

DLP991U Industrial Digital Micromirror Device

1 Features

- High resolution 4096 × 2176 micromirror array
	- > 8.9 million micromirrors
	- 5.4µm micromirror pitch
	- 0.99" micromirror array diagonal
	- ±12° micromirror tilt relative to flat S
	- Designed for corner illumination
	- Integrated micromirror driver circuitry
- Designed for visible light use (400nm to 800nm)
	- 97% window transmission (single pass, through two window surfaces)
	- 89% micromirror reflectivity
	- 79% average photopic weighted diffraction and 80% unweighted (410nm–800nm) efficiency (f/2.4) per photopic luminous efficiency—CIE 086-1990
	- 90% on-state array fill factor

2 Applications

- **Industrial**
	- [Direct imaging lithography](https://www.ti.com/dlp-chip/3d-printing-direct-imaging/overview.html)
	- [3D printing](https://www.ti.com/dlp-chip/3d-printing-direct-imaging/overview.html)
	- [Machine vision and quality control](https://www.ti.com/dlp-chip/3d-scan-machine-vision/overview.html)
	- Laser marking and repair
- Medical
	- Ophthalmology
	- [3D scanners for limb and skin measurement](https://www.ti.com/dlp-chip/3d-scan-machine-vision/overview.html)
- HyperSpectral imaging/scanning
- Displays
	- [3D imaging microscopes](https://www.ti.com/dlp-chip/3d-scan-machine-vision/overview.html)
	- [Augmented reality and information overlay](https://www.ti.com/solution/augmented-reality-glasses?keyMatch=DLP%20AUGMENTED%20REALITY)

3 Description

Featuring over 8.9 million micromirrors, the highresolution DLP991U digital micromirror device (DMD) is a spatial light modulator (SLM) that modulates the amplitude, direction, or phase of incoming light. This advanced light control technology has numerous applications in the industrial, medical, and consumer markets. The streaming nature of the DLP991U and its DLPC964 controller make it ideally suited for exceptionally high-speed continuous data streaming for direct imaging (LDI) applications. The DMD enables large 3D print build sizes and ultra-fine resolutions for various 3D printing applications. The high resolution provides a direct benefit to the scanning of larger objects in 3D machine vision applications.

Device Information

(1) For more information, see the *Mechanical, Packaging, and Orderable* addendum.

Simplified Application

Table of Contents

4 Pin Configuration and Functions

CAUTION

To ensure reliable, long-term operation of the DLP991U DMD, it is critical to properly manage the layout and operation of the signals identified in the table below. For specific details and guidelines, refer to the *PCB Design Requirements for TI DLP® Standard SST Digital Micromirror Devices***.**

[DLP991U](https://www.ti.com/product/DLP991U)

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Table 4-1. Package Pinout

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(1) I = Input, O = Output, P = Power, G = Ground, NC = No Connect

5 Specifications

5.1 Absolute Maximum Ratings

Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

(1) All voltage values are with respect to the ground terminals (V_{SS}). The following required power supplies must be connected for proper DMD operation: V_{DD} , V_{DDA} , V_{OFFSET} , V_{BIAS} , and V_{RESET} . All V_{SS} connections are also required.

(2) V_{OFFSET} supply transients must fall within specified voltages.

 (3) Exceeding the recommended allowable absolute voltage difference between V_{DDA} and V_{DD} may result in excessive current draw.

(4) Exceeding the recommended allowable absolute voltage difference between V_{BIAS} and V_{OFFSET} may result in excessive current draw.
(5) Exceeding the recommended allowable absolute voltage difference between V_{BIAS} a

(5) Exceeding the recommended allowable absolute voltage difference between V_{BIAS} and V_{RESET} may result in excessive current draw.
(6) This maximum input voltage rating applies when each input of a differential pair i

This maximum input voltage rating applies when each input of a differential pair is at the same voltage potential. LVDS differential inputs must not exceed the specified limit or damage may result to the internal termination resistors.

(7) Differential inputs must not exceed the specified limit or damage may result to the internal termination resistors. Specification applies to both the high speed serial interface (HSSI) and the low speed interface (LSI).

(8) The array temperature cannot be measured directly and must be computed analytically from the temperature measured at the test point (TP1) shown in [Figure 6-1](#page-25-0) and the package thermal resistances using the calculation in [Section 6.6](#page-25-0).

(9) Refer to [Section 6.6](#page-25-0) for the calculation.

5.2 Storage Conditions

Applicable for the DMD as a component or non-operating in a system.

5.3 ESD Ratings

(1) JEDEC document JEP155 states that 500V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250V CDM allows safe manufacturing with a standard ESD control process.

5.4 Recommended Operating Conditions

Over operating free-air temperature range and supply voltages (unless otherwise noted) (1)

5.4 Recommended Operating Conditions (continued)

Over operating free-air temperature range and supply voltages (unless otherwise noted) (1)

(1) [Section 5.4](#page-9-0) are applicable after the DMD is installed in the final product.

- (2) All power supply connections are required to operate the DMD: V_{DD} , V_{DDA} , V_{OFSET} , V_{BIAS} , and V_{RESET} . All V_{SS} connections are required to operate the DMD.
- (3) All voltage values are with respect to the V_{SS} ground pins.
- (4) V_{OFFSET} supply transients must fall within specified max voltages.
(5) To prevent excess current, the supply voltage delta | V_{DDA} V_{DD} |
- To prevent excess current, the supply voltage delta $|V_{DDA} V_{DD}|$ must be less than specified limit.
- (6) To prevent excess current, the supply voltage delta $|V_{BIAS} V_{OFFSET}|$ must be less than specified limit.
(7) LVCMOS input pin is DMD DEN ARSTZ.
- LVCMOS input pin is DMD_DEN_ARSTZ.
- (8) See the high-speed serial interface (HSSI) timing requirements in [Section 5.8.](#page-13-0)
- (9) See the low-speed interface (LSIF) timing requirements in [Section 5.8.](#page-13-0)
- (10) Simultaneous exposure of the DMD to the maximum [Section 5.4](#page-9-0) for temperature and UV illumination will reduce device lifetime.
- (11) The array temperature cannot be measured directly and must be computed analytically from the temperature measured at test point (TP1) shown in [Figure 6-1](#page-25-0), and the package thermal resistances using the [calculation.](#page-25-0)
- (12) The maximum operational array temperature should be derated based on the micromirror landed duty cycle that the DMD experiences in the end application. Refer to [Section 6.8.1](#page-29-0) for a definition of micromirror landed duty cycle.
- (13) Long-term is defined as the usable life of the device.
- (14) Short-term is defined as the cumulative time over the usable life of the device.
- (15) The maximum optical power that can be incident on the DMD is limited by the maximum optical power density for each wavelength range specified and the micromirror array temperature T_{ARRAY} .
- (16) Refer to [Section 6.6](#page-25-0) for calculation examples.
- (17) Refer to [Section 6.7](#page-27-0) for calculation examples.

- (18) Optimal, long-term performance and optical efficiency of the digital micromirror device (DMD) can be affected by various application parameters, including illumination spectrum, illumination power density, micromirror landed duty-cycle, ambient temperature (storage and operating), DMD temperature, ambient humidity (storage and operating), and power on or off duty-cycle. TI recommends that application-specific effects be considered as early as possible in the design cycle.
- (19) This is the illumination power density and illumination total power on the DMD and does not include illumination overfill of the DMD device outside the active array.
- (20) Landed Duty Cycle refers to the percentage of time an individual micromirror spends landed in one state (12 $^{\circ}$ or -12°) versus the opposite state (–12° or 12°). 50% equates to a 50/50 duty cycle where the mirror has been landed 50% in the on-state and 50% in the off-state. See [Section 7.8](#page-29-0) for more information on landed duty cycle.

Figure 5-1. Maximum Recommended Array Temperature—Derating Curve for 410nm–800nm (Visible Wavelengths)

5.5 Thermal Information

(1) The DMD is designed to conduct absorbed and dissipated heat to the back of the package where it can be removed by an appropriate heat sink. The heat sink and cooling system must be capable of maintaining the package within the specified operational temperatures. The total heat load on the DMD is largely driven by the incident light absorbed by the active area; although other contributions include light energy absorbed by the window aperture and electrical power dissipation of the array. Optical systems should be designed to minimize the light energy falling outside the window clear aperture since any additional thermal load in this area can significantly degrade the reliability of the device. Refer to [Figure 6-1](#page-25-0) for TP1 location.

5.6 Electrical Characteristics

Over operating free-air temperature range and supply voltages (unless otherwise noted)

5.6 Electrical Characteristics (continued)

Over operating free-air temperature range and supply voltages (unless otherwise noted)

(1) Device electrical characteristics are over Recommended Operating Conditions unless otherwise noted.

(2) All power supply connections are required to operate the DMD: V_{DD} , V_{DDA} , V_{OFSET} , $V_{B|AS}$, and V_{RESET} . All V_{SS} connections are required to operate the DMD.

(3) All voltage values are with respect to the ground pins (V_{SS}) .

(4) To prevent excess current, the supply voltage delta $|\overrightarrow{V}_{DDA} - V_{DD}|$ must be less than specified limit.

(5) To prevent excess current, the supply voltage delta $|V_{\text{BIAS}} - V_{\text{OFFSET}}|$ must be less than specified limit.

(6) Power dissipation based upon 1 Phased reset, 1 array load, and 1 global reset in 90μs

(7) The LVCMOS input specification is for pin DMD_DEN_ARSTZ.

(8) The LVCMOS output specification is for pins LS_RDATA_A and LS_RDATA_B.

(9) Refer to [Figure 5-11,](#page-17-0) Receiver Eye Mask (1e-12 BER).

(10) Defined in [Section 5.4](#page-9-0).

5.7 Switching Characteristics

Over operating free-air temperature range and supply voltages (unless otherwise noted)

EXAS **INSTRUMENTS**

5.7 Switching Characteristics (continued)

Over operating free-air temperature range and supply voltages (unless otherwise noted)

(1) See Figure 5-2.

5.8 Timing Requirements

Over operating free-air temperature range and supply voltages (unless otherwise noted)

(1) See [Figure 5-9](#page-16-0) for rise time and fall time for LVCMOS.

 (2) See [Figure 5-5](#page-14-0) for rise time and fall time for LSIF.

 (3) See [Figure 5-4](#page-14-0) for setup and hold time for LSIF.

(4) See [Figure 5-10](#page-16-0) for rise time and fall time for HSSI.

(2)

$$
V_{LVDS \, (max)} = V_{CM \, (max)} + \left| \frac{1}{2} \times V_{ID \, (max)} \right|
$$
\n
$$
V_{LVDS \, (min)} = V_{CM \, (min)} - \left| \frac{1}{2} \times V_{ID \, (max)} \right|
$$
\n(1)

Figure 5-4. LSIF Timing Requirements

Figure 5-5. LSIF Rise, Fall Time Slew

Figure 5-8. LVCMOS Input Hysteresis

Figure 5-10. HSSI Waveform Requirements

Figure 5-11. HSSI Eye Characteristics

Figure 5-12. HSSI CLK Characteristics

5.9 System Mounting Interface Loads

(1) Combined loads of the thermal and electrical interface areas in excess of the Datum A load shall be evenly distributed outside the Datum A area (1334+200 – Datum A), or the combined loads of the thermal and electrical areas reduced.

(2) Uniformly distributed within area shown in Figure 5-13.

Figure 5-13. System Mounting Interface Loads

5.10 Micromirror Array Physical Characteristics

(1) See [Figure 5-14](#page-20-0).
(2) The structure and

The structure and qualities of the border around the active array includes a band of partially functional micromirrors called the POM. These micromirrors are structurally and/or electrically prevented from tilting toward the bright or ON state, but still require an electrical bias to tilt toward OFF.

Figure 5-14. Micromirror Array Physical Characteristics

5.11 Micromirror Array Optical Characteristics

(1) Measured relative to the plane formed by the overall micromirror array.

- (2) Additional variation exists between the micromirror array and the package datums.
- (3) Represents the landed tilt angle variation relative to the nominal landed tilt angle.
- (4) Represents the variation that can occur between any two individual micromirrors, located on the same device or located on different devices.
- (5) For some applications, it is critical to account for the micromirror tilt angle variation in the overall system optical design. With some system optical designs, the micromirror tilt angle variation within a device may result in perceivable non-uniformities in the light field reflected from the micromirror array. With some system optical designs, the micromirror tilt angle variation between devices may result in colorimetry variations, system efficiency variations or system contrast variations.
- (6) The time required for a micromirror to nominally transition from one landed state to the opposite landed state.
- (7) The minimum time between successive transitions of a micromirror at the end of a Mirror Clocking Pulse to the beginning of the next Mirror Clocking Pulse.
- (8) Measured relative to the package datums 'B' and 'C'.
- (9) The minimum or maximum DMD optical efficiency observed in a specific application depends on numerous application-specific design variables, such as:
	- Illumination wavelength, bandwidth/line-width, degree of coherence
	- Illumination Angle, plus angle tolerance
	- Illumination and projection aperture size, and location in the system optical path
	- Illumination overfill of the DMD micromirror array
	- Aberrations present in the illumination source and/or illumination path
	- Aberrations present in the projection path

The specified nominal DMD optical efficiency is based on the following use conditions:

- Visible illumination (400 to 800 nm)
- Input illumination optical axis oriented at 24° relative to the window normal
- Projection optical axis oriented at 0° relative to the window normal
- $f/3$ illumination aperture
- $f/2.4$ projection aperture

Based on these use conditions, the nominal DMD optical efficiency results from the following four components:

- Micromirror array fill factor: nominally 90%
- Micromirror array diffraction efficiency: nominally 86%
- Micromirror surface reflectivity: nominally 88%
- Window transmission: nominally 97% (single pass, through two surface transitions)
- (10) Does not account for the effect of micromirror switching duty cycle, which is application dependent. Micromirror switching duty cycle represents the percentage of time that the micromirror is actually reflecting light from the optical illumination path to the optical projection path. This duty cycle depends on the illumination aperture size, the projection aperture size, and the micromirror array update rate.
- (11) Non-operating micromirror is defined as a micromirror that is unable to transition nominally from the "OFF" position to the "ON" position or vice versa.

5.12 Window Characteristics

(1) Single-pass through both surfaces and glass

(2) AOI—The angle of incidence is the angle between an incident ray and the normal to a reflecting or refracting surface.

5.13 Chipset Component Usage Specification

Reliable function and operation of the DLPC991U DMD requires that it be used in conjunction with the other components of the applicable DLP chipset, including those components that contain or implement TI DMD control technology. TI DMD control technology is the TI technology and devices for operating or controlling a DLP DMD.

6 Detailed Description

6.1 Overview

The DLP991U DMD is a 0.99-inch diagonal spatial light modulator that consists of an array of highly reflective aluminum micromirrors. The DMD is an electrical input, optical output micro-electrical-mechanical system (MEMS). The input electrical data interface is a differential high-speed serial interface (HSSI). The DMD consists of a two-dimensional array of 1-bit CMOS memory cells. The array is organized in a grid of M memory cell columns by N memory cell rows. Refer to [Figure 5-14.](#page-20-0) The positive or negative deflection angle of the micromirrors can be individually controlled by writing a '1' or a '0' to each memory cell thereby changing the address voltage of underlying CMOS addressing circuitry.

To ensure reliable operation, the DLP991U DMD must always be used with the TI-provided DLPC964 industrial controller.

6.2 Functional Block Diagram

For pin details on Channels A, B, C, and D, refer to [Section 4](#page-2-0) and HSSI Interface section of [Section 5.8](#page-13-0). Channels C and D are connected identically as A and B, but were omitted from this image for clarity.

6.3 Feature Description

6.3.1 Power Interface

The DLP991U DMD requires five DC voltages for proper operation: V_{DD}, V_{DDA}, V_{OFFSET}, V_{RESET}, and V_{BIAS}. VDD/VDDA power inputs require a 1.9V power supply. V_{OFFSET} (10V), V_{RESET} (-14V), and V_{BIAS} (18V) are supplied to the DMD to enable micromirror actuation control.

6.3.2 Timing

The data sheet provides timing at the device pin. For output timing analysis, the tester pin electronics and its transmission line effects must be considered. Timing reference loads are not intended as a precise representation of any particular system environment or depiction of the actual load presented by a production test. System designers should use IBIS or other simulation tools to correlate the timing reference load to a system environment. The load capacitance value stated is only for characterization and measurement of AC timing signals. This load capacitance value does not indicate the maximum load the device is capable of driving.

6.4 Device Functional Modes

DMD functional modes are controlled by the display controller. See the *[DLPC964 Digital Micromirror Device](https://www.ti.com/lit/pdf/DLPS167) [Controller Data Sheet](https://www.ti.com/lit/pdf/DLPS167)* or contact a TI applications engineer for more information.

6.5 Optical Interface and System Image Quality Considerations

Note TI assumes no responsibility for image quality artifacts or DMD failures caused by optical system operating conditions exceeding limits described previously.

TI assumes no responsibility for end-equipment optical performance. Achieving the desired end-equipment optical performance involves making trade-offs between numerous component and system design parameters. Optimizing system optical performance and image quality strongly relate to optical system design parameter trades. Although it is not possible to anticipate every conceivable application, projector image quality and optical performance is contingent on compliance to the optical system operating conditions described in the following sections.

6.5.1 Numerical Aperture and Stray Light Control

The angle defined by the numerical aperture of the illumination and projection optics at the DMD optical area should be the same. This angle should not exceed the nominal device micromirror tilt angle unless appropriate apertures are added in the illumination and/or projection pupils to block out flat-state and stray light from the projection lens. The micromirror tilt angle defines DMD capability to separate the "ON" optical path from any other light path, including undesirable flat-state specular reflections from the DMD window, DMD border structures, or other system surfaces near the DMD such as prism or lens surfaces. If the numerical aperture exceeds the micromirror tilt angle, or if the projection numerical aperture angle is more than two degrees larger than the illumination numerical aperture angle, objectionable artifacts in the display's border and/or active area could occur.

6.5.2 Pupil Match

TI's optical and image quality specifications assume that the exit pupil of the illumination optics is nominally centered within 2° of the entrance pupil of the projection optics. Misalignment of pupils can create objectionable artifacts in the display's border and/or active area, which may require additional system apertures to control, especially if the numerical aperture of the system exceeds the pixel tilt angle.

6.5.3 Illumination Overfill

The active area of the device is surrounded by an aperture on the inside DMD window surface that masks structures of the DMD chip assembly from normal view, and is sized to anticipate several optical operating conditions. Overfill light illuminating the window aperture can create artifacts from the edge of the window aperture opening and other surface anomalies that may be visible on the screen. The illumination optical system should be designed to have zero light flux incident anywhere on the window aperture. Depending on the

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particular system's optical architecture, overfill light may have to be further reduced below the maximum 10% level in order to be acceptable.

6.6 DMD Temperature Calculation

Figure 6-1. DMD Thermal Test Points

Micromirror array temperature can be computed analytically from measurement points on the outside of the package, the package thermal resistance, the electrical power, and the illumination heat load. The relationship between micromirror array temperature and the reference ceramic temperature is provided by the following equations:

 T_{MAX} array = $T_{CERAMIC}$ + (Q_{ARRAY} × R_{MAX} array-to-ceramic)

 $T_{MIN \tART} = T_{CERAMIC} + (Q_{ARRAY} \times R_{MIN \tARTO-CERAMIC})$

 $T_{\text{DELTA-MIN}}$ = [minimum of TP2 or TP3] – T_{MAX} ARRAY

 T_{DELTA} MAX = [maximum of TP2 or TP3] – T_{MIN} ARRAY

 $Q_{ARRAY} = Q_{ELECTRICAL} + Q_{ILLUMINATION}$

where

- T_{ARRAY} = Computed array temperature (°C)
- $T_{CFRAMIC}$ = Measured ceramic temperature (°C) (TP1 location)
- RARRAY-TO-CERAMIC = Thermal resistance of package from array to ceramic TP1 (°C/Watt)
- Q_{ARRAY} = Total DMD power on the array (Watts) (electrical + absorbed)
- $Q_{\text{ELECTRICAL}}$ = Nominal electrical power
- Q_{INCIDENT} = Total incident optical power to DMD
- Q_{II} UMINATION = (DMD average thermal absorptivity \times Q_{INCIDENT})
- DMD average thermal absorptivity on-state $= 0.25$
- DMD average thermal absorptivity off-state $= 0.40$

The electrical power dissipation of the DMD ($Q_{ELECTRICAL}$) is variable and depends on the voltages, data rates and operating frequencies of each specific application system. Q_{ELECTRICAL} should be measured in each specific application to determine the proper value of $Q_{\text{EIECRICAL}}$ to use in the equations below. To calculate array temperature, the value for electrical power dissipation of the DMD (Q_{ELECTRICAL}) used in the example calculations below is 6.2 Watts (Typ). The absorbed power from the illumination source is variable and depends on the operating state of the micromirrors and the intensity of the light source. The equations shown above are valid for each DMD chip in a system. It assumes an illumination distribution of 91.0% on the active array, and 9.0% on the array border.

Sample calculations for off-state and on-state are shown below.

6.6.1 Off-State Thermal Differential (T_{DELTA_MIN})

TP1 (ceramic) = 25.0°C (measured) TP2 (window) = 50.0°C (measured) TP3 (window) = 47.0° C (measured) QINCIDENT = 150W (measured) $Q_{FI\text{ FCTRICAL}} = 6.2W$ R_{MAX} ARRAY-TO-CERAMIC = 0.55° C/W $Q_{ARRAY} = 6.2W + (150W \times 0.40) = 66.2W$ $T_{MAX \; ARRAY} = 25.0^{\circ}C + (66.2W \times 0.55^{\circ}C/W) = 61.4^{\circ}C$ T_{DELTA MIN = [minimum of TP2 or TP3] $-T_{MAX}$ ARRAY = 47.0°C – 61.4°C = –14.4°C

6.6.2 On-State Thermal Differential (TDELTA_MAX)

TP1 (ceramic) = 22.0°C (measured)

TP2 (window) = 38.0°C (measured)

TP3 (window) = 35.0°C (measured)

QINCIDENT = 150W (measured)

 $Q_{ELECTRICAL} = 6.2W$

RMIN_ARRAY-TO-CERAMIC = 0.30°C/W

 $Q_{ARRAY} = 6.2W + (150W \times 0.25) = 43.7W$

 $T_{MIN \ ARRAY}$ = 22.0°C + (43.7W × 0.30°C/W) =35.1°C

 $T_{\text{DELTA MAX}} =$ [maximum of TP2 or TP3] – $T_{\text{MIN ARRAY}} = 38.0^{\circ}\text{C} - 35.1^{\circ}\text{C} = 2.9^{\circ}\text{C}$

6.7 Micromirror Power Density Calculation

The calculation of the optical power density of the illumination on the DMD in the different wavelength bands uses the total measured optical power on the DMD, percent illumination overfill, area of the active array, and the ratio of the spectrum in the wavelength band of interest to the total spectral optical power.

- ILL_{UV} = [OP_{UV-RATIO} × Q_{INCIDENT}] × 1000 (mW/W) ÷ A_{ILL} (mW/cm²)
- $ILL_{VIS} = [OP_{VIS-RATIO} × Q_{INCIDENT}] ÷ A_{ILL} (W/cm²)$
- $ILL_{IR} = [OP_{IR-RATIO} \times Q_{INCIDENT}] \times 1000 \ (mW/W) \div A_{ILL} \ (mW/cm^2)$
- $ILL_{BLU} = [OP_{BLU-RATIO} \times Q_{INCIDENT}] \div A_{ILL}$ (W/cm²)
- ILL $_{\text{BLU1}}$ = [OP $_{\text{BLU1-RATIO}}$ × Q_{INCIDENT}] ÷ A_{ILL} (W/cm²)
- ILL $_{\text{BLU2}}$ = [OP $_{\text{BLU2-RATIO}}$ × Q_{INCIDENT}] ÷ A_{ILL} (W/cm²)
- $A_{ILL} = A_{ARRAY} \div (1 OV_{ILL}) (cm^2)$

where:

- ILL_{UV} = UV illumination power density on the DMD (mW/cm²)
- ILL_{VIS} = VIS illumination power density on the DMD (W/cm²)
- $\,$ ILL_{IR} = IR illumination power density on the DMD (mW/cm²)
- ILL $_{\sf BLU}$ = BLU illumination power density on the DMD (W/cm²)
- ILL $_{\sf BLU1}$ = BLU1 illumination power density on the DMD (W/cm²)
- ILL $_{\sf BLU2}$ = BLU2 illumination power density on the DMD (W/cm²)
- A_{ILL} = illumination area on the DMD (cm²)
- Q_{INCIDENT} = total incident optical power on DMD (W) (measured)
- $A_{\sf ARRAY}$ = area of the array (cm²) (data sheet)
- OV_{II} = percent of total illumination on the DMD outside the array (%) (optical model)
- OP_{UV-RATIO} = ratio of the optical power for wavelengths <410nm to the total optical power in the illumination spectrum (spectral measurement)
- $OP_{VIS-RATIO}$ = ratio of the optical power for wavelengths ≥410nm and ≤800nm to the total optical power in the illumination spectrum (spectral measurement)
- $OP_{IR-RATIO}$ = ratio of the optical power for wavelengths >800nm to the total optical power in the illumination spectrum (spectral measurement)
- OP_{BLU-RATIO} = ratio of the optical power for wavelengths ≥410nm and ≤475nm to the total optical power in the illumination spectrum (spectral measurement)
- $OP_{BIIII-RATIO}$ = ratio of the optical power for wavelengths ≥410nm and ≤440nm to the total optical power in the illumination spectrum (spectral measurement)
- $OP_{\text{BUL2-RATIO}}$ = ratio of the optical power for wavelengths ≥400nm and ≤420nm to the total optical power in the illumination spectrum (spectral measurement)

The illumination area varies and depends on the illumination overfill. The total illumination area on the DMD is the array area and overfill area around the array. The optical model is used to determine the percent of the total illumination on the DMD that is outside the array $(OV_{\vert L\vert})$ and the percent of the total illumination that is on the active array. From these values the illumination area (A_{ILL}) is calculated. The illumination is assumed to be uniform across the entire array.

From the measured illumination spectrum, the ratio of the optical power in the wavelength bands of interest to the total optical power is calculated.

Sample Calculation—Illumination 410nm – 800nm (Visible Wavelengths)

QINCIDENT = 150W (measured) A_{ARRAY} = (22.1184mm × 11.7504mm) ÷ 100 (mm/cm) = 2.599cm² (data sheet) $OV_{ILL} = 9\%$ (optical model) OPUV-RATIO = 0.00017 (spectral measurement) $OP_{VIS-RATIO} = 0.99977$ (spectral measurement) OPIR-RATIO = 0.00006 (spectral measurement) $OP_{BI U-RATIO} = 0.28100$ (spectral measurement) $OP_{BI U1-RATIO} = 0.03200$ (spectral measurement) $A_{ILL} = 2.599cm^2 \div (1 - 0.09) = 2.8560cm^2$ ILL_{UV} = [0.00017 × 150W] × 1000 (mW/W) ÷ 2.8560cm² = 8.928mW/cm² $ILL_{VIS} = [0.99977 \times 150W] \div 2.8560cm^2 = 52.51W/cm^2$ $ILL_{IR} = [0.00006 \times 150W] \times 1000 \text{ (mW/W)} \div 2.8560 \text{cm}^2 = 3.151 \text{mW/cm}^2$ $ILL_{BLU} = [0.28100 \times 150W] \div 2.8560cm^2 = 14.76W/cm^2$

 $ILL_{BLU1} = [0.03200 \times 150W] \div 2.8560 \text{cm}^2 = 1.68 W/\text{cm}^2$

Sample Calculation—Illumination 400nm – 420nm

- Q_{INCIDENT} = 33W (measured)
- A_{ARRAY} = (22.1184mm × 11.7504mm) ÷ 100 (mm/cm) = 2.599cm² (data sheet)
- OV_{III} = 9% (optical model)
- OPUV-RATIO = 0.00076 (spectral measurement)
- OPBLU2-RATIO = 0.99924 (spectral measurement)
- $A_{ILL} = 2.599cm^2 \div (1 0.09) = 2.8560cm^2$
- $ILL_{UV} = [0.00076 \times 33W] \times 1000 \text{ (mW/W)} \div 2.8560 \text{cm}^2 = 8.782 \text{mW/cm}^2$

 $ILL_{BLU2} = [0.99924 \times 33W] \div 2.8560 \text{cm}^2 = 11.546 \text{W/cm}^2$

6.8 Micromirror Landed-On/Landed-Off Duty Cycle

6.8.1 Definition of Micromirror Landed-On/Landed-Off Duty Cycle

The micromirror landed-on/landed-off duty cycle (landed duty cycle) denotes the amount of time (as a percentage) that an individual micromirror is landed in the On state versus the amount of time the same micromirror is landed in the Off state.

As an example, a landed duty cycle of 75/25 indicates that the referenced pixel is in the On state 75% of the time (and in the Off state 25% of the time); whereas 25/75 would indicate that the pixel is in the Off state 75% of the time. Likewise, 50/50 indicates that the pixel is On 50% of the time and Off 50% of the time.

Note that when assessing landed duty cycle, the time spent switching from one state (ON or OFF) to the other state (OFF or ON) is considered negligible and is thus ignored.

Since a micromirror can only be landed in one state or the other (On or Off), the two numbers (percentages) always add to 100.

6.8.2 Landed Duty Cycle and Useful Life of the DMD

Knowing the long-term average landed duty cycle (of the end product or application) is important because subjecting all (or a portion) of the DMD's micromirror array (also called the active array) to an asymmetric landed duty cycle for a prolonged period of time can reduce the DMD's usable life.

Note that it is the symmetry/asymmetry of the landed duty cycle that is of relevance. The symmetry of the landed duty cycle is determined by how close the two numbers (percentages) are to being equal. For example, a landed duty cycle of 50/50 is perfectly symmetrical whereas a landed duty cycle of 100/0 or 0/100 is perfectly asymmetrical.

6.8.3 Landed Duty Cycle and Operational DMD Temperature

Operational DMD Temperature and Landed Duty Cycle interact to affect the DMD's usable life, and this interaction can be exploited to reduce the impact that an asymmetrical Landed Duty Cycle has on the DMD's usable life. This is quantified in the de-rating curve shown in [Figure 5-1.](#page-11-0) The importance of this curve is that:

- All points along this curve represent the same usable life.
- All points above this curve represent lower usable life (and the further away from the curve, the lower the usable life).
- All points below this curve represent higher usable life (and the further away from the curve, the higher the usable life).

In practice, this curve specifies the Maximum Operating DMD Temperature that the DMD should be operated at for a given long-term average Landed Duty Cycle.

6.8.4 Estimating the Long-Term Average Landed Duty Cycle of a Product or Application

During a given period of time, the Landed Duty Cycle of a given pixel follows from the image content being displayed by that pixel.

For example, in the simplest case, when displaying pure-white on a given pixel for a given time period, that pixel will experience a 100/0 Landed Duty Cycle during that time period. Likewise, when displaying pure-black, the pixel will experience a 0/100 Landed Duty Cycle.

Between the two extremes (ignoring for the moment color and any image processing that may be applied to an incoming image), the Landed Duty Cycle tracks one-to-one with the gray scale value, as shown in Table 6-1.

Table 6-1. Grayscale Value and Landed Duty Cycle

Table 6-1. Grayscale Value and Landed Duty Cycle (continued)

7 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

7.1 Application Information

Texas Instruments DLP technology is a micro-electro-mechanical systems (MEMS) technology that modulates light using a digital micromirror device (DMD). DMDs vary in resolution and size and can contain over 8.9 million micromirrors. Each micromirror of a DMD is independently controlled and can be synchronized with illuminators and cameras to enable a wide range of applications. DLP technology enables a wide variety of Industrial products worldwide, from digital imaging engines embedded in large lithography machines to high-resolution 3D Printing machines.

The most recent class of chipsets from Texas Instruments is based on a breakthrough micromirror technology, called SST. With a smaller pixel pitch of 5.4μm and a tilt angle of 12 degrees, SST chipsets enable higher resolution in a smaller form factor and enhanced image processing features while maintaining high optical efficiency. DLP chipsets are a great fit for any system that values high-resolution projection at high-modulation speeds.

7.2 Typical Application

The DLP991U DMD is a 4096 × 2176 resolution DLP digital micromirror device. When combined with the TI DLPC964 industrial controller and other electrical, optical and mechanical components the DLP991U DMD provides a superior solution for industrial direct imaging and 3D printer applications. Figure 7-1 shows a typical single-chip system application using the DLP991U DMD.

Table 7-1. DMD Overview

7.2.1 Design Requirements

At a high level, DLP991U DMD systems include an illumination source, a light engine, electronic components, and software. The designer must first choose an illumination source and design the optical engine taking into consideration the relationship between the optics and the illumination source. The designer must then understand the electronic components of a DMD system. The application PCB board supports all of the required electronic components to power and control the DLP991U DMD, which can include the DLPC964 industrial controller, power supplies, and the DMD device.

7.2.2 Detailed Design Procedure

For customer assistance in designing the electrical connections between the DLPC964 Industrial Controller and the DLP991U DMD, TI provides a reference design schematic and layout guidelines which are recommended to be followed to achieve a reliable projection subsystem. To complete the DLP system an optical module or light engine is required that contains the DMD, associated illumination sources, optical elements, necessary mechanical components, and recommended thermal design concepts and guidelines.

7.3 DMD Die Temperature Sensing

The DMD features a built-in thermal diode that measures the temperature at one corner of the die outside the micromirror array. The thermal diode can be interfaced with the TMP461 temperature sensor, as shown in Figure 7-2. The serial bus from the TMP461 can be connected to the DLPC964 industrial controller to enable its temperature sensing features. See the *[DLPC964 Digital Micromirror Device Controller Data Sheet](https://www.ti.com/lit/pdf/dlps167)* for more information about how to query the temperature readings.

The DLPC964 industrial controller can configure the TMP461 to read the DMD temperature sensor diode. This data can be leveraged to incorporate additional functionality in the overall system design such as adjusting illumination power, fan speeds, active cooling temperatures, or flow rates, and so on. All communication between the TMP461 and the DLPC964 industrial controller are completed using the I²C interface. The TMP461 connects to the DMD via pins E23 and F22, as outlined in [Pin Configuration and Functions.](#page-2-0)

Figure 7-2. System Board Routing Example for Temperature Sensor

- 1. Details are omitted for clarity. See the TI reference design for connections to the DLPC964 industrial controller.
- 2. See the [TMP461 Data Sheet](https://www.ti.com/lit/pdf/SBOS722) for system board layout recommendations.

- 3. See the [TMP461 Data Sheet](https://www.ti.com/lit/pdf/SBOS722) and the TI Reference Design for suggested component values for R1, R2, R3, R4, and C1.
- 4. R5 = 0Ω. R6 = 0Ω. Zero ohm resistors should be located close to the DMD package pins.

7.4 Power Supply Recommendations

The following power supplies are all required to operate the DMD: V_{DD} , V_{DDA} , V_{BIAS} , V_{OFFSET} , and V_{REF} . DMD power-up and power-down sequencing is strictly controlled by the DLP display controller.

Note

For reliable operation of the DMD, the following power supply sequencing requirements must be followed. Failure to adhere to any of the prescribed power-up and power-down requirements may affect device reliability. See [Figure 7-3](#page-34-0) DMD Power Supply Sequencing Requirements.

V_{DD,} V_{DDA}, V_{BIAS}, V_{OFFSET}, and V_{RESET} power supplies must be coordinated during power-up and power-down operations. Failure to meet any of the below requirements results in a significant reduction in the DMD's reliability and lifetime. Common ground VSS must also be connected.

Table 7-2. Power Supply Sequence Requirements

(1) See Sequence Delay Requirement.

7.4.1 DMD Power Supply Power-Up Procedure

- During power-up, V_{DD} and V_{DDA} must always start and settle before V_{OFFSET} plus Delay1 specified in [Table](#page-34-0) [7-3](#page-34-0), V_{BIAS} , and V_{RESET} voltages are applied to the DMD.
- During power-up, it is a strict requirement that the voltage delta between V_{BIAS} and V_{OFFSET} must be within the specified limit shown in [Section 5.4.](#page-9-0)
- During power-up, there is no requirement for the relative timing of V_{RESET} with respect to V_{BIAS} .
- Power supply slew rates during power-up are flexible, provided that the transient voltage levels follow the requirements specified in [Section 5.1,](#page-8-0) in [Section 5.4](#page-9-0), and in [Figure 7-3](#page-34-0).
- During power-up, LVCMOS input pins must not be driven high until after V_{DD} and V_{DDA} have settled at operating voltages listed in [Section 5.4](#page-9-0).

7.4.2 DMD Power Supply Power-Down Procedure

- During power-down, V_{DD} and V_{DDA} must be supplied until after V_{BIAS} , V_{RESET} , and V_{OFFSET} are discharged to within the specified limit of ground. See [Table 7-3](#page-34-0).
- During power-down, it is a strict requirement that the voltage delta between V_{BIAS} and V_{OFFSET} must be within the specified limit shown in [Section 5.4.](#page-9-0)
- During power-down, there is no requirement for the relative timing of V_{RESET} with respect to V_{BIAS} .
- Power supply slew rates during power-down are flexible, provided that the transient voltage levels follow the requirements specified in [Section 5.1,](#page-8-0) in [Section 5.4](#page-9-0), and in [Figure 7-3](#page-34-0).
- During power-down, LVCMOS input pins must be less than specified in [Section 5.4.](#page-9-0)

Figure 7-3. DMD Power Supply Requirements

- 1. See [Section 4.](#page-2-0)
- 2. To prevent excess current, the supply voltage delta $|V_{BIAS} V_{OFFSET}|$ must be less than specified in Section [5.4](#page-9-0).
- 3. To prevent excess current, the supply voltage delta $|V_{BIAS} V_{RESET}|$ must be less than specified limit in [Section 5.4](#page-9-0).
- 4. V_{BIAS} should power up after V_{OFFSET} has powered up, per the Delay1 specification in Table 7-3.
- 5. DLP controller software initiates the global V_{BIAS} command.
- 6. After the DMD micromirror park sequence is complete, the DLP controller software initiates a hardware power-down that activates DMD_EN_ARSTZ and disables V_{BIAS} , V_{RESET} , and V_{OFFSET} .
- 7. Under power-loss conditions where emergency DMD micromirror park procedures are being enacted by the DLP controller hardware DMD_EN_ARSTZ will go low.
- 8. V_{DD} / V_{DDA} must remain above the minimum values specified in [Section 6.4](#page-9-0) until after V_{OFFSET} , V_{BIAS} , VRESET go low, per Delay2 specification in Table 7-3.
- 9. To prevent excess current, the supply voltage delta $|V_{DDA} V_{DD}|$ must be less than specified limit in [Section](#page-9-0) [5.4](#page-9-0).

Table 7-3. DMD Power-Supply Requirements

7.5 Layout

7.5.1 Layout Guidelines

These guidelines are targeted at designing a PCB board with the DLP991U DMD. The DMD board is a highspeed multi-layer PCB, with primarily high-speed digital logic including 3.6Gbps differential data buses run to the DMD. Use full or mini power planes for V_{OFFSFT} , V_{RFSFT} , and V_{BIAS} . Solid planes are required for ground. The target impedance for single-ended traces on the PCB is 50Ω ±10% and 100Ω ±10% for differential traces, as outlined in Table 7-5. Manufacture the PCB with a high-quality FR-4 material.

7.5.1.1 PCB Design Standards

PCBs must be designed and built in accordance with the industry specifications shown in Industry Design Specifications.

Table 7-4. Industry Design Specifications

7.5.1.2 General PCB Routing

7.5.1.2.1 Trace Impedance and Routing Priority

For best performance, TI recommends a target impedance for the PCB of $50\Omega \pm 10\%$ for single-ended signals. The differential signals that are 100Ω ±10% are described in Trace Impedance.

Table 7-5. Trace Impedance

Table 7-6 lists the routing priority of the signals.

Table 7-6. Routing Priority

7.5.1.2.2 Example PCB Layer Stack-Up

Careful attention to the PCB layer design is required to meet system design requirements. [Table 7-7](#page-36-0) shows an example PCB stack-up. To maximize signal integrity of the high-speed differential signals that make up the HSSI DMD input interface, the differential signals are routed on the internal layers and referenced to solid ground planes. To further improve the signal integrity of the DMD board, Nelco N4000-13 SI is used as the dielectric material to improve the signal slew rate for better performance of the HSSI DMD Input Interface.

1. As noted in the DLP991U DMD mechanical ICD drawing, the DMD device pads are plated with 50–100 micro-inches electrolytic nickel under 30 micro-inches minimum electrolytic gold.

7.5.1.2.3 Trace Width, Spacing

Unless otherwise specified, TI recommends that all signals follow the 0.005"/0.0015" (Trace-Width/Spacing) design rule. Use an analysis of impedance and stack-up requirements to determine and calculate actual trace widths.

Maximize the width of all voltage signals as space permits.

Follow the width and spacing requirements listed in Table 7-8 and [Table 7-9](#page-37-0).

Table 7-8. Trace Minimum Spacing

SIGNAL	PWR	GND	- SINGLE-ENDED	DIFFERENTIAL PAIRS	UNIT
				PAIR-TO-PAIR	
PWR	15	5	15	15	mils
GND	5		5	5	mils
HSSI DMD Interface —DMD D $(A,B,C,D)[7:0],$ DMD DCLK (A,B,C,D),	15	5	3x intra-pair (P-to-N) spacing	3x intra-pair (P-to-N) spacing	mils
DMD LS Interface- DMD LS CLK, DMD LS WDATA, DMD_LS_RDATA_(A,B,C,D)	15	5	3x trace width spacing	3x intra-pair (P-to-N) spacing	mils
All other signals	15	5	3x trace width spacing	3x intra-pair (P-to-N) spacing	mils

[DLP991U](https://www.ti.com/product/DLP991U)

Table 7-9. Voltage Trace Widths and Spacing Recommendations

7.5.1.2.4 Power and Ground Planes

TI strongly discourages signal routing on power planes or on planes adjacent to power planes. If signals must be routed on layers adjacent to power planes, they must not cross splits in power planes to prevent EMI and preserve signal integrity.

Connect all internal digital ground (GND) planes in as many places as possible. Connect all internal ground planes with a minimum distance between connections of 0.5". Extra vias may not be required if there are sufficient ground vias due to normal ground connections of devices.

Connect power and ground pins of each component to the power and ground planes with at least one via for each pin. Minimize trace lengths for component power and ground pins. (ideally, less than 0.100").

Ground plane slots are strongly discouraged.

7.5.1.2.5 Trace Length Matching

7.5.1.2.5.1 HSSI Input Bus Skew

High-Speed Serial DMD Interface Routing Constraints lists the high-speed serial DMD interface routing constraints.

Table 7-10. High-Speed Serial DMD Interface Routing Constraints

Table 7-10. High-Speed Serial DMD Interface Routing Constraints (continued)

7.5.1.2.5.2 Other Timing Critical Signals

Other Timing Critical Signals lists the routing constraints for other timing critical signals.

Table 7-11. Other Timing Critical Signals

8 Device and Documentation Support

8.1 Device Support

8.1.1 Device Nomenclature

Figure 8-1. Part Number Description

8.1.2 Device Markings

The device marking includes both human-readable information and a 2-dimensional matrix code. The humanreadable information is described in Figure 8-2. The 2-dimensional matrix code is an alpha-numeric character string that contains the DMD part number, part 1 of the serial number, and part 2 of the serial number. The first character of the DMD serial number (part 1) is the manufacturing year. The second character of the DMD serial number (part 1) is the manufacturing month.

Example: DLP991UFLV GHXXXXX LLLLLLM

Figure 8-2. DMD Marking Locations

8.2 Documentation Support

8.2.1 Related Documentation

The following documents contain additional information related to the chipset components used with the DLP991UFLV DMD.

- *[DLPC964 Digital Micromirror Device Controller Data Sheet](https://www.ti.com/lit/pdf/DLPS167)*
- *[DLPLCRC964 Evaluation Module Quick Start Guide](https://www.ti.com/lit/pdf/dlpu132)*
- *DLP DLPC964 Apps FPGA User's Guide*

8.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com.](https://www.ti.com) Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

8.4 Support Resources

TI E2E™ [support forums](https://e2e.ti.com) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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8.5 Trademarks

TI E2E™ is a trademark of Texas Instruments.

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8.6 Electrostatic Discharge Caution

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

8.7 Glossary

[TI Glossary](https://www.ti.com/lit/pdf/SLYZ022) This glossary lists and explains terms, acronyms, and definitions.

9 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

10 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

10.1 Package Option Addendum

10.1.1 Packaging Information

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PRE_PROD Unannounced device, not in production, not available for mass market, nor on the web, samples not available.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check<http://www.ti.com/productcontent>for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

- (3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
- (4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device
- (5) Multiple Device markings will be inside parentheses. Only on Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

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NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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