V to perform this test. (4)





# **DEVICE INFORMATION**

**Fixed Voltage Version** 



A. For most applications, V<sub>SENSE1</sub> and V<sub>SENSE2</sub> should be externally connected to V<sub>OUT1</sub> and V<sub>OUT2</sub>, respectively, as close as possible to the device. For other implementations, refer to SENSE terminal connection discussion in the *Application Information* section.

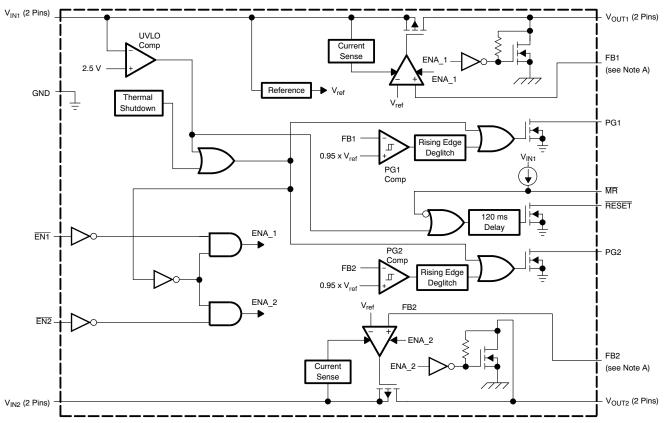
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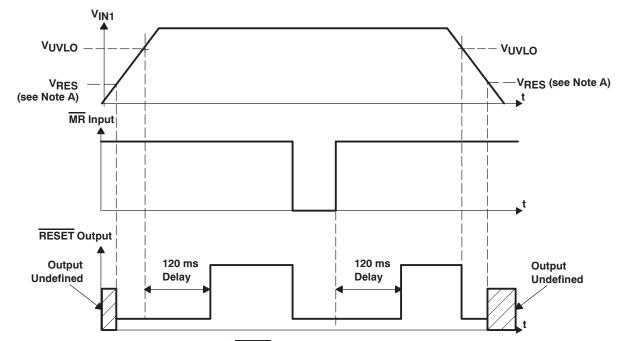


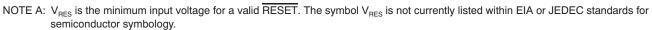
Α. For most applications, FB1 and FB2 should be externally connected to resistor dividers as close as possible to the device. For other implementations, refer to FB terminals connection discussion in the Application Information section.

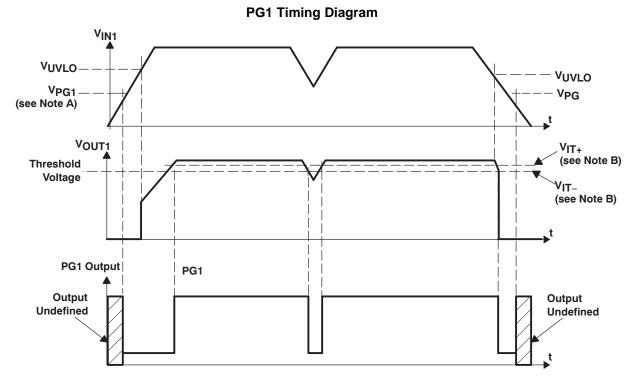




**RESET** Timing Diagram





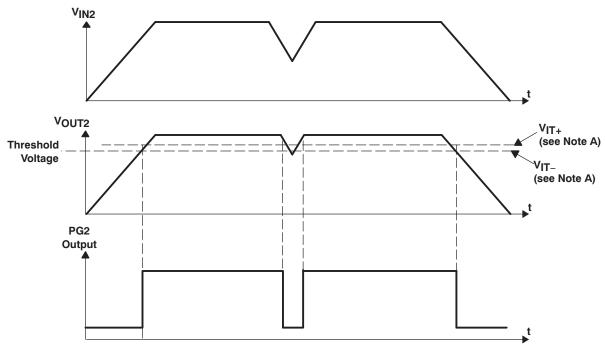


NOTES: A. V<sub>PG1</sub> is the minimum input voltage for a valid PG1. The symbol V<sub>PG1</sub> is not currently listed within EIA or JEDEC standards for semiconductor symbology.

B.  $V_{IT-}$  trip voltage is typically 5% lower than the output voltage (95%  $V_0$ ).  $V_{IT-}$  to  $V_{IT+}$  is the hysteresis voltage.







NOTE A:  $V_{IT_{-}}$  trip voltage is typically 5% lower than the output voltage (95% V<sub>0</sub>).  $V_{IT_{-}}$  to  $V_{IT_{+}}$  is the hysteresis voltage.

TERMINAL I/O		1/0	DESCRIPTION			
NAME	NO.	1/0	DESCRIPTION			
EN1	5	I	Active low enable for V <sub>OUT1</sub>			
EN2	6	I	Active low enable for V <sub>OUT2</sub>			
GND	8	_	Ground			
MR	4	I	Manual reset input, active low, pulled up internally			
NC	1, 11, 20	_	No connection			
PG1	16	0	Open drain output, low when V <sub>OUT1</sub> voltage is less than 95% of the nominal regulated voltage			
PG2	15	0	Open drain output, low when V <sub>OUT2</sub> voltage is less than 95% of the nominal regulated voltage			
RESET	7	I	Open drain output, SVS (power-on reset) signal, active low			
V <sub>IN1</sub>	2, 3	I	Input voltage of regulator 1			
V <sub>IN2</sub>	9, 10	I	Input voltage of regulator 2			
V <sub>OUT1</sub>	18, 19	0	Output voltage of regulator 1			
V <sub>OUT2</sub>	12, 13	0	Output voltage of regulator 2			
V <sub>SENSE2</sub> /FB2	14	I	Regulator 2 output voltage sense/regulator 2 feedback for adjustable			
V <sub>SENSE1</sub> /FB1	17	I	Regulator 1 output voltage sense/regulator 1 feedback for adjustable			

### **TERMINAL FUNCTIONS**



### **Detailed Description**

The TPS702xx low dropout regulator family provides dual regulated output voltages with independent enable functions. These devices provide fast transient response and high accuracy with small output capacitors, while drawing low quiescent current. Other features are integrated SVS (power-on reset, RESET) and power good (PG1, PG2) that monitor output voltages and provide logic output to the system. These differentiated features provide a complete power solution.

The TPS702xx, unlike many other LDOs, features very low quiescent current that remains virtually constant even with varying loads. Conventional LDO regulators use a pnp pass element, the base current of which is directly proportional to the load current through the regulator ( $I_B = I_C/\beta$ ). The TPS702xx uses a PMOS transistor to pass current; the gate of the PMOS is voltage-driven, so operating current is low and stable over the full load range.

## **Pin Functions**

## Enable (EN1, EN2)

The EN terminals are inputs that enable or shut down each respective regulator. If EN is at a voltage high signal, the respective regulator is in shutdown mode. When EN goes to voltage low, the respective regulator is enabled.

### Power-Good (PG1, PG2)

The PG terminals are open drain, active high output terminals that indicate the status of each respective regulator. When  $V_{OUT1}$  reaches 95% of its regulated voltage, PG1 goes to a high impedance state. When  $V_{OUT2}$  reaches 95% of its regulated voltage, PG2 goes to a high impedance state. Each PG goes to a low impedance state when its respective output voltage is pulled below 95% (that is, goes to an overload condition) of its regulated voltage. The open drain outputs of the PG terminals require a pull-up resistor.

### Manual Reset Pin

 $\overline{\text{MR}}$  is an active low input terminal used to trigger a reset condition. When  $\overline{\text{MR}}$  is pulled to logic low, a POR (RESET) occurs. The terminal has a 6µA pull-up current to V<sub>IN1</sub>.

### Sense (V<sub>SENSE1</sub>, V<sub>SENSE2</sub>)

The sense terminals of fixed-output options must be connected to the regulator outputs, and the connection should be as short as possible. Internally, the sense terminal connects to high-impedance, wide-bandwidth amplifiers through a resistor-divider network and noise pickup feeds through to the regulator output. It is essential to route the sense connection in such a way as to minimize or avoid noise pickup. Adding RC networks between sense terminals and  $V_{OUT}$  terminals to filter noise is not recommended because these networks can cause the regulators to oscillate.



### FB1 and FB2

FB1 and FB2 are input terminals used for adjustable-output devices and must be connected to the external feedback resistor divider. FB1 and FB2 connections should be as short as possible. It is essential to route them in such a way as to minimize or avoid noise pickup. Adding RC networks between FB terminals and  $V_{OUT}$  terminals to filter noise is not recommended because these networks can cause the regulators to oscillate.

## **RESET** Indicator

The TPS702xx features a RESET (SVS, POR, or power on reset). RESET can be used to drive power on reset circuitry or a low-battery indicator. RESET is an active low, open drain output that indicates the status of the manual reset pin (MR). When MR is in a high impedance state, RESET goes to a high impedance state after a 120 ms delay. To monitor  $V_{OUT1}$ , the PG1 output pin can be connected to MR. To monitor  $V_{OUT2}$ , the PG2 output pin can be connected to MR. To monitor V<sub>OUT2</sub>, the PG2 output pin can be connected to MR. To monitor I RESET is not used, it can be left floating.

### $V_{\text{IN1}}$ and $V_{\text{IN2}}$

 $V_{IN1}$  and  $V_{IN2}$  are inputs to each regulator. Internal bias voltages are powered by  $V_{IN1}$ .

### V<sub>OUT1</sub> and V<sub>OUT2</sub>

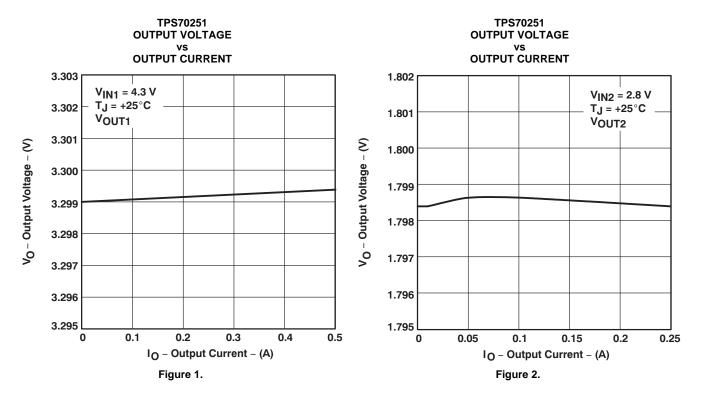
 $V_{OUT1}$  and  $V_{OUT2}$  are output terminals of each regulator.



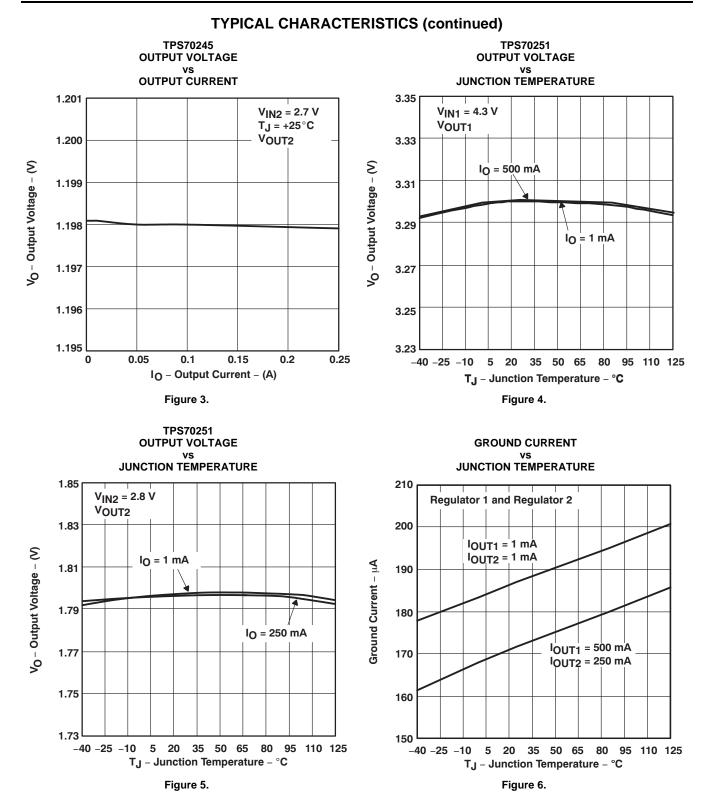
# **TYPICAL CHARACTERISTICS**

### **Table of Graphs**

			FIGURE
V	Output voltage	vs Output current	Figure 1 to Figure 3
Vo	Oulput voltage	vs Junction temperature	Figure 4 to Figure 5
	Ground current	vs Junction temperature	Figure 6
PSRR	Power-supply rejection ratio	vs Frequency	Figure 7 to Figure 10
	Output spectral noise density	vs Frequency	Figure 11 to Figure 14
ZO	Output impedance	vs Frequency	Figure 15 to Figure 18
	Dropout veltage	vs Temperature	Figure 19 and Figure 20
	Dropout voltage	vs Input voltage	Figure 21 and Figure 22
	Load transient response		Figure 23 and Figure 24
	Line transient response (V <sub>OUT1</sub> )		Figure 25
	Line transient response (V <sub>OUT2</sub> )		Figure 26
Vo	Output voltage	vs Time (start-up)	Figure 27 and Figure 28
	Equivalent series resistance (ESR)	vs Output current	Figure 30 to Figure 33





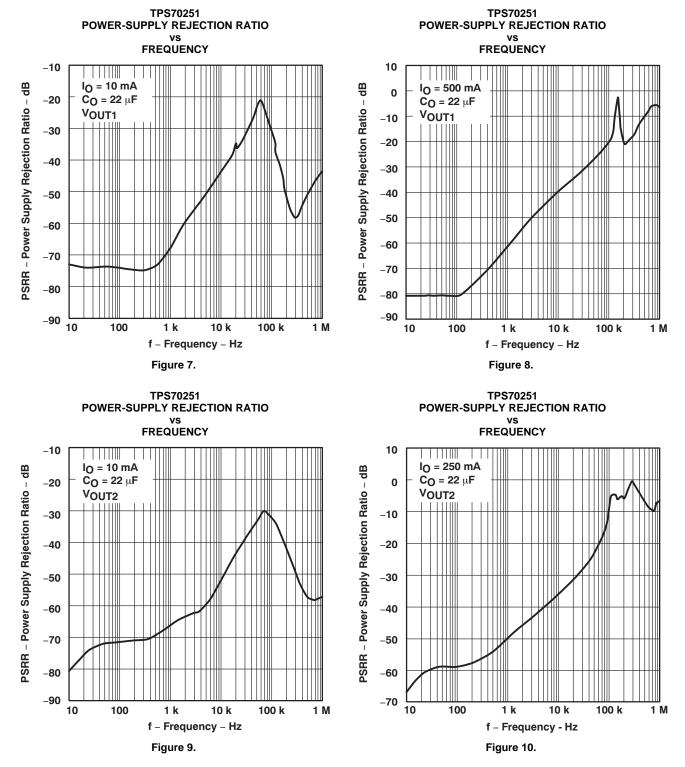




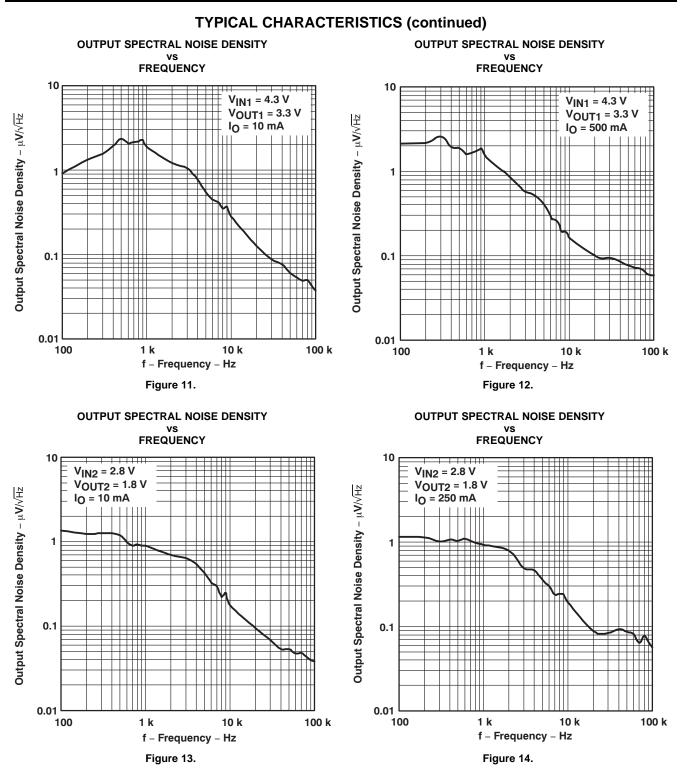
TPS70245, TPS70248 TPS70251, TPS70258 TPS70202 SLVS286E – JUNE 2000–REVISED DECEMBER 2009

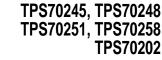










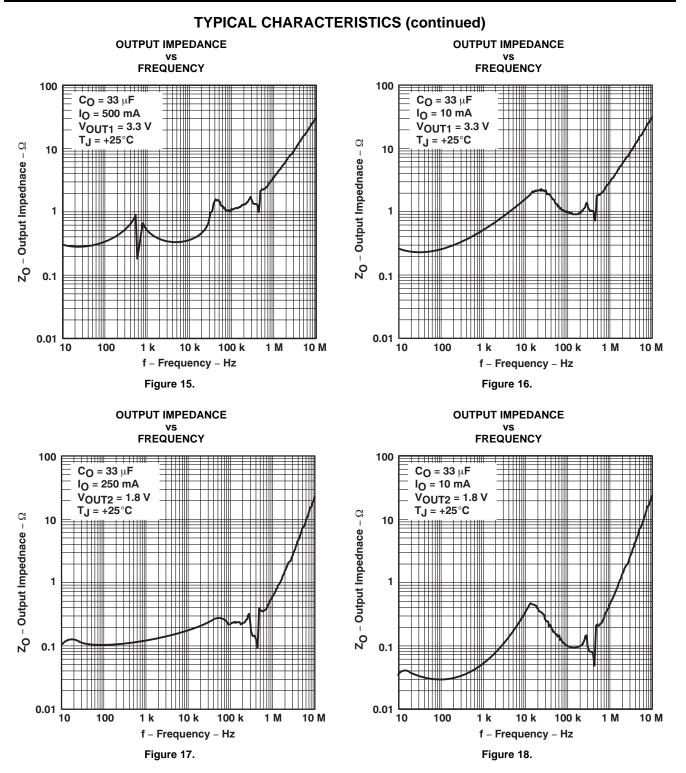


SLVS286E – JUNE 2000 – REVISED DECEMBER 2009

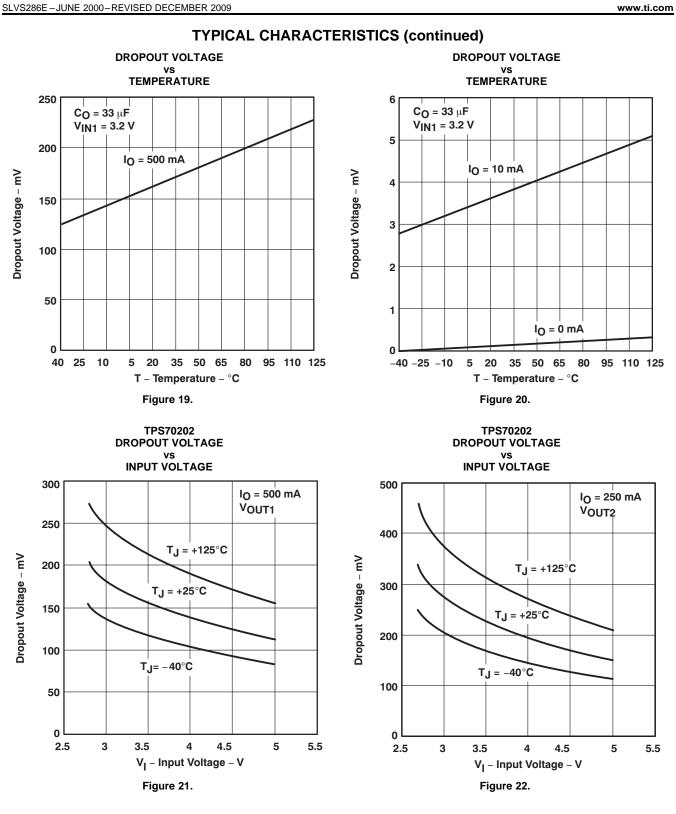


Texas

**INSTRUMENTS** 

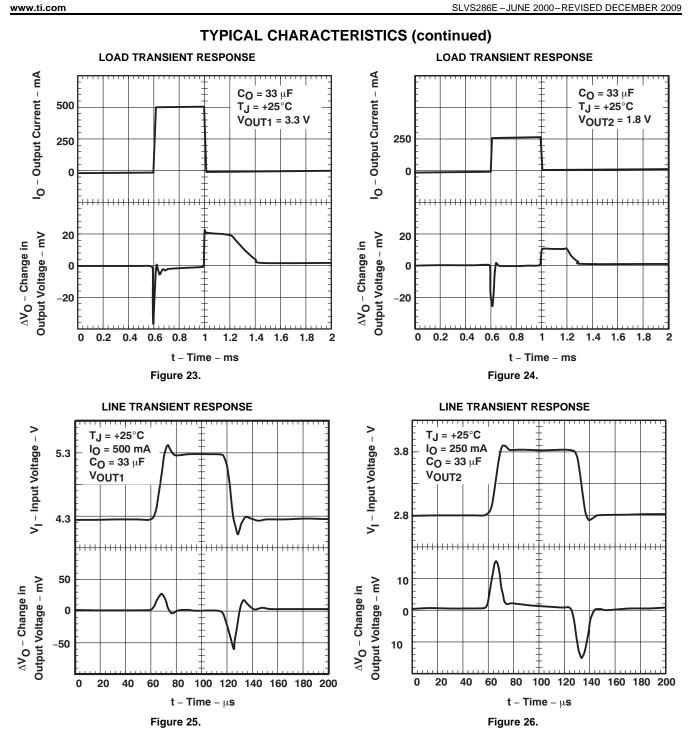








TPS70245, TPS70248 TPS70251, TPS70258 TPS70202





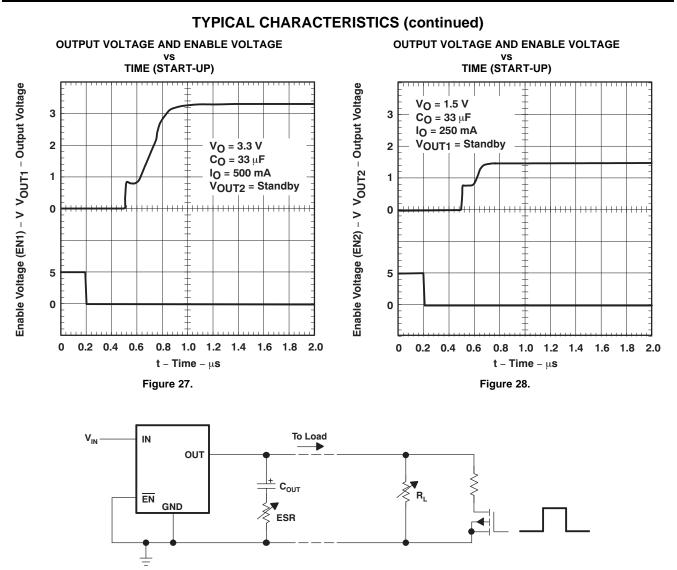


Figure 29. Test Circuit for Typical Regions of Stability

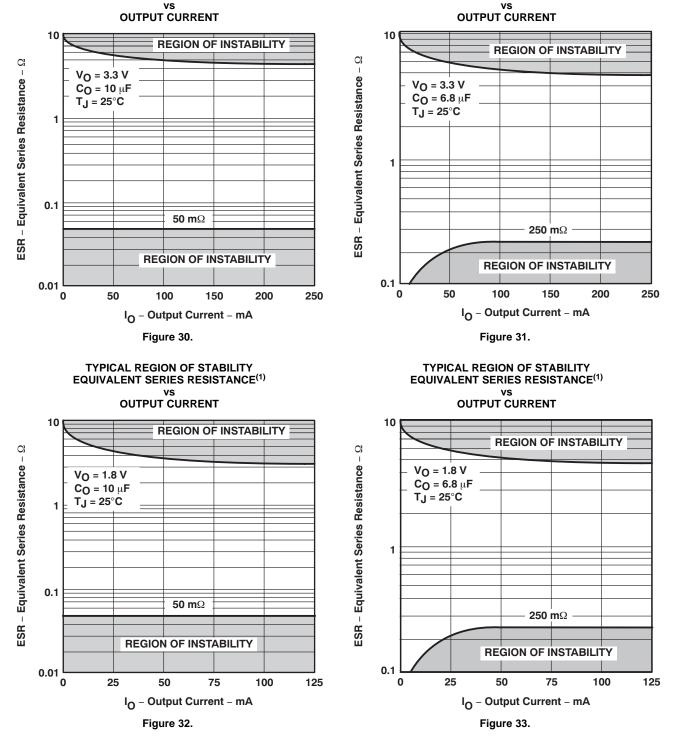




**TYPICAL CHARACTERISTICS (continued)** 

TYPICAL REGION OF STABILITY EQUIVALENT SERIES RESISTANCE<sup>(1)</sup>

### TYPICAL REGION OF STABILITY EQUIVALENT SERIES RESISTANCE<sup>(1)</sup>



<sup>(1)</sup> Equivalent series resistance (ESR) refers to the total series resistance, including the ESR of the capacitor, any series resistance added externally, and PWB trace resistance to  $C_0$ .



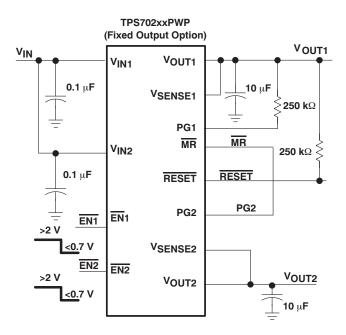
# **APPLICATION INFORMATION**

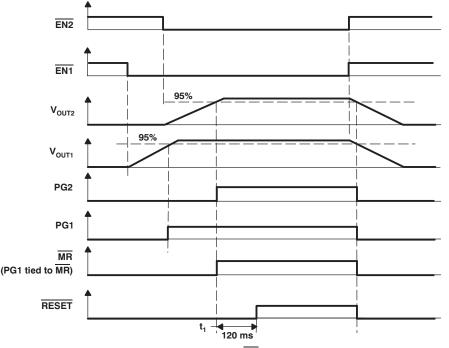
# Sequencing Timing Diagrams

This section provides a number of timing diagrams showing how this device functions in different configurations.

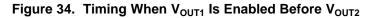
**Application condition:**  $V_{IN1}$  and  $V_{IN2}$  are tied to the same fixed input voltage greater than  $V_{UVLO}$ . PG2 is tied to MR.

 $\overline{\text{EN1}}$  and  $\overline{\text{EN2}}$  are initially high; therefore, both regulators are off, and PG1 and PG2 (tied to MR) are at logic low. Since MR is at logic low, RESET is also at logic low. When  $\overline{\text{EN1}}$  is taken to logic low,  $V_{\text{OUT1}}$ turns on. Later, when  $\overline{\text{EN2}}$  is taken to logic low,  $V_{\text{OUT2}}$ turns on. When  $V_{\text{OUT1}}$  reaches 95% of its regulated output voltage, PG1 goes to logic high. When  $V_{\text{OUT2}}$ reaches 95% of its regulated output voltage, PG2 (tied to MR) goes to logic high. When  $V_{\text{IN1}}$  is greater than  $V_{\text{UVL0}}$  and M R (tied to PG2) is at logic high, RESET is pulled to logic high after a 120ms delay. When EN1 and EN2 are returned to logic high, both devices power down and both PG1, PG2 (tied to MR2), and RESET return to logic low.





NOTES: A.  $t_1$ : Time at which  $V_{IN}$  is greater than  $V_{UVLO}$  and  $\overline{MR}$  is logic high. B. The timing diagram is not drawn to scale.

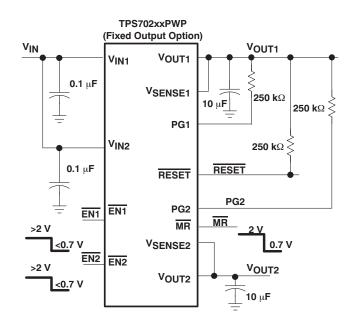


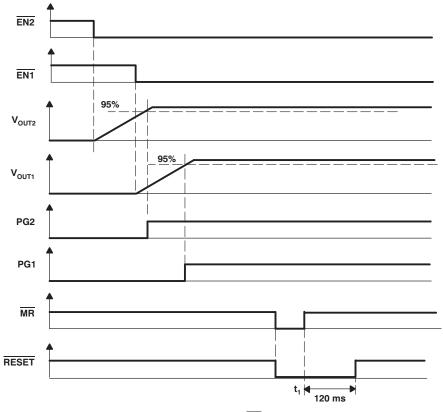


**Application condition:**  $V_{IN1}$  and  $V_{IN2}$  are tied to the same fixed input voltage greater than  $V_{UVLO}$ . MR is initially logic high but is eventually toggled.

 $\overline{\text{EN1}}$  and  $\overline{\text{EN2}}$  are initially high; therefore, both regulators are off, and PG1 and PG2 are at logic low. Since  $V_{\text{IN1}}$  is greater than  $V_{\text{UVLO}}$  and  $\overline{\text{MR}}$  is at logic high, RESET is also at logic high. When  $\overline{\text{EN2}}$  is taken to logic low,  $V_{\text{OUT2}}$  turns on. Later, when  $\overline{\text{EN1}}$  is taken to logic low,  $V_{\text{OUT2}}$  turns on. When  $V_{\text{OUT2}}$  reaches 95% of its regulated output voltage, PG2 goes to logic high. When  $V_{\text{OUT1}}$  reaches 95% of its regulated output voltage, PG1 goes to logic high. When  $M\overline{\text{R}}$  is taken to logic low, RESET is taken low. When  $\overline{\text{MR}}$  is taken to logic low, RESET returns to logic high, RESET returns to logic high, after a 120ms delay.

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NOTES: A.  $t_1$ : Time at which  $V_{IN}$  is greater than  $V_{UVLO}$  and  $\overline{MR}$  is logic high. B. The timing diagram is not drawn to scale.

Figure 35. Timing When MR is Toggled

# TPS70245, TPS70248 TPS70251, TPS70258 TPS70202

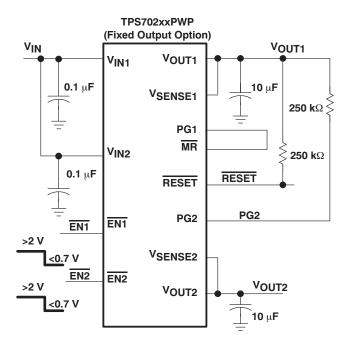
SLVS286E – JUNE 2000 – REVISED DECEMBER 2009

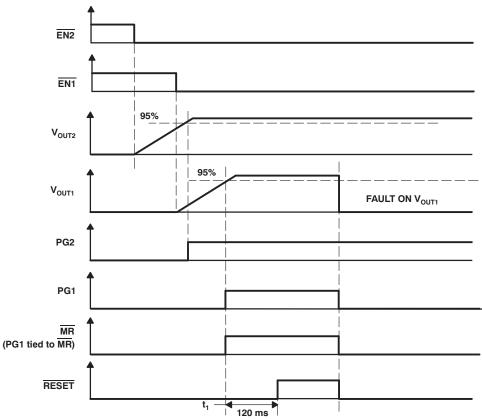
Application condition:  $V_{IN1}$  and  $V_{IN2}$  are tied to same fixed input voltage greater than  $V_{UVLO}$ . PG1 is tied to  $\overline{MR}$ .

 $\overline{\rm EN1}$  and  $\overline{\rm EN2}$  are initially high; therefore, both regulators are off, and PG1 (tied to MR) and PG2 are at logic low. Since MR is at logic low, RESET is also at logic low. When  $\overline{\rm EN2}$  is taken to logic low,  $V_{\rm OUT2}$  turns on. Later, when EN1 is taken to logic low,  $V_{\rm OUT1}$  turns on. When  $V_{\rm OUT2}$  reaches 95% of its regulated output voltage, PG2 goes to logic high. When  $V_{\rm OUT1}$  reaches 95% of its regulated output voltage, PG1 goes to logic high. When  $V_{\rm IN1}$  is greater than  $V_{\rm UVL0}$  and MR (tied to PG2) is at logic high, RESET is pulled to logic high after a 120ms delay. When a fault on  $V_{\rm OUT1}$  causes it to fall below 95% of its regulated output voltage, PG1 (tied to MR) goes to logic low. Since MR is logic low, RESET goes to logic low.  $V_{\rm OUT2}$  is unaffected.



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NOTES: A.  $t_{1}$ : Time at which  $V_{\rm IN}$  is greater than  $V_{\rm UVLO}$  and  $\overline{\rm MR}$  is logic high. B. The timing diagram is not drawn to scale.

Figure 36. Timing When V<sub>OUT1</sub> Faults Out



# **APPLICATION INFORMATION**

## **Input Capacitor**

For a typical application, an input bypass capacitor  $(0.1\mu F$  to  $1\mu F)$  is recommended. This capacitor filters any high-frequency noise generated in the line. For fast transient conditions where droop at the input of the LDO may occur because of high inrush current, it is recommended to place a larger capacitor at the input as well. The size of this capacitor depends on the output current and response time of the main power supply, as well as the distance to the V<sub>1</sub> pins of the LDO.

# **Output Capacitor**

As with most LDO regulators, the TPS702xx requires an output capacitor connected between OUT and GND to stabilize the internal control loop. The minimum recommended capacitance values are 10µF ceramic capacitors with an ESR (equivalent series resistance) between  $50m\Omega$  and  $2.5\Omega$  or  $6.8\mu$ F tantalum capacitors with ESR between  $250m\Omega$  and  $4\Omega$ . Solid tantalum electrolytic, aluminum electrolytic, and multilayer ceramic capacitors with capacitance values greater than  $10\mu$ F are all suitable, provided they meet the requirements described above. Larger capacitors provide a wider range of stability and better load transient response. Table 1 gives a partial listing of surface-mount capacitors suitable for use with the TPS702xx for fast transient response applications.

This information, along with the ESR graphs, is included to assist in selection of suitable capacitance for user applications. When necessary to achieve low height requirements along with high output current and/or high load capacitance, several higher ESR capacitors can be used in parallel to meet the guidelines above.

	•	•	-
VALUE	MANUFACTURER	MAXIMUM ESR	MFR PART NO.
22µF	Kemet	345mΩ	7495C226K0010AS
33µF	Sanyo	100mΩ	10TPA33M
47µF	Sanyo	100mΩ	6TPA47M
68µF	Sanyo	45mΩ	10TPC68M

Table 1 Pa	rtial Listing of	TPS702xx-Compatible	Surface-Mount	Canacitors
	$\Box$		5 Juliace-Would	Capacitors

## ESR and Transient Response

LDOs typically require an external output capacitor for stability. In fast transient response applications, capacitors are used to support the load current while the LDO amplifier is responding. In most applications, one capacitor is used to support both functions.

Besides its capacitance, every capacitor also contains parasitic impedances. These parasitic impedances are resistive as well as inductive. The resistive impedance is called *equivalent series resistance* (ESR), and the inductive impedance is called *equivalent series inductance* (ESL). The equivalent schematic diagram of any capacitor can therefore be drawn as shown in Figure 37.



Figure 37. ESR and ESL

In most cases one can neglect the effect of inductive impedance ESL. Therefore, the following application focuses mainly on the parasitic resistance ESR.



Figure 38 shows the output capacitor and its parasitic impedances in a typical LDO output stage.

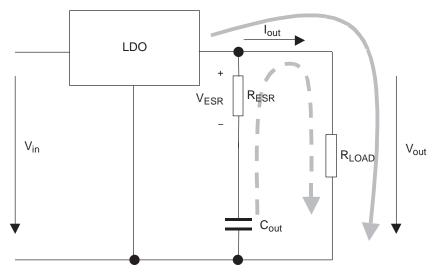


Figure 38. LDO Output Stage with Parasitic Resistances ESR

In steady state (dc state condition), the load current is supplied by the LDO (solid arrow) and the voltage across the capacitor is the same as the output voltage ( $V_{(CO)} = V_{OUT}$ ). This condition means no current is flowing into the C<sub>OUT</sub> branch. If I<sub>OUT</sub> suddenly increases (a transient condition), the following results occur:

- The LDO is not able to supply the sudden current need because of its response time (t<sub>1</sub> in Figure 39). Therefore, capacitor C<sub>OUT</sub> provides the current for the new load condition (dashed arrow). C<sub>OUT</sub> now acts like a battery with an internal resistance, ESR. Depending on the current demand at the output, a voltage drop occurs at R<sub>ESR</sub>. This voltage is shown as V<sub>ESR</sub> in Figure 38.
- When C<sub>OUT</sub> is conducting current to the load, initial voltage at the load will be V<sub>OUT</sub> = V<sub>(CO)</sub> V<sub>ESR</sub>. As a result of the discharge of C<sub>OUT</sub>, the output voltage V<sub>OUT</sub> drops continuously until the response time t<sub>1</sub> of the LDO is reached and the LDO resumes supplying the load. From this point, the output voltage starts rising again until it reaches the regulated voltage. This period is shown as t<sub>2</sub> in Figure 39.

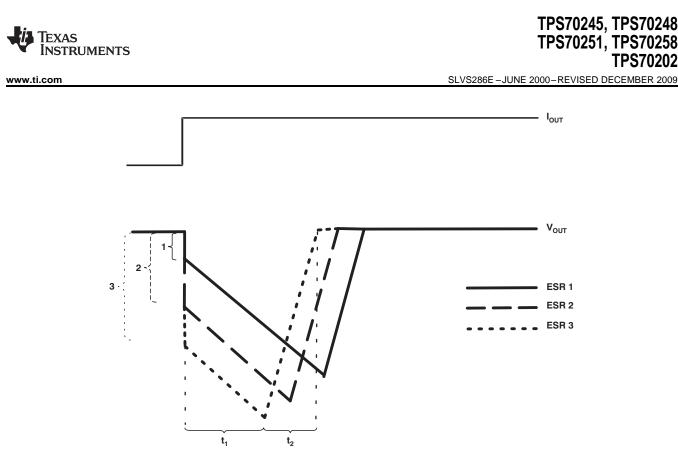


Figure 39. Correlation of Different ESRs and Their Influence on the Regulation of V<sub>0</sub> at a Load Step from Low-to-High Output Current

Figure 39 also shows the impact of different ESRs on the output voltage. The left brackets show different levels of ESRs where number 1 displays the lowest and number 3 displays the highest ESR.

From above, the following conclusions can be drawn:

- The higher the ESR, the larger the droop at the beginning of the load transient.
- The smaller the output capacitor, the faster the discharge time and the greater the voltage droop during the LDO response period.

## Conclusion

To minimize the transient output droop, capacitors must have a low ESR and be large enough to support the minimum output voltage requirement.

## Programming the TPS70202 Adjustable LDO Regulator

The output voltage of the TPS70202 adjustable regulators is programmed using external resistor dividers as shown in Figure 40.

Resistors R1 and R2 should be chosen for approximately a 50 $\mu$ A divider current. Lower value resistors can be used, but offer no inherent advantage and waste more power. Higher values should be avoided as leakage currents at the sense terminal increase the output voltage error. The recommended design procedure is to choose R2 = 30.1k $\Omega$  to set the divider current at approximately 50 $\mu$ A, and then calculate R1 using Equation 1:

$$R1 = \left(\frac{V_{OUT}}{V_{REF}} - 1\right) \times R2$$

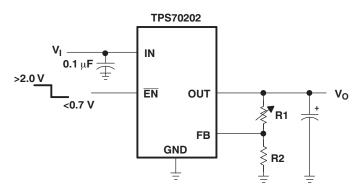
(1)

where:

•  $V_{RFF} = 1.224V$  typ (the internal reference voltage)

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OUTPUT VOLTAGE	
PROGRAMMING GUIDE	

OUTPUT VOLTAGE	R1	R2	UNIT
2.5 V	31.6	30.1	kΩ
3.3 V	51.1	30.1	kΩ
3.6 V	59.0	30.1	kΩ

Figure 40. TPS70202 Adjustable LDO Regulator Programming

### **Regulator Protection**

Both TPS702xx PMOS-pass transistors have built-in back diodes that conduct reverse currents when the input voltage drops below the output voltage (for example, during power-down). Current is conducted from the output to the input and is not internally limited. When extended reverse voltage is anticipated, external limiting may be appropriate.

The TPS702xx also features internal current limiting and thermal protection. During normal operation, the TPS702xx regulator 1 limits output current to approximately 1.6A (typ) and regulator 2 limits output current to approximately 750mA (typ). When current limiting engages, the output voltage scales back linearly until the overcurrent condition ends. While current limiting is designed to prevent gross device failure, care should be taken not to exceed the power dissipation ratings of the package. If the temperature of the device exceeds +150°C (typ), thermal-protection circuitry shuts it down. Once the device has cooled below +130°C (typ), regulator operation resumes.

## **Power Dissipation and Junction Temperature**

Specified regulator operation is assured to a junction temperature of +125°C; the maximum junction temperature should be restricted to +125°C under normal operating conditions. This restriction limits the power dissipation the regulator can handle in any given application. To ensure the junction temperature is within acceptable limits, calculate the maximum allowable dissipation,  $P_{D(max)}$ , and the actual dissipation,  $P_D$ , which must be less than or equal to  $P_{D(max)}$ .

The maximum-power-dissipation limit is determined using Equation 2:

$$\mathsf{P}_{\mathsf{D}(\mathsf{max})} = \frac{\mathsf{T}_{\mathsf{J}} \mathsf{max} - \mathsf{T}_{\mathsf{A}}}{\mathsf{R}_{\mathsf{\theta}\mathsf{J}\mathsf{A}}}$$

where:

- T<sub>Jmax</sub> is the maximum allowable junction temperature
- $R_{\theta JA}$  is the thermal resistance junction-to-ambient for the package; that is, 32.6°C/W for the 20-terminal PWP with no airflow
- T<sub>A</sub> is the ambient temperature

The regulator dissipation is calculated using Equation 3:

$$\mathbf{P}_{\mathsf{D}} = (\mathsf{V}_{\mathsf{I}} - \mathsf{V}_{\mathsf{O}}) \times \mathsf{I}_{\mathsf{O}}$$

Power dissipation resulting from quiescent current is negligible. Excessive power dissipation triggers the thermal protection circuit.

(2)

(3)



# **REVISION HISTORY**

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

C	hanges from Revision D (December, 2007) to Revision E	Page
•	Corrected typo in output current limit specification units	5
•	Deleted falling edge delay specification	6
•	Updated Fixed Voltage Version block diagram	7
•	Updated Adjustable Voltage Version block diagram	8



# PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TPS70202PWP	ACTIVE	HTSSOP	PWP	20	70	RoHS & Green	(6) NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70202	Samples
TPS70202PWPG4	ACTIVE	HTSSOP	PWP	20	70	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70202	Samples
TPS70202PWPR	ACTIVE	HTSSOP	PWP	20	2000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70202	Samples
TPS70245PWP	ACTIVE	HTSSOP	PWP	20	70	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70245	Samples
TPS70245PWPR	ACTIVE	HTSSOP	PWP	20	2000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70245	Samples
TPS70248PWP	ACTIVE	HTSSOP	PWP	20	70	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70248	Samples
TPS70248PWPR	ACTIVE	HTSSOP	PWP	20	2000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70248	Samples
TPS70251PWP	ACTIVE	HTSSOP	PWP	20	70	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70251	Samples
TPS70251PWPR	ACTIVE	HTSSOP	PWP	20	2000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70251	Samples
TPS70258PWP	ACTIVE	HTSSOP	PWP	20	70	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70258	Samples
TPS70258PWPG4	ACTIVE	HTSSOP	PWP	20	70	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70258	Samples
TPS70258PWPR	ACTIVE	HTSSOP	PWP	20	2000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	PT70258	Samples

<sup>(1)</sup> The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

<sup>(2)</sup> RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <= 1000ppm threshold. Antimony trioxide based flame retardants must also meet the <= 1000ppm threshold requirement.



# PACKAGE OPTION ADDENDUM

<sup>(3)</sup> MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

<sup>(4)</sup> There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

<sup>(5)</sup> Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

<sup>(6)</sup> Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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Texas

STRUMENTS

# TAPE AND REEL INFORMATION





### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

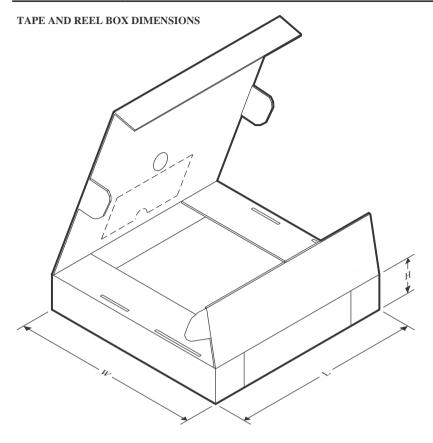


All dimensions are nomina		Dealers	Dine	600	Deal	Deal	4.0		1/0	<b>D</b> 4	14/	Dind
Device	Туре	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS70202PWPR	HTSSOP	PWP	20	2000	330.0	16.4	6.95	7.1	1.6	8.0	16.0	Q1
TPS70245PWPR	HTSSOP	PWP	20	2000	330.0	16.4	6.95	7.1	1.6	8.0	16.0	Q1
TPS70248PWPR	HTSSOP	PWP	20	2000	330.0	16.4	6.95	7.1	1.6	8.0	16.0	Q1
TPS70251PWPR	HTSSOP	PWP	20	2000	330.0	16.4	6.95	7.1	1.6	8.0	16.0	Q1
TPS70258PWPR	HTSSOP	PWP	20	2000	330.0	16.4	6.95	7.1	1.6	8.0	16.0	Q1



# PACKAGE MATERIALS INFORMATION

5-Dec-2023



*All	dimensions	are	nominal	
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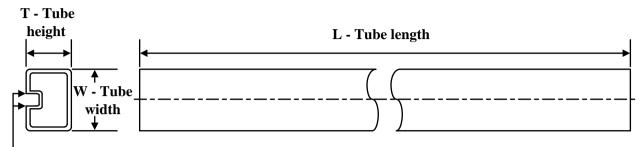
Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS70202PWPR	HTSSOP	PWP	20	2000	350.0	350.0	43.0
TPS70245PWPR	HTSSOP	PWP	20	2000	350.0	350.0	43.0
TPS70248PWPR	HTSSOP	PWP	20	2000	350.0	350.0	43.0
TPS70251PWPR	HTSSOP	PWP	20	2000	350.0	350.0	43.0
TPS70258PWPR	HTSSOP	PWP	20	2000	350.0	350.0	43.0

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# TUBE



# - B - Alignment groove width

### \*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	Τ (μm)	B (mm)
TPS70202PWP	PWP	HTSSOP	20	70	530	10.2	3600	3.5
TPS70202PWPG4	PWP	HTSSOP	20	70	530	10.2	3600	3.5
TPS70245PWP	PWP	HTSSOP	20	70	530	10.2	3600	3.5
TPS70248PWP	PWP	HTSSOP	20	70	530	10.2	3600	3.5
TPS70251PWP	PWP	HTSSOP	20	70	530	10.2	3600	3.5
TPS70258PWP	PWP	HTSSOP	20	70	530	10.2	3600	3.5
TPS70258PWPG4	PWP	HTSSOP	20	70	530	10.2	3600	3.5

# **PWP 20**

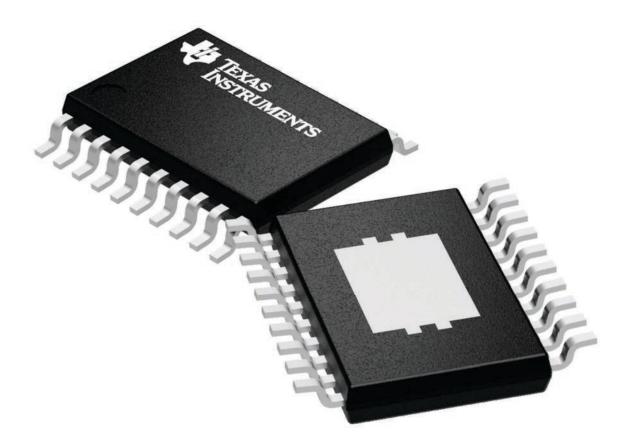
# **GENERIC PACKAGE VIEW**

# HTSSOP - 1.2 mm max height

6.5 x 4.4, 0.65 mm pitch

SMALL OUTLINE PACKAGE

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.





PWP (R-PDSO-G20)

PowerPAD<sup>™</sup> PLASTIC SMALL OUTLINE



All linear dimensions are in millimeters. NOTES: Α.

- Β. This drawing is subject to change without notice.
- Body dimensions do not include mold flash or protrusions. Mold flash and protrusion shall not exceed 0.15 per side. C.
- This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad D.
- Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>. E. See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions. E. Falls within JEDEC MO-153

PowerPAD is a trademark of Texas Instruments.



#### PowerPAD<sup>™</sup> SMALL PLASTIC OUTLINE PWP (R-PDSO-G20)

### THERMAL INFORMATION

This PowerPAD<sup>™</sup> package incorporates an exposed thermal pad that is designed to be attached to a printed circuit board (PCB). The thermal pad must be soldered directly to the PCB. After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.



NOTE: A. All linear dimensions are in millimeters

A Exposed tie strap features may not be present.

PowerPAD is a trademark of Texas Instruments





NOTES:

Α.

B. This drawing is subject to change without notice.

All linear dimensions are in millimeters.

- C. Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
- D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002, SLMA004, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <http://www.ti.com>. Publication IPC-7351 is recommended for alternate designs.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.
- F. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.



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