

Selecting Electrolytic Bus Capacitor for Universal input (85-V to 265-V RMS) Low Power Adapters ($P_{in} < 75\text{-W}$)

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1 Introduction

In the past designers would have selected the converter's bus capacitor (C_{bus}) using various approximations and "rules of thumb" which are not particularly accurate.

This application note presents a quick and reliable method for selecting the smallest electrolytic input bus capacitors that will provide the desired service life in ac-to-dc converters with capacitive input filters.

We will consider a quasi resonant flyback converter (Figure 1). Since most inexpensive simulator tools do not allow use of subscripts, so subscripts were intentionally left out of this application note.

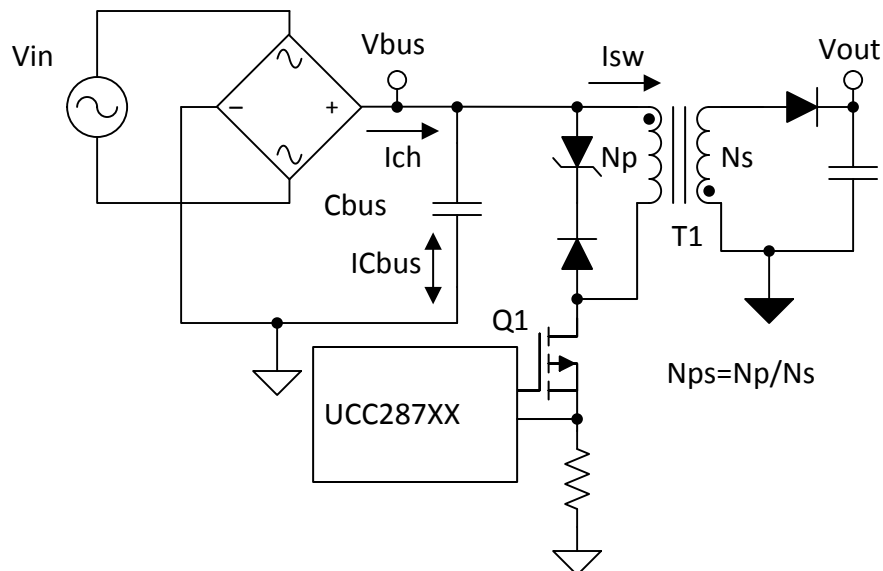


Figure 1. Simplified Low Power AC-to-DC Adapter Flyback Schematic

The bus capacitor C_{bus} , sometime referred to as the bulk capacitor, stores and delivers energy (w) to the power system.

$$w = \frac{1}{2} C_{bus} \times V_{bus}^2 \quad (1)$$

Capacitor C_{bus} is charged every half line cycle by low frequency current and discharged continuously by the high-frequency current pulses drawn by the converter. This action results in a low frequency ac current (I_{lf}) and a high frequency ac current (I_{hf}) passing through C_{bus} . This application brief will use circuit simulation to obtain the RMS current of I_{lf} and calculate I_{hf} going through C_{bus} .

$$I_{Cbus} = I_{lf} + I_{hf} \quad (2)$$

The bus capacitor (C_{bus}) selection algorithm consists of few simulation iterations of a circuit model based on the output power requirements (P_{out}), assumed efficiency (η), and the duty cycle of the converter (D) this algorithm enables selection of capacitors that will provide the service life required by the application.

The algorithm will be illustrated for the converter with the following specifications:

- $P_{out} = 45\text{-W}$ output power
- $V_{out} = 20\text{-V}$, output voltage
- $V_{in} = 85\text{-}265\text{-V}$ RMS, input voltage
- $\eta = 90\%$
- $V_{bus(\min)} = 75\text{ v}$, lowest allowable dc bus voltage
- Service life: 2000 hours @full load, 100v 50hz input, 80°C internal ambient temperature.
- $f_{sw} = 100\text{ khz}$, converter switching frequency @ highest I_{lf} and I_{hf}
- $D_{\max} = 50\%$, maximum duty cycle

Selecting the bus capacitor (C_{bus}):

1. Select a bus capacitor voltage rating greater than the maximum bus voltage ($V_{bus(\max)}$).

$V_{bus(\max)}$ can be calculated on the maximum RMS input voltage ($V_{in(\max)}$) using equation 3. For this design the maximum bus voltage would be 375-V the voltage rating of C_{bus} needs to be rated for higher voltage than calculated, so 400-V is appropriate for this design.

$$V_{bus(\max)} = V_{in(\max)} \times \sqrt{2} = 265V \times \sqrt{2} = 375V \quad (3)$$

2. Assuming a minimum dc bus voltage of 75-V, calculate the average input current of the converter and select an initial bus capacitor ($C_{bus(\text{init})}$) value based on 120uF/ampere dc:

$$C_{bus(\text{init})} = \frac{120\mu F}{1A} \times \frac{P_{out}}{V_{bus(\min)} \times \eta} = \frac{120\mu F}{1A} \times \frac{45W}{75V \times 0.9} \approx 80\mu F \quad (4)$$

3. We select the next standard value capacitor equal to or greater than $C_{bus(\text{init})}$

$$C_{bus} = 82\mu F \quad (5)$$

4. Use your favorite circuit simulator and the model presented in figure 2 to extract the maximum C_{bus} low frequency current (I_{lf}), which occurs at the maximum output power and minimum input voltage. In order to avoid division by zero at divider on C_{bus} should be set to a positive voltage (say 70-V) and the simulation run until the circuit reaches steady-state.

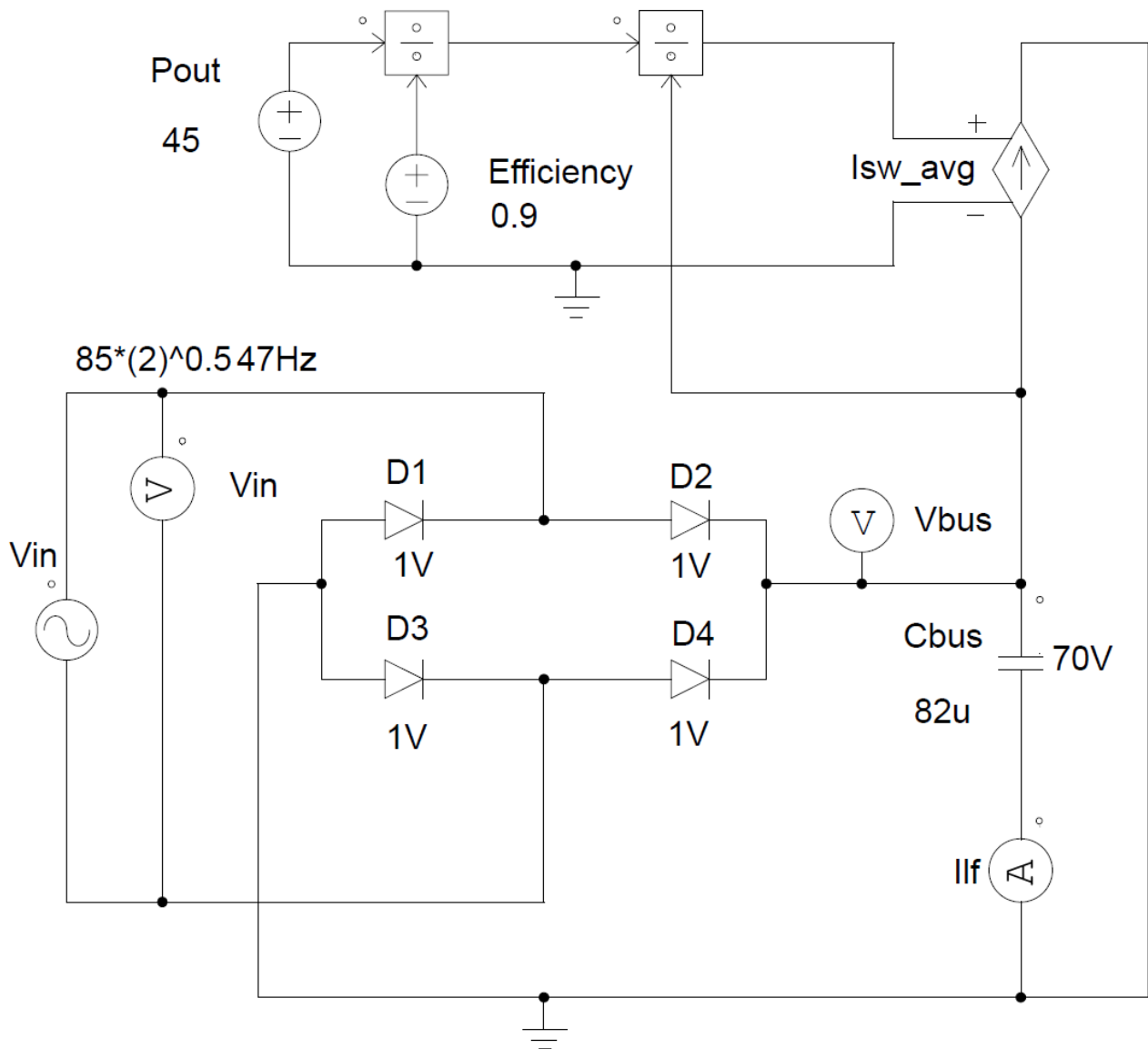


Figure 2. Cbus Low Frequency Current (Ilf) Simulation Model

The 82uf capacitor yields a minimum bus voltage of 71.6 v, which is below the minimum 75v bus voltage requirement, so a larger capacitance value must be selected.

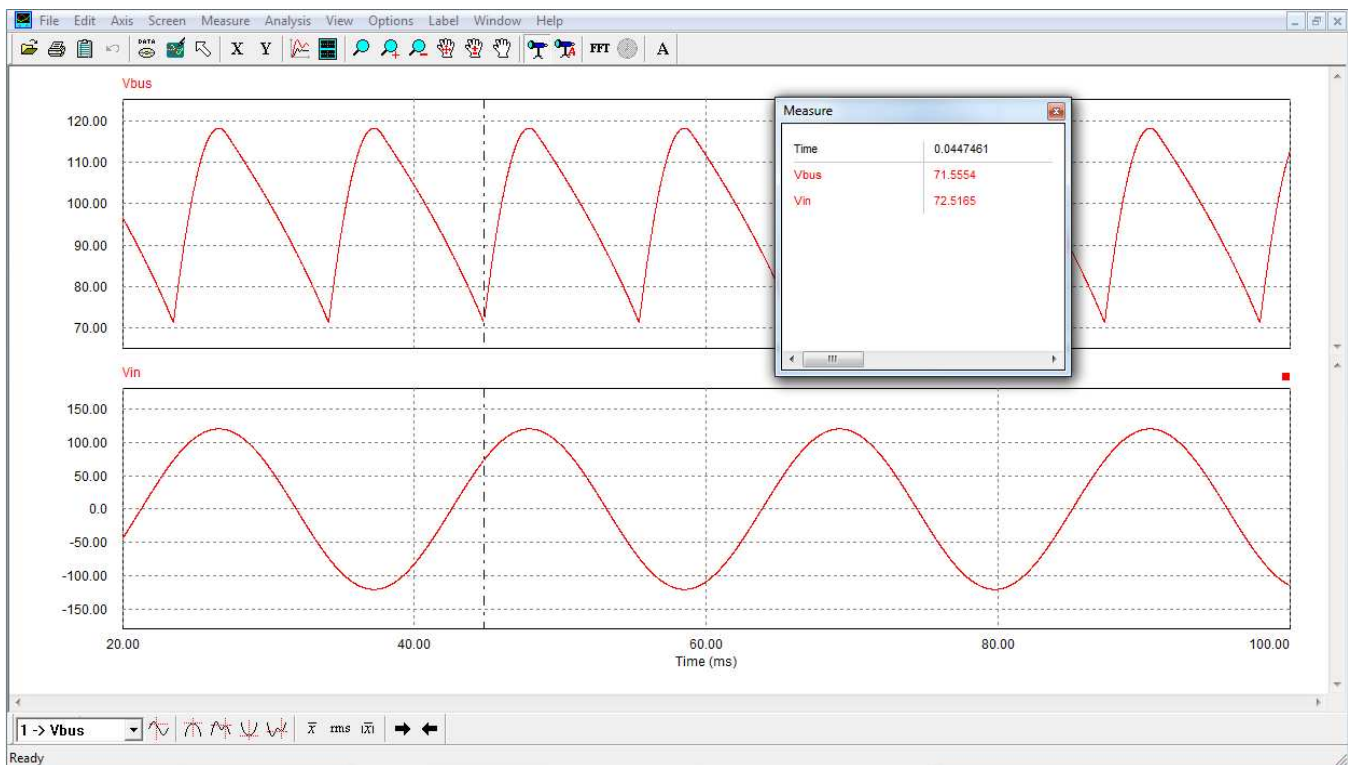


Figure 3. first Vbus Ripple Voltage Simulation

5. Selecting two 47uf capacitors in parallel for a total of 94 uf yields a minimum bus voltage of 78-V and a total (I_{lft}) of 924 mA, 100-Hz RMS low frequency current , (462 mA of low frequency current (I_{lf}) through each C_{bus} capacitor).

$$I_{lft} \approx 924mA \tag{6}$$

$$I_{lf} \approx \frac{924}{2} mA = 462mA \tag{7}$$

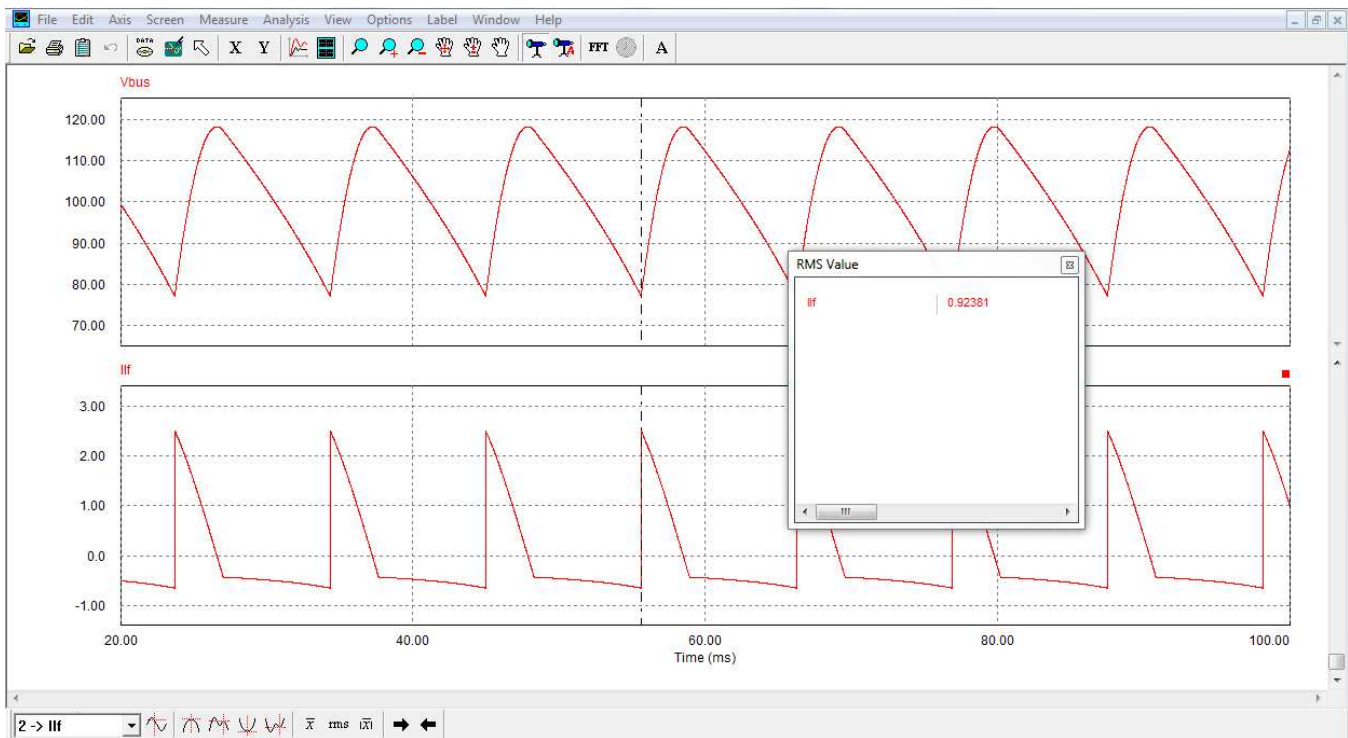


Figure 4. Ripple Voltage Simulation, Cbus = 2x47uf

Having two capacitors in parallel provides the opportunity to create a differential mode EMI π filter by inserting an RF filter inductor (L_f) in between the two caps (figure 5), which will force the high-frequency current to flow into C_{bus} , but have little impact on the sharing of low frequency current between the two capacitors.

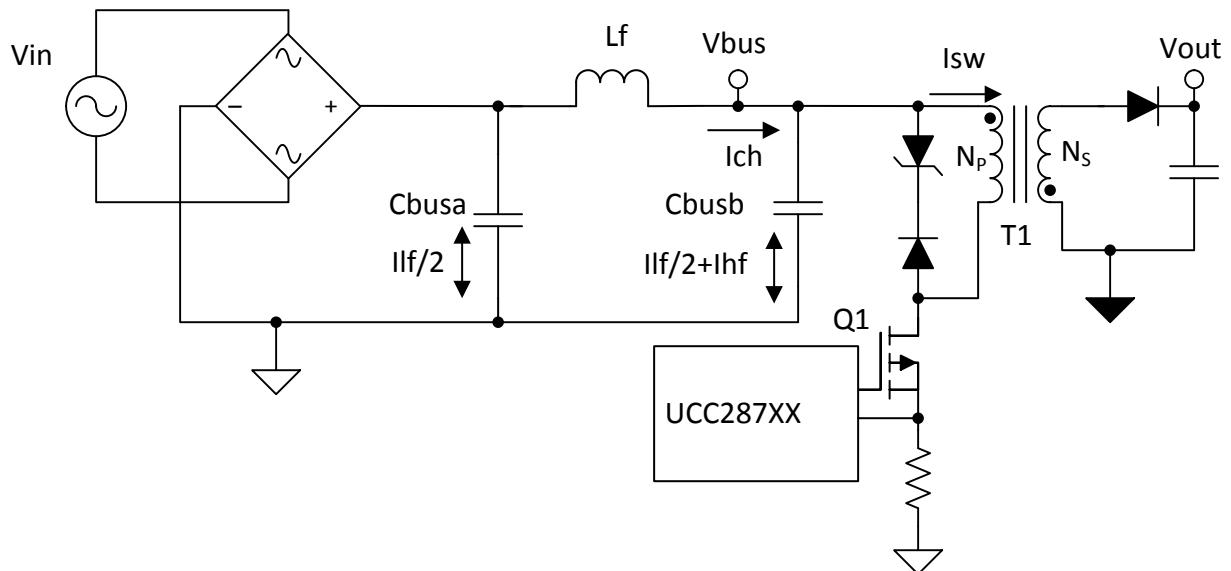


Figure 5. low power offline power adaptor.

The maximum high frequency RMS current (I_{hf}) going through the bus capacitor (C_{busb}) in this example can be calculated based on p_{out} , $V_{bus(min)}$, estimated efficiency (η), and knowing the converters maximum duty cycle. for this design example the maximum duty cycle was limited to 50%.

$$D_{max} = 0.5 \quad (8)$$

First calculate the peak switch current (I_{swpk}):

$$I_{swpk} = \frac{P_{out} \times 2}{V_{bus(min)} \times Efficiency \times D_{max}} = \frac{45W \times 2}{78V \times 0.9 \times 0.5} \approx 2.56 \quad (9)$$

With I_{swpk} the I_{hf} RMS current can be calculated:

$$I_{hf} = \sqrt{\left(I_{swpk} \times \sqrt{\frac{D_{max}}{3}} \right)^2 - \left(I_{swpk} \times \frac{D_{max}}{2} \right)^2} \quad (10)$$

$$I_{hf} = \sqrt{\left(2.56A \times \sqrt{\frac{0.5}{3}} \right)^2 - \left(2.56 \times \frac{0.5}{2} \right)^2} = 826mA \quad (11)$$

6. Once the simulation is complete and you have the simulated value of I_{lf} and calculated I_{hf} for the bus capacitor/s used in your design, extract from the datasheet of your favorite electrolytic capacitors family the rated 120 Hz ripple current (I_{lf}), the frequency ripple current coefficient (K) and the rated load life (L) of 47- μ f, 400-V at the current I_{lf} and rated ambient temperature. For our example, we select an 47- μ f capacitor with a 100-kHz ripple current rating (I_{lf}) of 1.2-A @85° C, a frequency ripple current ripple coefficient K of 2 and load life L of 2000 hours @85°C.
7. Calculate the effective RMS current (I_{eff}) in the bus capacitor using equation 4 (see appendix for derivation):

$$I_{eff} = \sqrt{I_{lf}^2 + \frac{I_{hf}^2}{K^2}} = \sqrt{(462mA)^2 + \left(\frac{826mA}{2}\right)^2} \approx 620mA \quad (12)$$

8. The load life L_x of the capacitor can be calculated using equation 13. Please note there is a derivation of the formula in the appendix at the end of the application note. in our design example we are calculating L_x based on:
 - T_{max} is the rated ambient temperature from the datasheet (85° C for our case)
 - ΔT_{max} is the maximum allowed hotspot temperature rise above the ambient T_{max} (typically 5° C for 105° C rated capacitors, 15° C for 85° C rated capacitors - contact the manufacturer for more specific information)
 - L is the rated load life at @ the rated ambient temperature T_{max} (2000 hrs. for our case)
 - T_x is the operating ambient temperature (80°C for our case)
 - In our example the life of the capacitor is calculated to be 2144 hours
 - If this service life is not acceptable, the next larger value or higher ambient temperature (105oc instead of 85oc) can be selected – the change will have size and/or cost consequences.

$$L_x = L \times 2^{\left[\frac{T_{max} - T_x + \Delta T_{max} \times \left(1 - \frac{I_{eff}^2}{I_{lf}^2}\right)}{10} \right]} = 2000hr \times 2^{\left[\frac{85^\circ C - 80^\circ C + 5^\circ C \times \left(1 - \frac{(620mA)^2}{(462mA)^2}\right)}{10} \right]} = 2144hrs \quad (13)$$

This application note demonstrated with the use of proper simulation and modeling a bus capacitor or capacitors can be more accurately selected to meet your design requirements in low power offline flyback converters. This technique gives a more accurate prediction of the low and high frequency bus capacitor RMS current that can be used to select a better bus capacitor for the design with a longer life.

2 Appendix: Formulas Derivation.

1. Effective RMS current (I_{eff}):

Since the capacitor's maximum internal temperature rise above the ambient is the same for low and high-frequency ripple current power dissipation must be equal for both:

$$ESR_{LF} \times I_{LF}^2 = ESR_{HF} \times I_{HF}^2 \quad (14)$$

$$\frac{I_{HF}}{I_{LF}} = K \quad (15)$$

(Where k is the frequency ripple current coefficient provided by the datasheet)

Therefore, the high frequency ESR is:

$$ESR_{HF} = \frac{I_{LF}}{K^2} \quad (16)$$

The equivalent RMS current for the mix of low and high-frequency currents will be:

$$I_{eff}^2 \times ESR_{LF} = I_{LFx}^2 \times ESR_{LF} + I_{HFx}^2 \times \frac{ESR_{LF}}{K^2} \quad (17)$$

$$I_{eff}^2 = \sqrt{\frac{I_{HFx}^2}{K^2} + I_{LFx}^2} \quad (18)$$

2. Life Expectancy Calculation:

The life expectancy vs. temperature of electrolytic capacitors follows arrhenius' law, i.e. it decreases by a factor of 2 for every 10°C increase in temperature. most caps manufacturers specify the internal hot spot ΔT of 5° c and 15° c respectively for capacitors rated 105° C and 85° C ambient temperature.

Defining:

- T_{max} Rated ambient temperature
- ΔT_{max} Maximum allowed internal hotspot temperature rise above Tmax
- T_x Operating ambient temperature
- ΔT_x Operating hotspot temperature rise above T_x
- L Rated load life at T_{max}
- L_x Load life at T_x

$$\Delta T_x = \Delta T_{max} \times \left(\frac{I_{eff}}{I_{LF}}\right)^2 \quad (19)$$

$$L_x = L \times 2 \frac{[T_{max} + \Delta T_{max} - (T_x + \Delta T_x)]}{10} \quad (20)$$

$$L_x = L \times 2 \frac{[T_{max} + \Delta T_{max} \times (1 - \frac{I_{eff}^2}{I_{LF}^2})]}{10} \quad (21)$$

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