

# TLV936x 10-MHz, 40-V, RRO, Operational Amplifier for Cost-Sensitive Systems

## 1 Features

- Low offset voltage:  $\pm 400 \mu\text{V}$
- Low offset voltage drift:  $\pm 1.25 \mu\text{V}/^\circ\text{C}$
- Low noise:  $8.5 \text{ nV}/\sqrt{\text{Hz}}$  at 1 kHz,  $6 \text{ nV}/\sqrt{\text{Hz}}$  broadband
- High common-mode rejection: 110 dB
- Low bias current:  $\pm 10 \text{ pA}$
- Rail-to-rail output
- Wide bandwidth: 10.6-MHz GBW, unity-gain stable
- High slew rate:  $25 \text{ V}/\mu\text{s}$
- Low quiescent current: 2.6 mA per amplifier
- Wide supply:  $\pm 2.25 \text{ V}$  to  $\pm 20 \text{ V}$ , 4.5 V to 40 V
- Robust EMIRR performance

## 2 Applications

- [AC and motor drive servo control module](#)
- [AC and motor drive power stage module](#)
- [Test and measurement equipment](#)
- [Programmable logic controllers](#)

## 3 Description

The TLV936x family (TLV9361, TLV9362, and TLV9364) is a family of 40-V cost-optimized operational amplifiers.

These devices offer strong DC and AC specifications, including rail-to-rail output, low offset ( $\pm 400 \mu\text{V}$ , typ), low offset drift ( $\pm 1.25 \mu\text{V}/^\circ\text{C}$ , typ), and 10.6-MHz bandwidth.

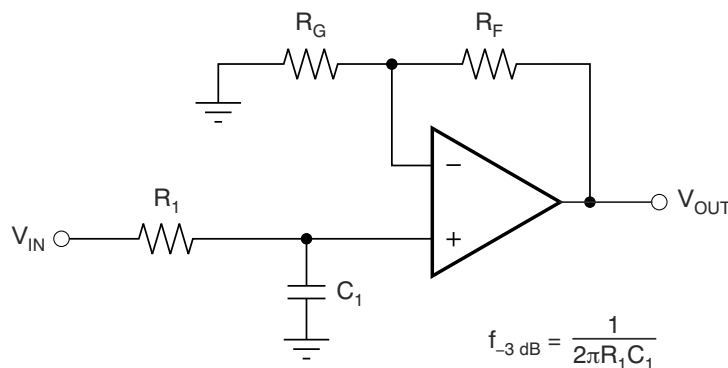
Features such as EMIRR filtering, high output current ( $\pm 60 \text{ mA}$ ), and high slew rate ( $25 \text{ V}/\mu\text{s}$ ) make the TLV936x a robust operational amplifier for high-voltage, cost-sensitive applications.

The TLV936x family of op amps is available in standard packages and is specified from  $-40^\circ\text{C}$  to  $125^\circ\text{C}$ .

### Device Information

PART NUMBER <sup>(1)</sup>	PACKAGE	BODY SIZE (NOM)
TLV9361	SOT-23 (5)	2.90 mm × 1.60 mm
	SC70 (5)	2.00 mm × 1.25 mm
TLV9362	SOIC (8)	4.90 mm × 3.90 mm
	SOT-23 (8)	2.90 mm × 1.60 mm
	TSSOP (8)	3.00 mm × 4.40 mm
TLV9364	VSSOP (8)	3.00 mm × 3.00 mm
	SOIC (14)	8.65 mm × 3.90 mm
	TSSOP (14)	5.00 mm × 4.40 mm

(1) For all available packages, see the orderable addendum at the end of the data sheet.



$$\frac{V_{\text{OUT}}}{V_{\text{IN}}} = \left(1 + \frac{R_F}{R_G}\right) \left(\frac{1}{1 + sR_1 C_1}\right)$$

TLV936x in a Single-Pole, Low-Pass Filter



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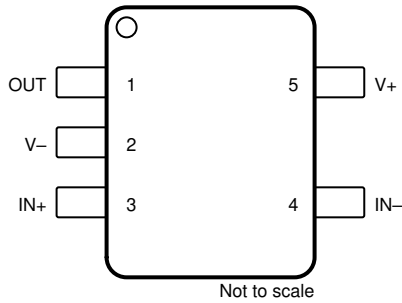
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## 4 Revision History

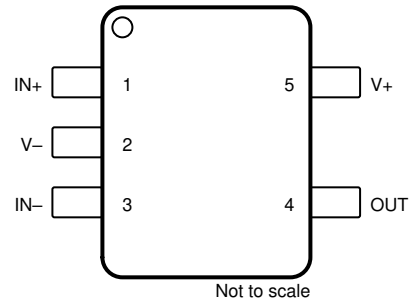
NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

<b>Changes from Revision A (December 2021) to Revision B (March 2022)</b>	<b>Page</b>
• Adjusted $A_{OL}$ test condition at $V_S = 40\text{ V}$ across temperature from " $V_S = 40\text{ V}$ , $V_{CM} = V_S / 2$ , $(V-) + 0.1\text{ V} < V_O < (V+) - 0.1\text{ V}$ " to " $V_S = 40\text{ V}$ , $V_{CM} = V_S / 2$ , $(V-) + 0.12\text{ V} < V_O < (V+) - 0.12\text{ V}$ ".....	8
<b>Changes from Revision * (November 2021) to Revision A (December 2021)</b>	<b>Page</b>
• Removed preview notation from TLV9364 SOIC (14) package from <i>Device Information</i> table.....	1
• Removed preview notation from TLV9364 TSSOP (14) package from <i>Device Information</i> table.....	1
• Removed preview notation from TLV9364 D package (SOIC) in the <i>Pin Configuration and Functions</i> section... 3	
• Removed preview notation from TLV9364 PW package (TSSOP) in the <i>Pin Configuration and Functions</i> section.....	3
• Removed preview notation from TLV9164 D package (SOIC) in the <i>Thermal Information for Quad Channel</i> section.....	7
• Removed preview notation from TLV9164 PW package (TSSOP) in the <i>Thermal Information for Quad Channel</i> section.....	7

## 5 Pin Configuration and Functions



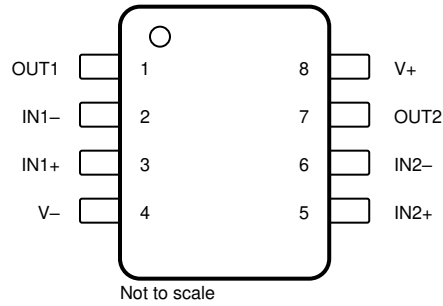
**Figure 5-1. TLV9361 DBV Package  
5-Pin SOT-23  
(Top View)**



**Figure 5-2. TLV9361 DCK Package  
5-Pin SC70  
(Top View)**

**Table 5-1. Pin Functions: TLV9361**

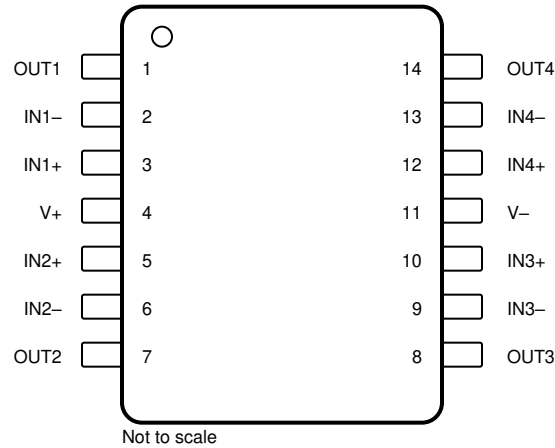
NAME	PIN		I/O	DESCRIPTION
	SOT-23	SC70		
IN+	3	1	I	Noninverting input
IN-	4	3	I	Inverting input
OUT	1	4	O	Output
V+	5	5	—	Positive (highest) power supply
V-	2	2	—	Negative (lowest) power supply



**Figure 5-3. TLV9362 D, DDF, DGK, and PW Package  
8-Pin SOIC, SOT-23, VSSOP, and TSSOP  
(Top View)**

**Table 5-2. Pin Functions: TLV9362**

PIN		I/O	DESCRIPTION
NAME	NO.		
IN1+	3	I	Noninverting input, channel 1
IN1-	2	I	Inverting input, channel 1
IN2+	5	I	Noninverting input, channel 2
IN2-	6	I	Inverting input, channel 2
OUT1	1	O	Output, channel 1
OUT2	7	O	Output, channel 2
V+	8	—	Positive (highest) power supply
V-	4	—	Negative (lowest) power supply



**Figure 5-4. TLV9364 D and PW Package  
SOIC and TSSOP  
(Top View)**

**Table 5-3. Pin Functions: TLV9364**

PIN		I/O	DESCRIPTION
NAME	NO.		
IN1+	3	I	Noninverting input, channel 1
IN1-	2	I	Inverting input, channel 1
IN2+	5	I	Noninverting input, channel 2
IN2-	6	I	Inverting input, channel 2
IN3+	10	I	Noninverting input, channel 3
IN3-	9	I	Inverting input, channel 3
IN4+	12	I	Noninverting input, channel 4
IN4-	13	I	Inverting input, channel 4
OUT1	1	O	Output, channel 1
OUT2	7	O	Output, channel 2
OUT3	8	O	Output, channel 3
OUT4	14	O	Output, channel 4
V+	4	—	Positive (highest) power supply
V-	11	—	Negative (lowest) power supply

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating ambient temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
Supply voltage, $V_S = (V+) - (V-)$		0	42	V
Signal input pins	Common-mode voltage <sup>(3)</sup>	$(V-) - 0.5$	$(V+) + 0.5$	V
	Differential voltage <sup>(3)</sup>		$V_S + 0.2$	V
	Current <sup>(3)</sup>	-10	10	mA
Output short-circuit <sup>(2)</sup>		Continuous		
Operating ambient temperature, $T_A$		-55	150	°C
Junction temperature, $T_J$			150	°C
Storage temperature, $T_{stg}$		-65	150	°C

- Operating the device beyond the ratings listed under *Absolute Maximum Ratings* will cause permanent damage to the device. These are stress ratings only, based on process and design limitations, and this device has not been designed to function outside the conditions indicated under *Recommended Operating Conditions*. Exposure to any condition outside *Recommended Operating Conditions* for extended periods, including absolute-maximum-rated conditions, may affect device reliability and performance.
- Short-circuit to ground, one amplifier per package. Extended short-circuit current, especially with higher supply voltage, can cause excessive heating and eventual destruction.
- Input pins are diode-clamped to the power-supply rails. Input signals that may swing more than 0.5 V beyond the supply rails must be current limited to 10 mA or less.

### 6.2 ESD Ratings

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2500	V
		Charged-device model (CDM), per ANSI/ESDA/JEDEC JS-002 <sup>(2)</sup>	±1500	

- JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

over operating ambient temperature range (unless otherwise noted)

		MIN	MAX	UNIT
$V_S$	Supply voltage, $(V+) - (V-)$	4.5	40	V
$V_I$	Common mode voltage range	$(V-)$	$(V+) - 2$	V
$T_A$	Specified temperature	-40	125	°C

### 6.4 Thermal Information for Single Channel

THERMAL METRIC <sup>(1)</sup>		TLV9361, TLV9361S		UNIT
		DBV (SOT-23)	DCK (SC70)	
		5 PINS	5 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	185.4	198.1	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	83.9	94.1	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	52.5	45.3	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	25.4	16.9	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	52.1	45.0	°C/W
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	N/A	N/A	°C/W

- For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, [SPRA953](#).

## 6.5 Thermal Information for Dual Channel

THERMAL METRIC <sup>(1)</sup>		TLV9362				Unit
		D (SOIC)	DDF (SOT-23)	DGK (VSSOP)	PW (TSSOP)	
		8 PINS	8 PINS	8 PINS	8 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	131.0	149.6	174.2	183.4	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	73.0	85.3	65.9	72.4	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	74.5	68.6	95.9	114.0	°C/W
ψ <sub>JT</sub>	Junction-to-top characterization parameter	25.0	7.9	11.0	12.1	°C/W
ψ <sub>JB</sub>	Junction-to-board characterization parameter	73.8	68.4	94.4	112.3	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	N/A	N/A	N/A	N/A	°C/W

- (1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, [SPRA953](#).

## 6.6 Thermal Information for Quad Channel

THERMAL METRIC <sup>(1)</sup>		TLV9364		UNIT
		D (SOIC)	PW (TSSOP)	
		14 PINS	14 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	99.0	118.8	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	55.1	47.0	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	54.8	61.9	°C/W
ψ <sub>JT</sub>	Junction-to-top characterization parameter	16.7	5.5	°C/W
ψ <sub>JB</sub>	Junction-to-board characterization parameter	54.4	61.3	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	N/A	N/A	°C/W

- (1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, [SPRA953](#).

## 6.7 Electrical Characteristics

For  $V_S = (V+) - (V-) = 4.5\text{ V to }40\text{ V}$  ( $\pm 2.25\text{ V to } \pm 20\text{ V}$ ) at  $T_A = 25^\circ\text{C}$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = V_S / 2$ , and  $V_{OUT} = V_S / 2$ , unless otherwise noted.

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
<b>OFFSET VOLTAGE</b>							
$V_{OS}$	Input offset voltage	$V_{CM} = V_-$	$T_A = -40^\circ\text{C to }125^\circ\text{C}$		$\pm 0.4$	$\pm 1.7$	mV
						$\pm 2$	
$dV_{OS}/dT$	Input offset voltage drift	$V_{CM} = V_-$	$T_A = -40^\circ\text{C to }125^\circ\text{C}$		$\pm 1.25$		$\mu\text{V}/^\circ\text{C}$
PSRR	Input offset voltage versus power supply	$V_{CM} = V_-$ , $V_S = 5\text{ V to }40\text{ V}^{(1)}$	$T_A = -40^\circ\text{C to }125^\circ\text{C}$		$\pm 1.5$	$\pm 7.5$	$\mu\text{V}/\text{V}$
	DC channel separation				1		$\mu\text{V}/\text{V}$
<b>INPUT BIAS CURRENT</b>							
$I_B$	Input bias current				$\pm 10$		pA
$I_{OS}$	Input offset current				$\pm 10$		pA
<b>NOISE</b>							
$E_N$	Input voltage noise	$f = 0.1\text{ Hz to }10\text{ Hz}$			6		$\mu\text{V}_{PP}$
					1		$\mu\text{V}_{RMS}$
$e_N$	Input voltage noise density	$f = 1\text{ kHz}$			8.5		$\text{nV}/\sqrt{\text{Hz}}$
		$f = 10\text{ kHz}$			6		
$i_N$	Input current noise density	$f = 1\text{ kHz}$			100		$\text{fA}/\sqrt{\text{Hz}}$
<b>INPUT VOLTAGE RANGE</b>							
$V_{CM}$	Common-mode voltage range			$(V_-)$		$(V+) - 2$	V
CMRR	Common-mode rejection ratio	$V_S = 40\text{ V}$ , $V_- < V_{CM} < (V+) - 2\text{ V}$	$T_A = -40^\circ\text{C to }125^\circ\text{C}$	95	110		dB
		$V_S = 5\text{ V}$ , $V_- < V_{CM} < (V+) - 2\text{ V}^{(1)}$		75	85		
<b>INPUT IMPEDANCE</b>							
$Z_{ID}$	Differential				$100 \parallel 9$		$\text{M}\Omega \parallel \text{pF}$
$Z_{ICM}$	Common-mode				$6 \parallel 1$		$\text{T}\Omega \parallel \text{pF}$
<b>OPEN-LOOP GAIN</b>							
$A_{OL}$	Open-loop voltage gain	$V_S = 40\text{ V}$ , $V_{CM} = V_S / 2$ , $(V_-) + 0.1\text{ V} < V_O < (V+) - 0.1\text{ V}$	$T_A = -40^\circ\text{C to }125^\circ\text{C}$	115	130		dB
		$V_S = 40\text{ V}$ , $V_{CM} = V_S / 2$ , $(V_-) + 0.12\text{ V} < V_O < (V+) - 0.12\text{ V}$			130		
		$V_S = 5\text{ V}$ , $V_{CM} = V_S / 2$ , $(V_-) + 0.1\text{ V} < V_O < (V+) - 0.1\text{ V}^{(1)}$	$T_A = -40^\circ\text{C to }125^\circ\text{C}$	100	120		
					120		
<b>FREQUENCY RESPONSE</b>							
GBW	Gain-bandwidth product				10.6		MHz
SR	Slew rate	$V_S = 40\text{ V}$ , $G = +1$ , $V_{STEP} = 10\text{ V}$ , $C_L = 20\text{ pF}^{(3)}$			25		$\text{V}/\mu\text{s}$
$t_s$	Settling time	To 0.1%, $V_S = 40\text{ V}$ , $V_{STEP} = 10\text{ V}$ , $G = +1$ , $C_L = 20\text{ pF}$			0.65		$\mu\text{s}$
		To 0.1%, $V_S = 40\text{ V}$ , $V_{STEP} = 2\text{ V}$ , $G = +1$ , $C_L = 20\text{ pF}$			0.3		
		To 0.01%, $V_S = 40\text{ V}$ , $V_{STEP} = 10\text{ V}$ , $G = +1$ , $C_L = 20\text{ pF}$			0.86		
		To 0.01%, $V_S = 40\text{ V}$ , $V_{STEP} = 2\text{ V}$ , $G = +1$ , $C_L = 20\text{ pF}$			0.44		
	Phase margin	$G = +1$ , $R_L = 10\text{ k}\Omega$ , $C_L = 20\text{ pF}$			64		$^\circ$
	Overload recovery time	$V_{IN} \times \text{gain} > V_S$			170		ns
THD+N	Total harmonic distortion + noise	$V_S = 40\text{ V}$ , $V_O = 3\text{ V}_{RMS}$ , $G = 1$ , $f = 1\text{ kHz}$ , $R_L = 10\text{ k}\Omega$			0.0001%		
					120		dB
		$V_S = 10\text{ V}$ , $V_O = 3\text{ V}_{RMS}$ , $G = 1$ , $f = 1\text{ kHz}$ , $R_L = 128\ \Omega$			0.0056%		
					85		dB
		$V_S = 10\text{ V}$ , $V_O = 0.4\text{ V}_{RMS}$ , $G = 1$ , $f = 1\text{ kHz}$ , $R_L = 32\ \Omega$			0.00056%		
					105		dB



## 6.7 Electrical Characteristics (continued)

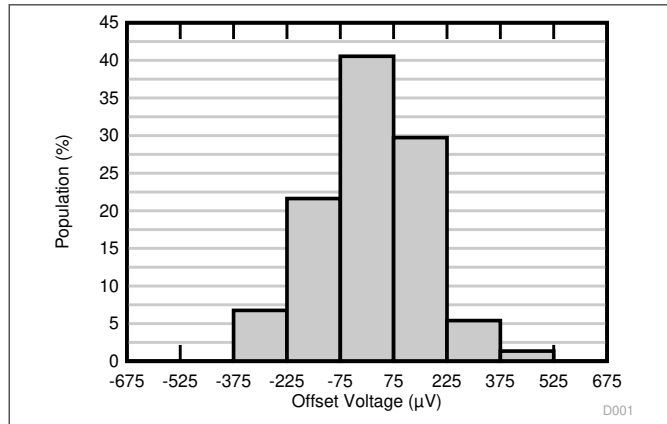
For  $V_S = (V+) - (V-) = 4.5\text{ V to }40\text{ V}$  ( $\pm 2.25\text{ V to } \pm 20\text{ V}$ ) at  $T_A = 25^\circ\text{C}$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = V_S / 2$ , and  $V_{OUT} = V_S / 2$ , unless otherwise noted.

PARAMETER	TEST CONDITIONS		MIN	TYP	MAX	UNIT
<b>OUTPUT</b>						
Voltage output swing from rail	Positive and negative rail headroom	$V_S = 40\text{ V}$ , $R_L = \text{no load}$		10		mV
		$V_S = 40\text{ V}$ , $R_L = 10\text{ k}\Omega$		60	100	
		$V_S = 40\text{ V}$ , $R_L = 2\text{ k}\Omega$		250	400	
$I_{SC}$	Short-circuit current			$\pm 60^{(2)}$		mA
$C_{LOAD}$	Capacitive Load Drive			See <a href="#">Figure 6-28</a>		pF
$Z_O$	Open-loop output impedance	$I_O = 0\text{ A}$		See <a href="#">Figure 6-25</a>		$\Omega$
<b>POWER SUPPLY</b>						
$I_Q$	Quiescent current per amplifier	$I_O = 0\text{ A}$		2.6	3	mA
			$T_A = -40^\circ\text{C to }125^\circ\text{C}$			

- (1) Specified by characterization only.
- (2) At high supply voltage, placing the TLV936x in a sudden short to mid-supply or ground will lead to rapid thermal shutdown. Output current greater than  $I_{SC}$  can be achieved if rapid thermal shutdown is avoided as per [Figure 6-12](#).
- (3) See [Figure 6-11](#) for more information.

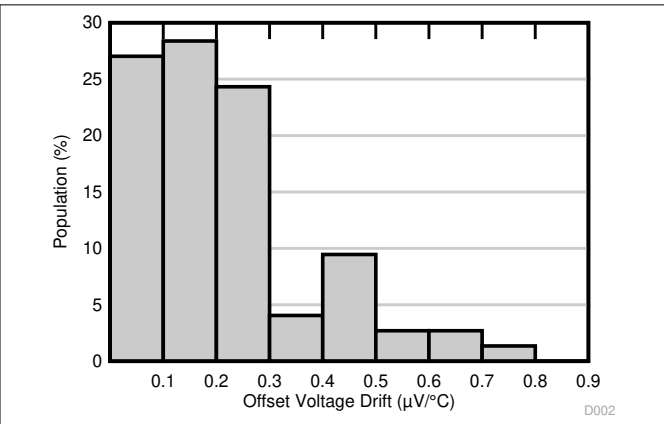
## 6.8 Typical Characteristics

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 20\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  (unless otherwise noted)



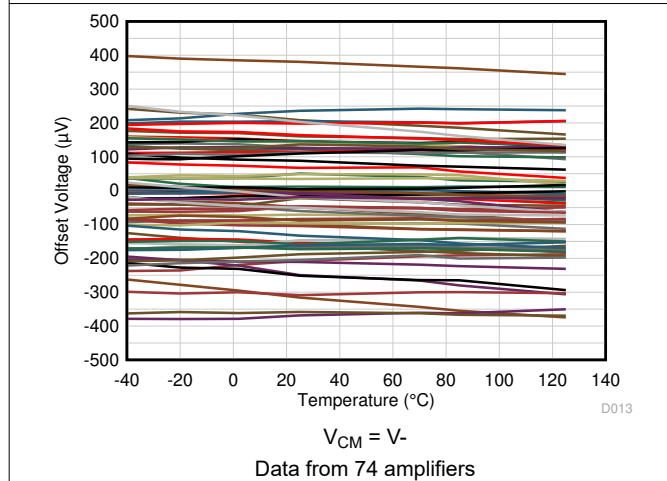
Distribution from 74 amplifiers,  $T_A = 25^\circ\text{C}$

**Figure 6-1. Offset Voltage Production Distribution**



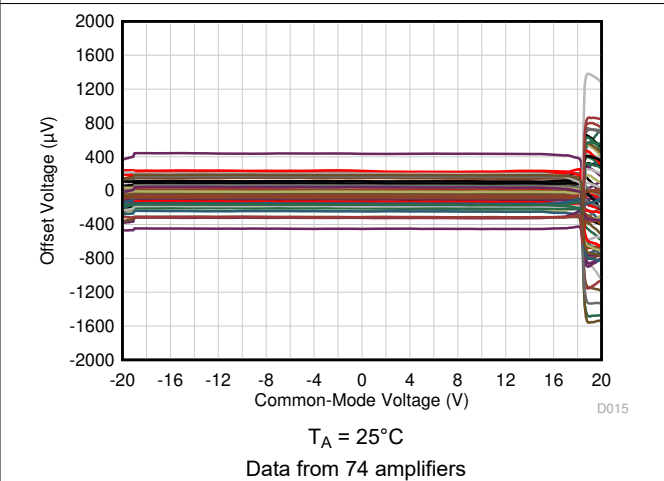
Distribution from 74 amplifiers

**Figure 6-2. Offset Voltage Drift Distribution**



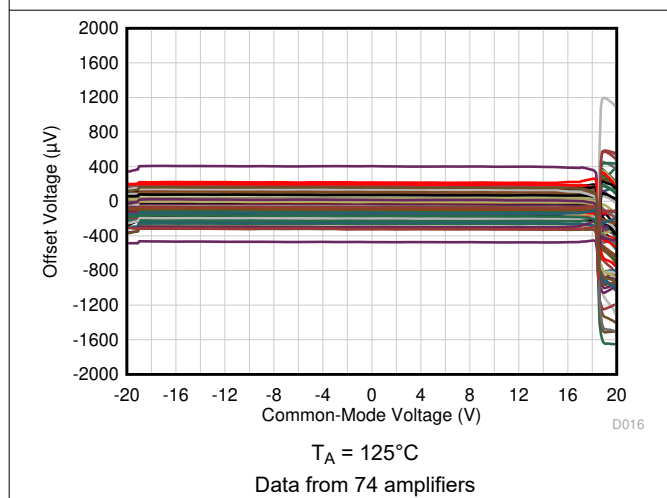
$V_{CM} = V_-$   
Data from 74 amplifiers

**Figure 6-3. Offset Voltage vs Temperature**



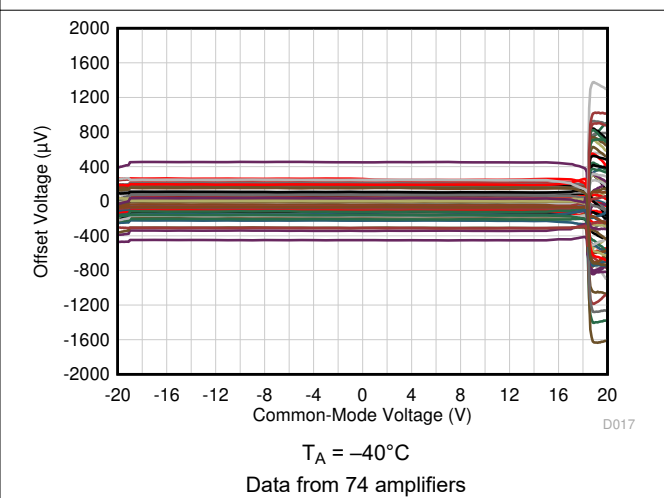
$T_A = 25^\circ\text{C}$   
Data from 74 amplifiers

**Figure 6-4. Offset Voltage vs Common-Mode Voltage**



$T_A = 125^\circ\text{C}$   
Data from 74 amplifiers

**Figure 6-5. Offset Voltage vs Common-Mode Voltage**



$T_A = -40^\circ\text{C}$   
Data from 74 amplifiers

**Figure 6-6. Offset Voltage vs Common-Mode Voltage**

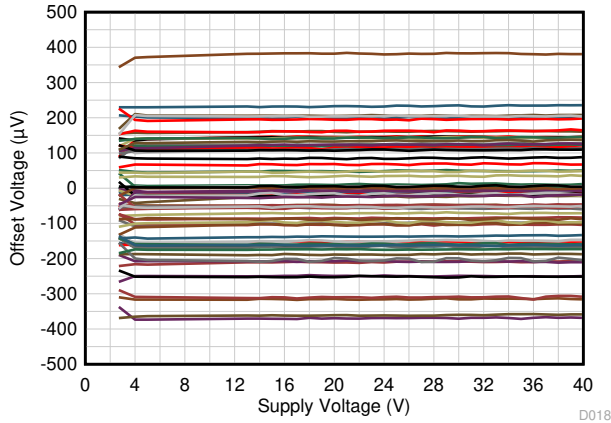


Figure 6-7. Offset Voltage vs Power Supply

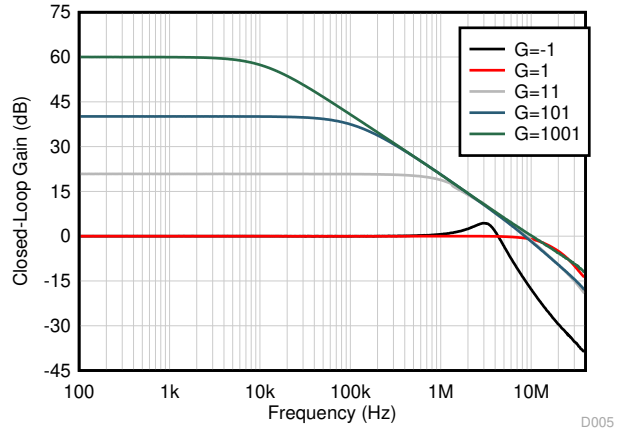


Figure 6-8. Closed-Loop Gain vs Frequency

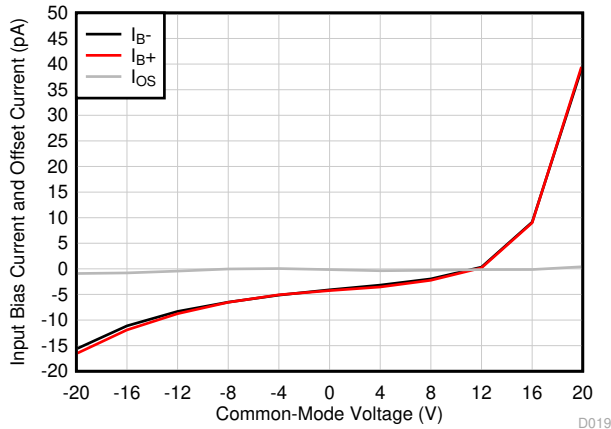


Figure 6-9. Input Bias Current and Offset Current vs Common-Mode Voltage

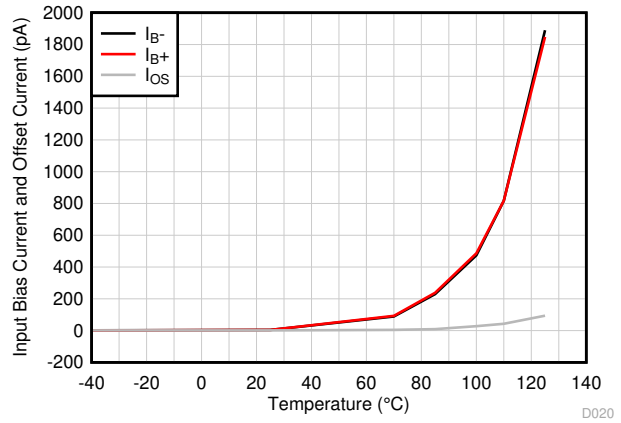
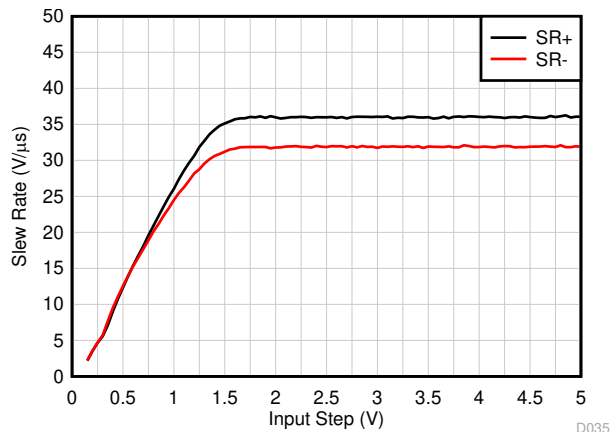


Figure 6-10. Input Bias Current and Offset Current vs Temperature



$G = +1, C_L = 20 \text{ pF}$

Figure 6-11. Slew Rate vs Input Step Voltage

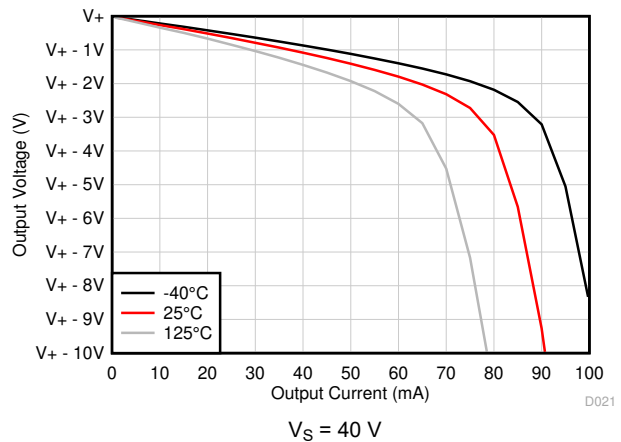
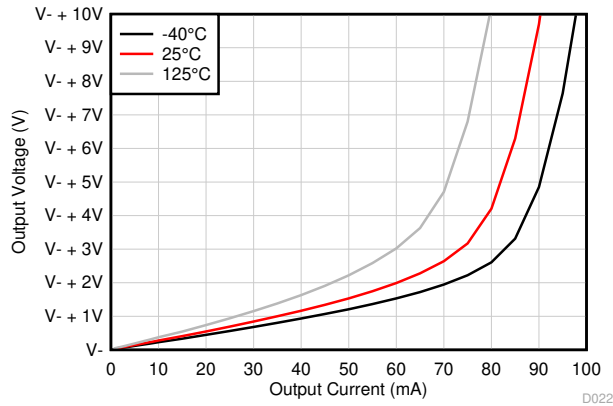
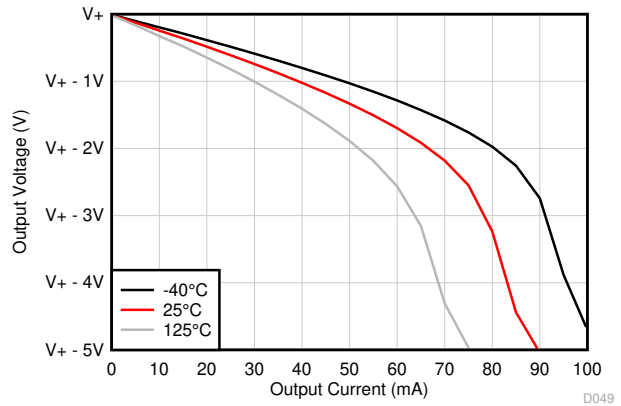


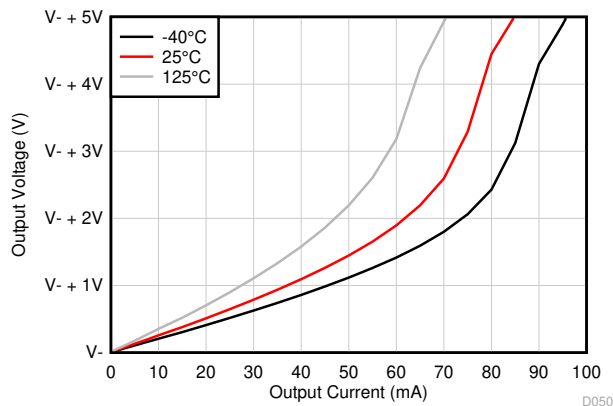
Figure 6-12. Output Voltage Swing vs Output Current (Sourcing)



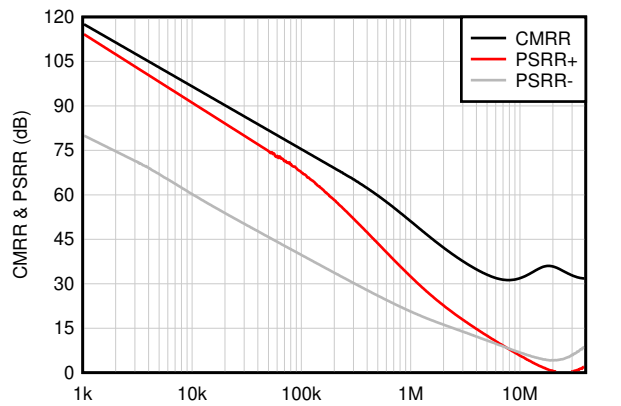
**Figure 6-13. Output Voltage Swing vs Output Current (Sinking)**



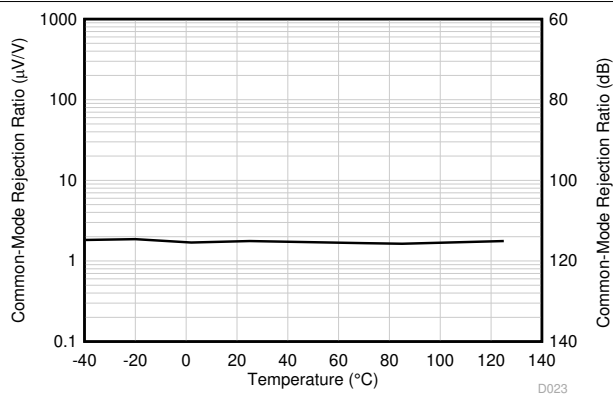
**Figure 6-14. Output Voltage Swing vs Output Current (Sourcing)**



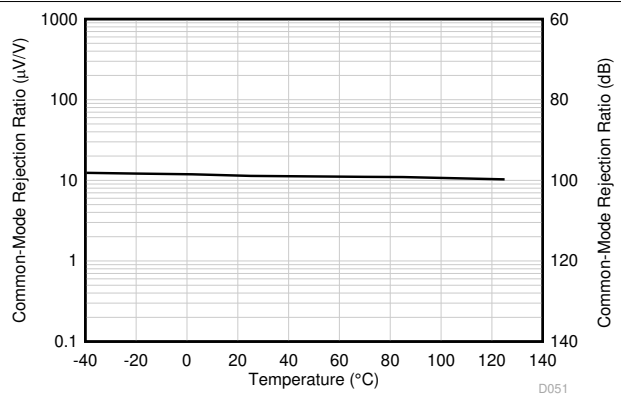
**Figure 6-15. Output Voltage Swing vs Output Current (Sinking)**



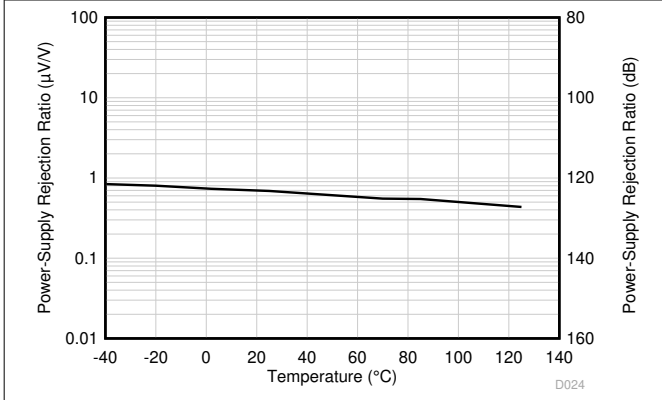
**Figure 6-16. CMRR and PSRR vs Frequency**



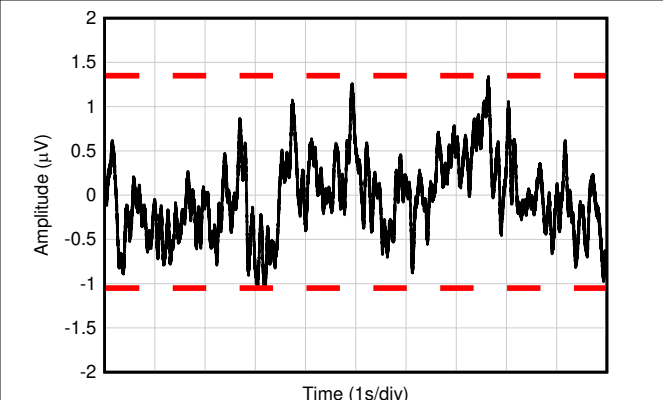
**Figure 6-17. CMRR vs Temperature**



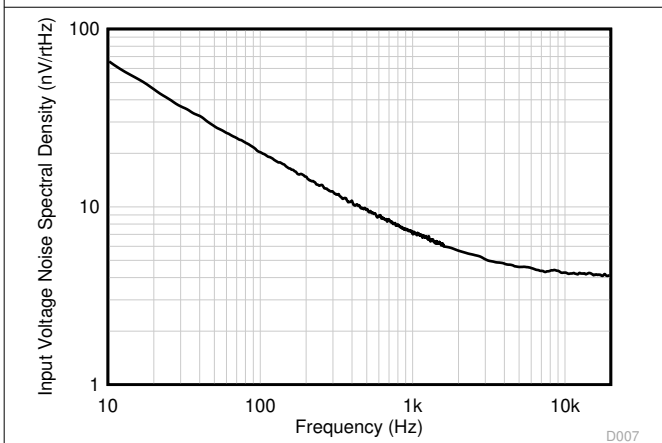
**Figure 6-18. CMRR vs Temperature**



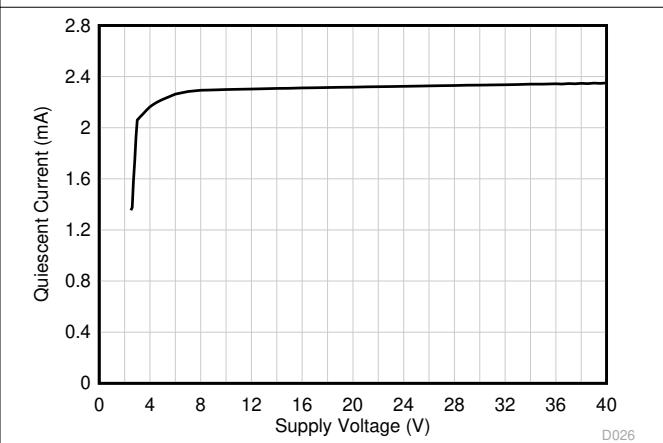
**Figure 6-19. PSRR vs Temperature**



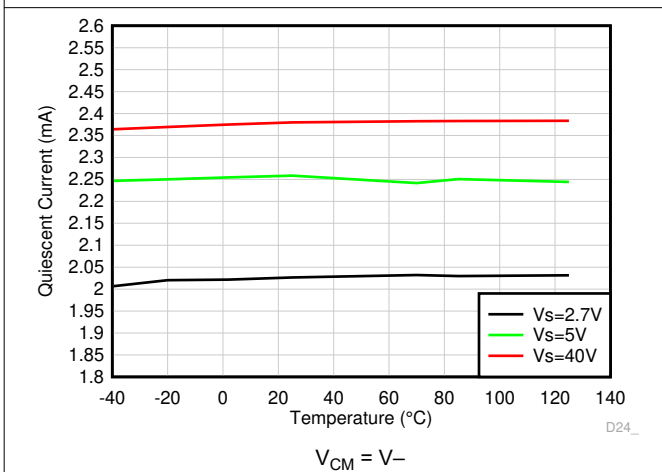
**Figure 6-20. 0.1-Hz to 10-Hz Noise**



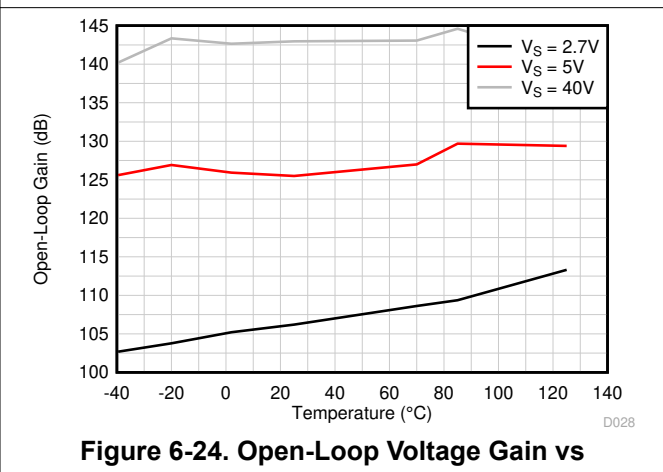
**Figure 6-21. Input Voltage Noise Spectral Density vs Frequency**



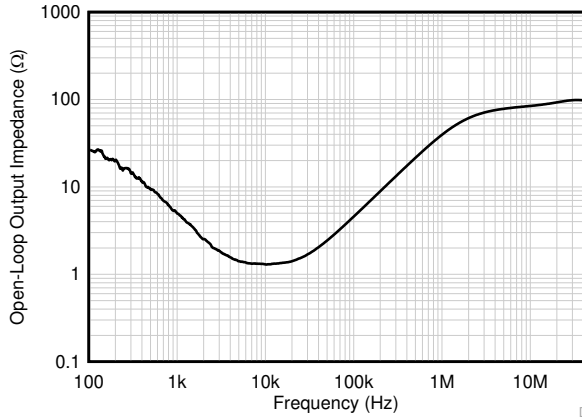
**Figure 6-22. Quiescent Current vs Supply Voltage**  
 $V_{CM} = V^-$



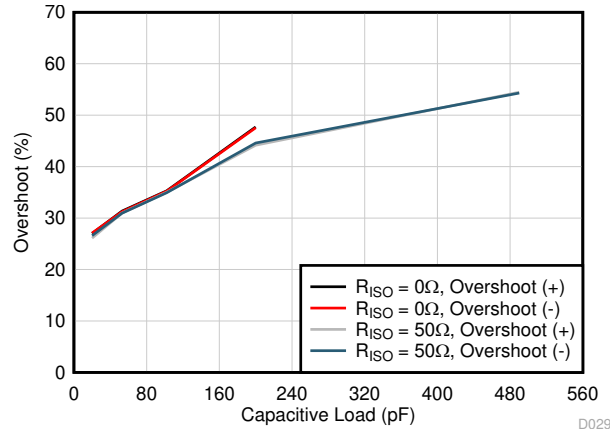
**Figure 6-23. Quiescent Current vs Temperature**  
 $V_{CM} = V^-$



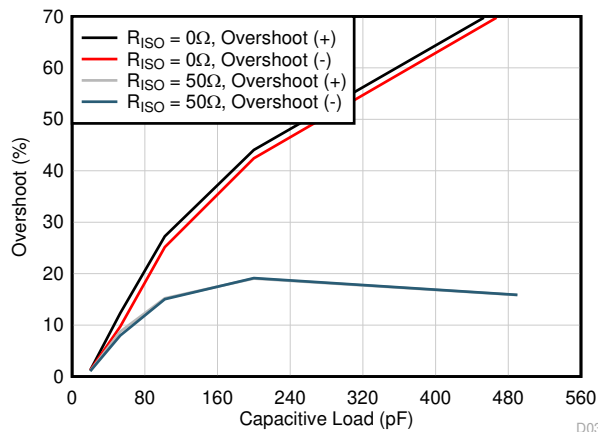
**Figure 6-24. Open-Loop Voltage Gain vs Temperature (dB)**



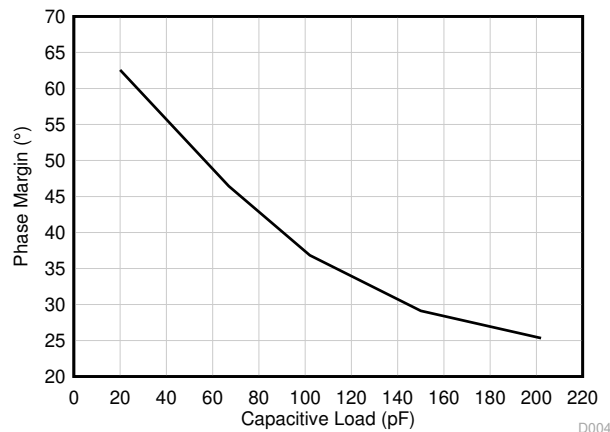
**Figure 6-25. Open-Loop Output Impedance vs Frequency**



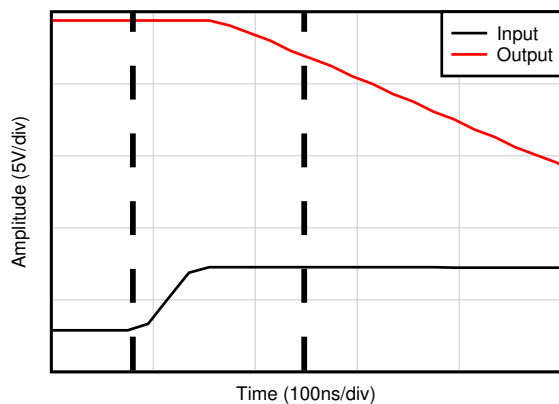
**Figure 6-26. Small-Signal Overshoot vs Capacitive Load**



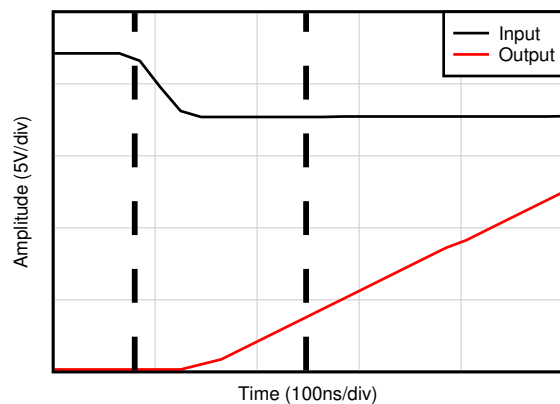
**Figure 6-27. Small-Signal Overshoot vs Capacitive Load**



**Figure 6-28. Phase Margin vs Capacitive Load**



**Figure 6-29. Positive Overload Recovery**



**Figure 6-30. Negative Overload Recovery**

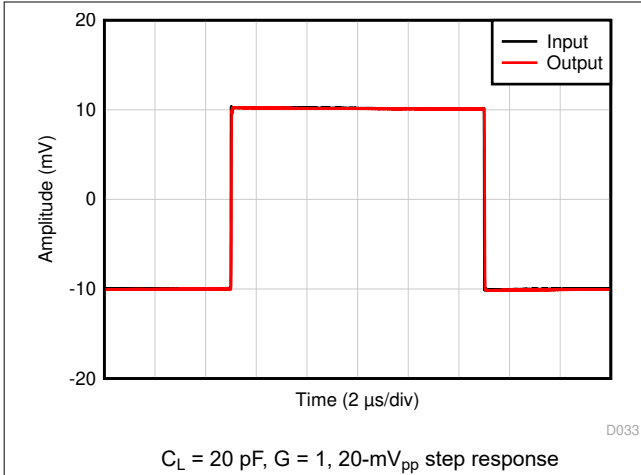


Figure 6-31. Small-Signal Step Response

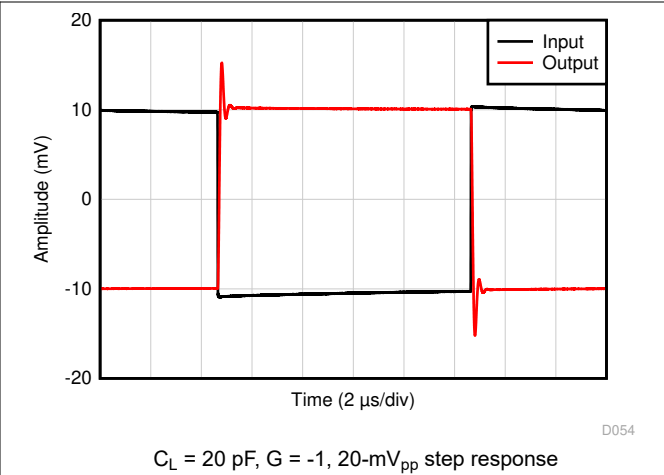


Figure 6-32. Small-Signal Step Response

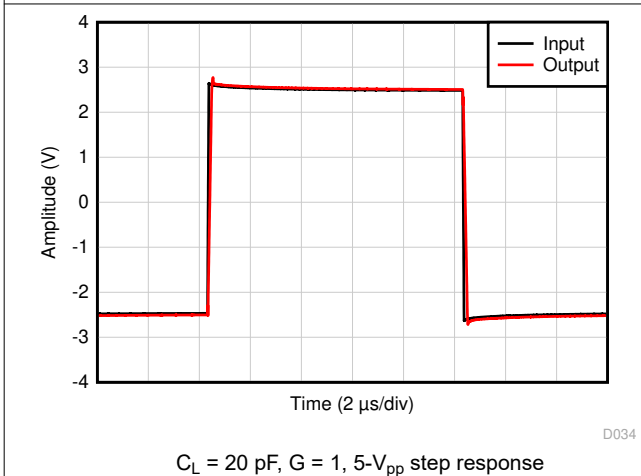


Figure 6-33. Large-Signal Step Response

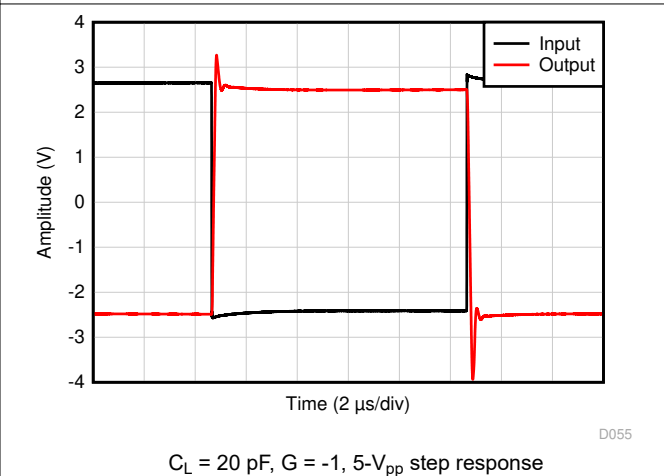


Figure 6-34. Large-Signal Step Response

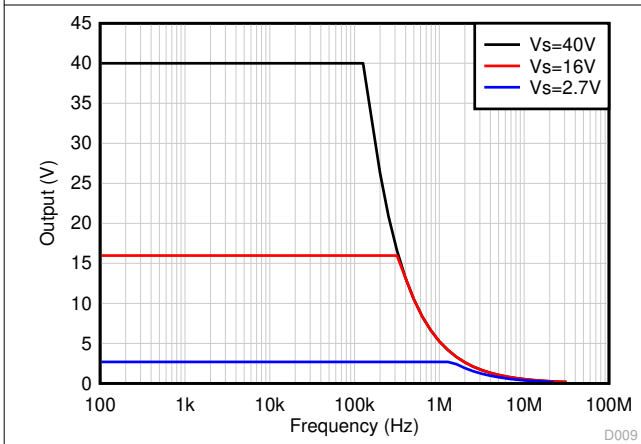


Figure 6-35. Maximum Output Voltage vs Frequency

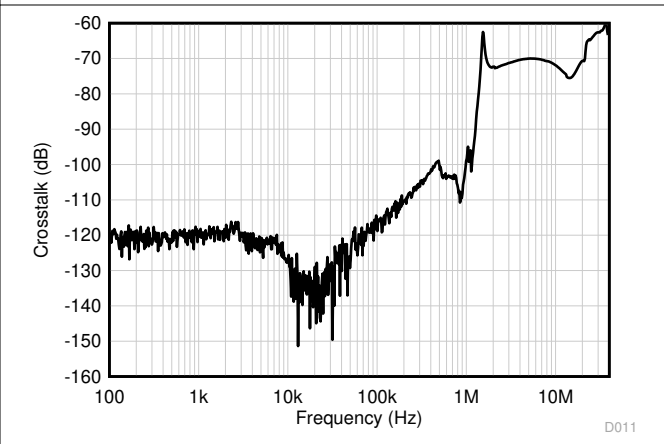
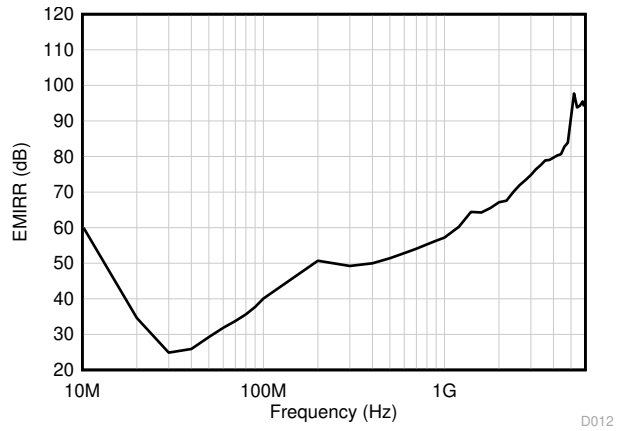


Figure 6-36. Channel Separation vs Frequency



**Figure 6-37. EMIRR (Electromagnetic Interference Rejection Ratio) vs Frequency**



## 7 Detailed Description

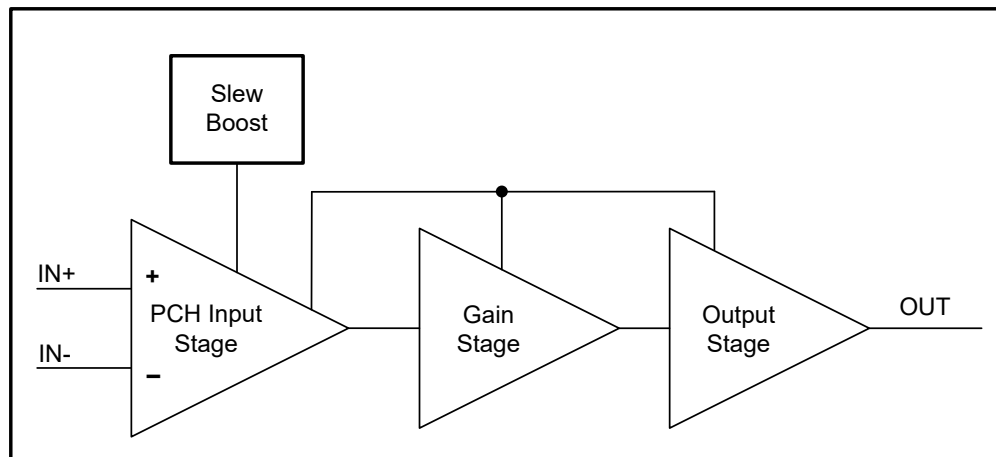
### 7.1 Overview

The TLV936x family (TLV9361, TLV9362, and TLV9364) is a family of 40-V, cost-optimized operational amplifiers. These devices offer strong general-purpose DC and AC specifications, including rail-to-rail output, low offset ( $\pm 400 \mu\text{V}$ , typ), low offset drift ( $\pm 1.25 \mu\text{V}/^\circ\text{C}$ , typ), and 10.6-MHz bandwidth.

Convenient features such as wide differential input-voltage range, high output current ( $\pm 60 \text{ mA}$ ), and high slew rate ( $25 \text{ V}/\mu\text{s}$ ) make the TLV936x a robust operational amplifier for high-voltage, cost-sensitive applications.

The TLV936x family of op amps is available in standard packages and is specified from  $-40^\circ\text{C}$  to  $125^\circ\text{C}$ .

### 7.2 Functional Block Diagram



## 7.3 Feature Description

### 7.3.1 EMI Rejection

The TLV936x uses integrated electromagnetic interference (EMI) filtering to reduce the effects of EMI from sources such as wireless communications and densely-populated boards with a mix of analog signal chain and digital components. EMI immunity can be improved with circuit design techniques; the TLV936x benefits from these design improvements. Texas Instruments has developed the ability to accurately measure and quantify the immunity of an operational amplifier over a broad frequency spectrum extending from 10 MHz to 6 GHz. [Figure 7-1](#) shows the results of this testing on the TLV936x. [Table 7-1](#) shows the EMIRR IN+ values for the TLV936x at particular frequencies commonly encountered in real-world applications. [Table 7-1](#) lists applications that may be centered on or operated near the particular frequency shown. The [EMI Rejection Ratio of Operational Amplifiers](#) application report contains detailed information on the topic of EMIRR performance as it relates to op amps and is available for download from [www.ti.com](http://www.ti.com).

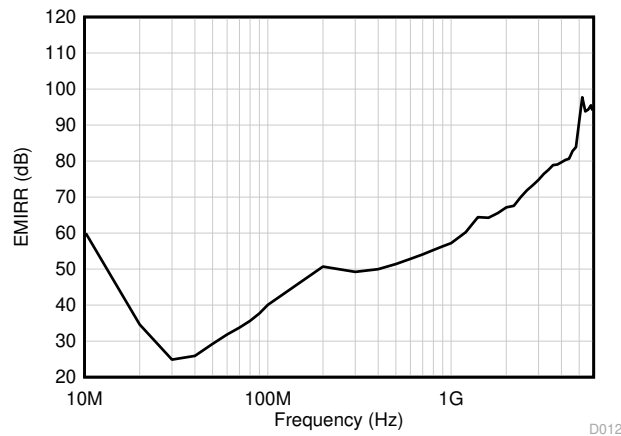


Figure 7-1. EMIRR Testing

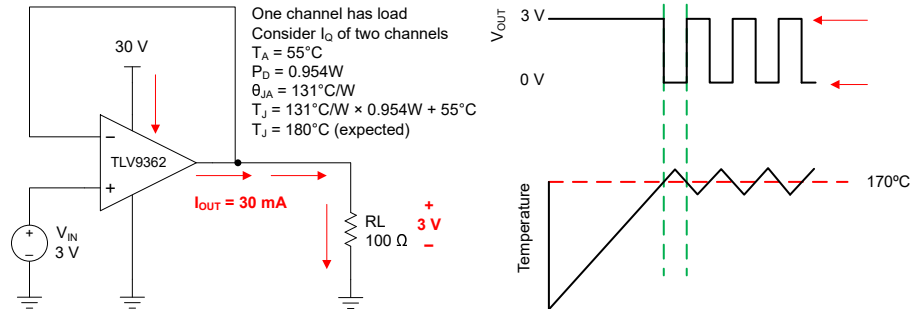
Table 7-1. TLV936x EMIRR IN+ for Frequencies of Interest

FREQUENCY	APPLICATION OR ALLOCATION	EMIRR IN+
400 MHz	Mobile radio, mobile satellite, space operation, weather, radar, ultra-high frequency (UHF) applications	50.0 dB
900 MHz	Global system for mobile communications (GSM) applications, radio communication, navigation, GPS (to 1.6 GHz), GSM, aeronautical mobile, UHF applications	56.3 dB
1.8 GHz	GSM applications, mobile personal communications, broadband, satellite, L-band (1 GHz to 2 GHz)	65.6 dB
2.4 GHz	802.11b, 802.11g, 802.11n, Bluetooth®, mobile personal communications, industrial, scientific and medical (ISM) radio band, amateur radio and satellite, S-band (2 GHz to 4 GHz)	70.0 dB
3.6 GHz	Radiolocation, aero communication and navigation, satellite, mobile, S-band	78.9 dB
5 GHz	802.11a, 802.11n, aero communication and navigation, mobile communication, space and satellite operation, C-band (4 GHz to 8 GHz)	91.0 dB

### 7.3.2 Thermal Protection

The internal power dissipation of any amplifier causes its internal (junction) temperature to rise. This phenomenon is called *self heating*. The absolute maximum junction temperature of the TLV936x is 150°C. Exceeding this temperature causes damage to the device. The TLV936x has a thermal protection feature that reduces damage from self heating. The protection works by monitoring the temperature of the device and turning off the op amp output drive for temperatures above 170°C. [Figure 7-2](#) shows an application example for the TLV9362 that has significant self heating because of its power dissipation (0.954 W). In this example, both channels have a quiescent power dissipation while one of the channels has a significant load. Thermal calculations indicate that for an ambient temperature of 55°C, the device junction temperature reaches 180°C. The actual device, however, turns off the output drive to recover towards a safe junction temperature. [Figure 7-2](#) shows how the circuit behaves during thermal protection. During normal operation, the device acts as a buffer so the output is 3 V. When self heating causes the device junction temperature to increase above the internal limit,

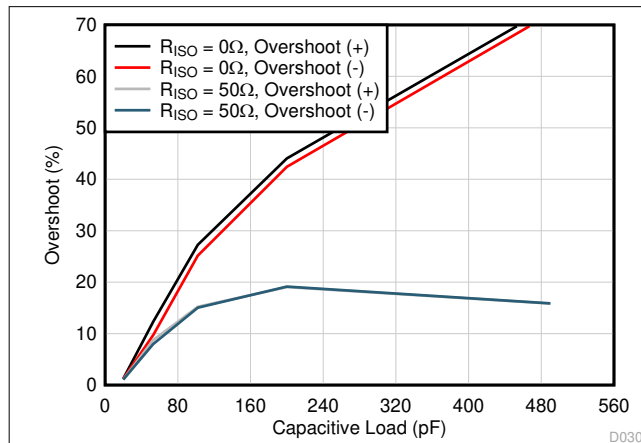
the thermal protection forces the output to a high-impedance state and the output is pulled to ground through resistor  $R_L$ . If the condition that caused excessive power dissipation is not removed, the amplifier will oscillate between a shutdown and enabled state until the output fault is corrected. Please note that thermal performance can vary greatly depending on the package selected and the PCB layout design. This example uses the thermal performance of the SOIC (8) package.



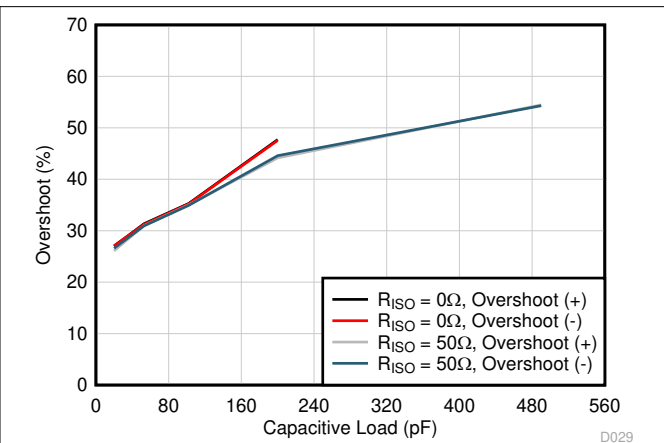
**Figure 7-2. Thermal Protection**

### 7.3.3 Capacitive Load and Stability

The TLV936x features an output stage capable of driving moderate capacitive loads, and by leveraging an isolation resistor, the device can easily be configured to driver large capacitive loads. Increasing the gain enhances the ability of the amplifier to drive greater capacitive loads; see [Figure 7-3](#) and [Figure 7-4](#). The particular op amp circuit configuration, layout, gain, and output loading are some of the factors to consider when establishing whether an amplifier is stable in operation.

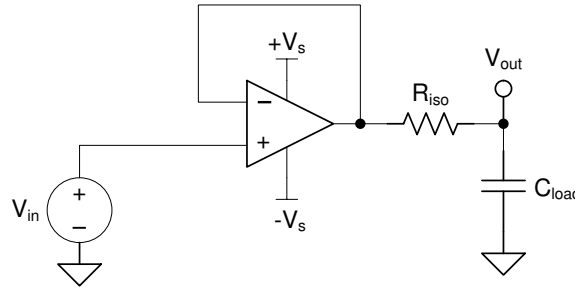


**Figure 7-3. Small-Signal Overshoot vs Capacitive Load (20-mV<sub>pp</sub> Output Step, G = +1)**



**Figure 7-4. Small-Signal Overshoot vs Capacitive Load (20-mV<sub>pp</sub> Output Step, G = -1)**

For additional drive capability in unity-gain configurations, improve capacitive load drive by inserting a small resistor,  $R_{ISO}$ , in series with the output, as shown in [Figure 7-5](#). This resistor significantly reduces ringing and maintains DC performance for purely capacitive loads. However, if a resistive load is in parallel with the capacitive load, then a voltage divider is created, thus introducing a gain error at the output and slightly reducing the output swing. The error introduced is proportional to the ratio  $R_{ISO} / R_L$ , and is generally negligible at low output levels. A high capacitive load drive makes the TLV936x well suited for applications such as reference buffers, MOSFET gate drives, and cable-shield drives. The circuit shown in [Figure 7-5](#) uses an isolation resistor,  $R_{ISO}$ , to stabilize the output of an op amp.  $R_{ISO}$  modifies the open-loop gain of the system for increased phase margin.

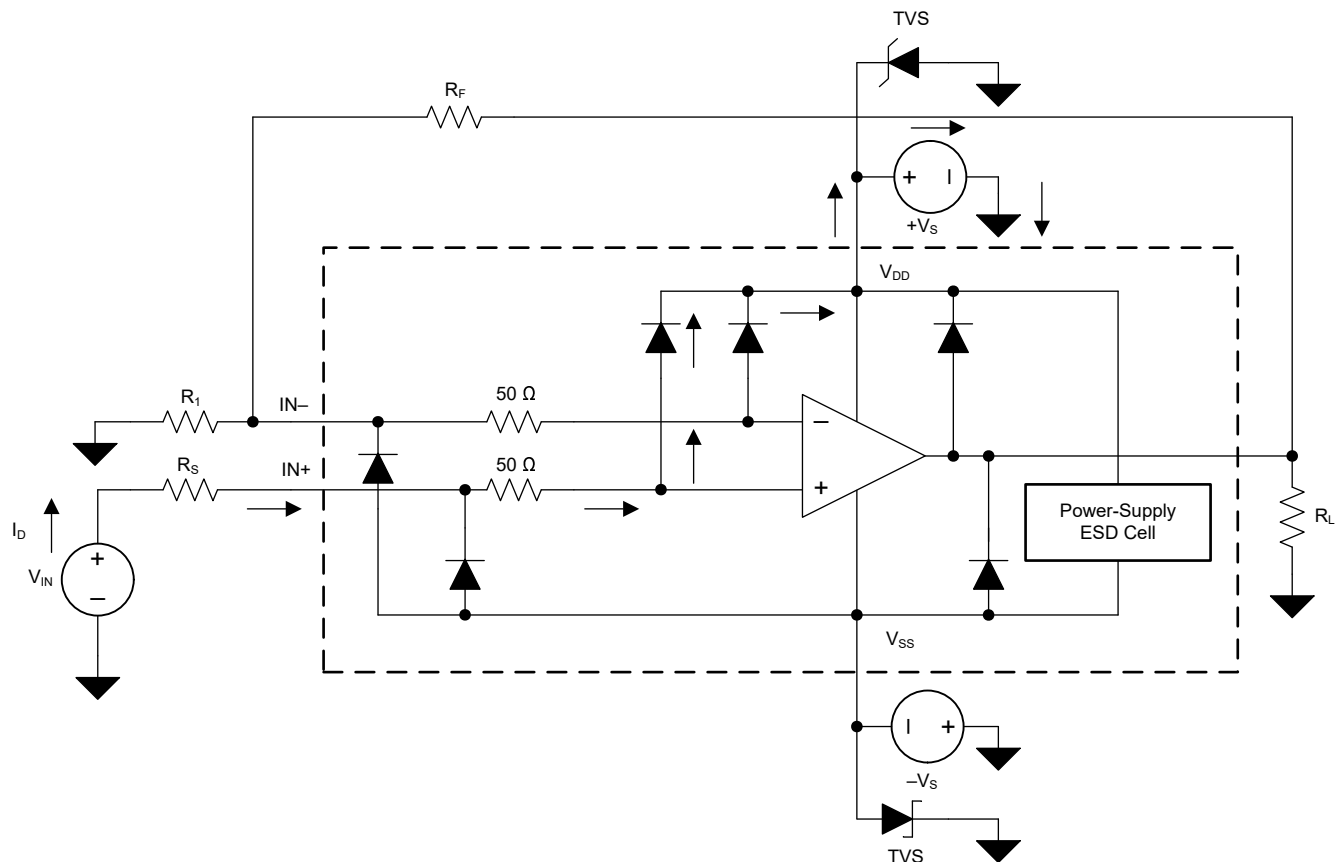


**Figure 7-5. Extending Capacitive Load Drive With the TLV9361**

### 7.3.4 Electrical Overstress

Designers often ask questions about the capability of an operational amplifier to withstand electrical overstress (EOS). These questions tend to focus on the device inputs, but may involve the supply voltage pins or even the output pin. Each of these different pin functions have electrical stress limits determined by the voltage breakdown characteristics of the particular semiconductor fabrication process and specific circuits connected to the pin. Additionally, internal electrostatic discharge (ESD) protection is built into these circuits to protect them from accidental ESD events both before and during product assembly.

Having a good understanding of this basic ESD circuitry and its relevance to an electrical overstress event is helpful. Figure 7-6 shows an illustration of the ESD circuits contained in the TLV936x (indicated by the dashed line area). The ESD protection circuitry involves several current-steering diodes connected from the input and output pins and routed back to the internal power-supply lines, where the diodes meet at an absorption device or the power-supply ESD cell, internal to the operational amplifier. This protection circuitry is intended to remain inactive during normal circuit operation.



**Figure 7-6. Equivalent Internal ESD Circuitry Relative to a Typical Circuit Application**

An ESD event is very short in duration and very high voltage (for example; 1 kV, 100 ns), whereas an EOS event is long duration and lower voltage (for example; 50 V, 100 ms). The ESD diodes are designed for out-of-circuit ESD protection (that is; during assembly, test, and storage of the device before being soldered to the PCB). During an ESD event, the ESD signal is passed through the ESD steering diodes to an absorption circuit (labeled ESD power-supply circuit). The ESD absorption circuit clamps the supplies to a safe level.

Although this behavior is necessary for out-of-circuit protection, excessive current and damage is caused if activated in-circuit. A transient voltage suppressors (TVS) can be used to prevent against damage caused by turning on the ESD absorption circuit during an in-circuit ESD event. Using the appropriate current limiting resistors and TVS diodes allows for the use of device ESD diodes to protect against EOS events.

### 7.3.5 Overload Recovery

Overload recovery is defined as the time required for the op amp output to recover from a saturated state to a linear state. The output devices of the op amp enter a saturation region when the output voltage exceeds the rated operating voltage, either due to the high input voltage or the high gain. After the device enters the saturation region, the charge carriers in the output devices require time to return back to the linear state. After the charge carriers return back to the linear state, the device begins to slew at the specified slew rate. Thus, the propagation delay in case of an overload condition is the sum of the overload recovery time and the slew time. The overload recovery time for the TLV936x is approximately 170 ns.

### 7.3.6 Typical Specifications and Distributions

Designers often have questions about a typical specification of an amplifier in order to design a more robust circuit. Due to natural variation in process technology and manufacturing procedures, every specification of an amplifier will exhibit some amount of deviation from the ideal value, like an amplifier's input offset voltage. These deviations often follow *Gaussian* ("bell curve"), or *normal* distributions, and circuit designers can leverage this information to guardband their system, even when there is not a minimum or maximum specification in the [Electrical Characteristics](#) table.

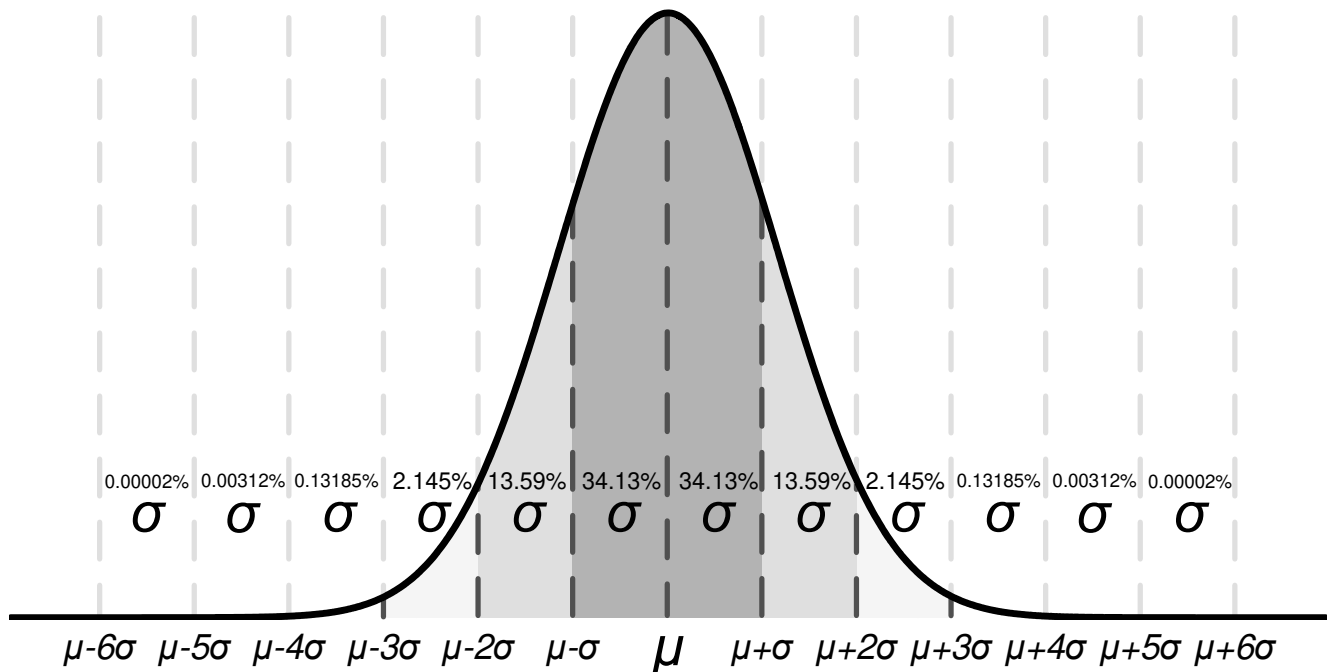


Figure 7-7. Ideal Gaussian Distribution

Figure 7-7 shows an example distribution, where  $\mu$ , or  $mu$ , is the mean of the distribution, and where  $\sigma$ , or *sigma*, is the standard deviation of a system. For a specification that exhibits this kind of distribution, approximately two-thirds (68.26%) of all units can be expected to have a value within one standard deviation, or one sigma, of the mean (from  $\mu - \sigma$  to  $\mu + \sigma$ ).

Depending on the specification, values listed in the *typical* column of the [Electrical Characteristics](#) table are represented in different ways. As a general rule of thumb, if a specification naturally has a nonzero mean (for example, like gain bandwidth), then the typical value is equal to the mean ( $\mu$ ). However, if a specification naturally has a mean near zero (like input offset voltage), then the typical value is equal to the mean plus one standard deviation ( $\mu + \sigma$ ) in order to most accurately represent the typical value.

You can use this chart to calculate approximate probability of a specification in a unit; for example, for TLV936x, the typical input voltage offset is 400  $\mu$ V, so 68.2% of all TLV936x devices are expected to have an offset from  $-400 \mu$ V to 400  $\mu$ V. At 4  $\sigma$  ( $\pm 1600 \mu$ V), 99.9937% of the distribution has an offset voltage less than  $\pm 1600 \mu$ V, which means 0.0063% of the population is outside of these limits, which corresponds to about 1 in 15,873 units.

Specifications with a value in the minimum or maximum column are assured by TI, and units outside these limits will be removed from production material. For example, the TLV936x family has a maximum offset voltage of 1.7 mV at 125°C, and even though this corresponds to about 4.25  $\sigma$  ( $\approx 2$  in 100,000 units), which is unlikely, TI assures that any unit with larger offset than 1.7 mV will be removed from production material.

For specifications with no value in the minimum or maximum column, consider selecting a sigma value of sufficient guardband for your application, and design worst-case conditions using this value. For example, the 6- $\sigma$  value corresponds to about 1 in 500 million units, which is an extremely unlikely chance, and could be an option as a wide guardband to design a system around. In this case, the TLV936x family does not have a maximum or minimum for offset voltage drift, but based on the typical value of 1.25  $\mu$ V/°C in the [Electrical Characteristics](#) table, it can be calculated that the 6- $\sigma$  value for offset voltage drift is about 7.5  $\mu$ V/°C. When designing for worst-case system conditions, this value can be used to estimate the worst possible offset across temperature without having an actual minimum or maximum value.

However, process variation and adjustments over time can shift typical means and standard deviations, and unless there is a value in the minimum or maximum specification column, TI cannot assure the performance of a device. This information should be used only to estimate the performance of a device.

## 7.4 Device Functional Modes

The TLV936x has a single functional mode and is operational when the power-supply voltage is greater than 4.5 V ( $\pm 2.25$  V). The maximum power supply voltage for the TLV936x is 40 V ( $\pm 20$  V).

## 8 Application Information Disclaimer

### Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

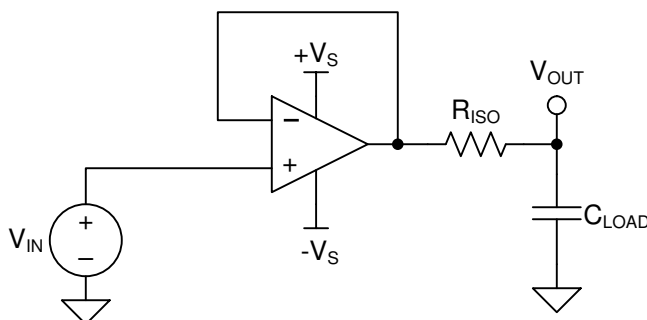
### 8.1 Application Information

The TLV936x family offers excellent DC precision and DC performance. These devices operate up to 40-V supply rails and offer true rail-to-rail output, low offset voltage and offset voltage drift, as well as 10.6-MHz bandwidth and high output drive. These features make the TLV936x a robust, high-performance operational amplifier for high-voltage cost-sensitive applications.

### 8.2 Typical Applications

#### 8.2.1 Unity-Gain Buffer With $R_{ISO}$ Stability Compensation

This circuit can drive capacitive loads (such as cable shields, reference buffers, MOSFET gates, and diodes). The circuit uses an isolation resistor ( $R_{ISO}$ ) to stabilize the output of an operational amplifier.  $R_{ISO}$  modifies the open-loop gain of the system to ensure that the circuit has sufficient phase margin.



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**Figure 8-1. Unity-Gain Buffer With  $R_{ISO}$  Stability Compensation**

#### 8.2.1.1 Design Requirements

The design requirements are:

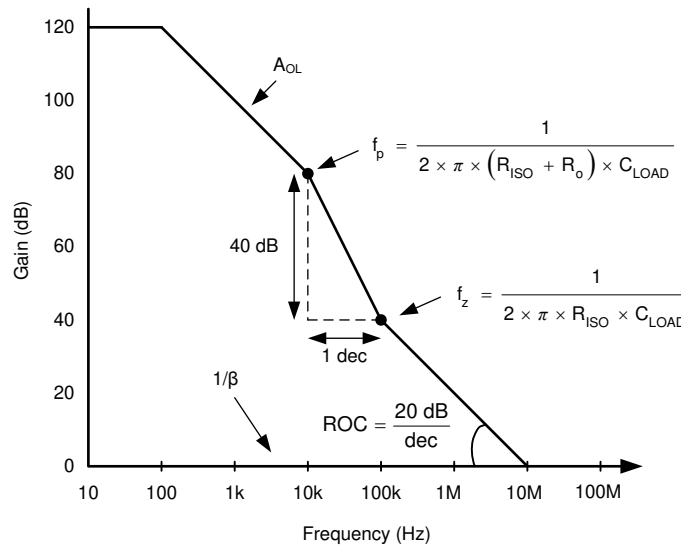
- Supply voltage: 30 V ( $\pm 15$  V)
- Capacitive loads: 20 pF, 100 pF, 200 pF, and 500 pF
- Phase margin: 45°

#### 8.2.1.2 Detailed Design Procedure

Figure 8-1 shows a unity-gain buffer driving a capacitive load. Equation 1 shows the transfer function for the circuit in Figure 8-1. Figure 8-1 does not show the open-loop output resistance of the operational amplifier ( $R_o$ ).

$$T(s) = \frac{1 + C_{LOAD} \times R_{ISO} \times s}{1 + (R_o + R_{ISO}) \times C_{LOAD} \times s} \quad (1)$$

The transfer function in Equation 1 has a pole and a zero. The frequency of the pole ( $f_p$ ) is determined by ( $R_o + R_{ISO}$ ) and  $C_{LOAD}$ . The  $R_{ISO}$  and  $C_{LOAD}$  components determine the frequency of the zero ( $f_z$ ). A stable system is obtained by selecting  $R_{ISO}$  so that the rate of closure (ROC) between the open-loop gain ( $A_{OL}$ ) and  $1/\beta$  is 20 dB per decade. Figure 8-2 shows the concept. The  $1/\beta$  curve for a unity-gain buffer is 0 dB.



**Figure 8-2. Unity-Gain Amplifier With  $R_{ISO}$  Compensation**

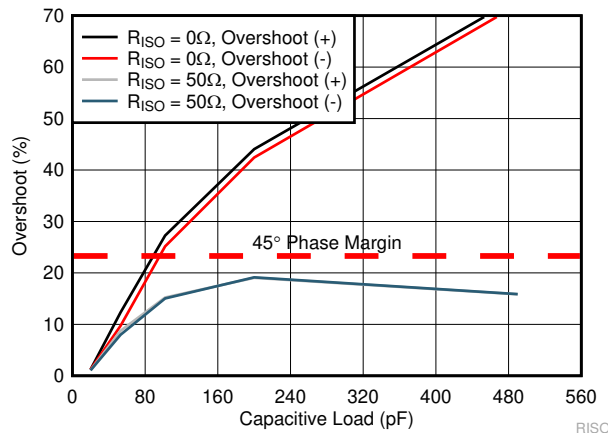
Typically, ROC stability analysis is simulated. The validity of the analysis depends on multiple factors, especially the accurate modeling of  $R_o$ . In addition to simulating the ROC, a robust stability analysis includes a measurement of overshoot percentage and/or AC gain peaking of the circuit using a function generator, oscilloscope, and gain and phase analyzer. Phase margin is then calculated from these measurements. [Table 8-1](#) shows the overshoot percentage and AC gain peaking that correspond to a phase margin of  $45^\circ$ . For more details on this design and other alternative devices that can replace the TLV936x, see the [Capacitive Load Drive Solution Using an Isolation Resistor](#) precision design.

**Table 8-1. Phase Margin versus Overshoot and AC Gain Peaking**

PHASE MARGIN	OVERSHOOT	AC GAIN PEAKING
$45^\circ$	23.3%	2.35 dB

### 8.2.1.3 Application Curve

The values of  $R_{ISO}$  that yield phase margins of  $45^\circ$ , or other typical design targets such as  $60^\circ$ , for various capacitive loads can be determined using the described methodology. [Figure 8-3](#) shows the results that can be achieved with no  $R_{ISO}$  compensation vs an  $R_{ISO}$  of  $50 \Omega$ .



**Figure 8-3. Small-Signal Overshoot vs Capacitive Load With  $R_{ISO}$**



## 9 Power Supply Recommendations

The TLV936x is specified for operation from 4.5 V to 40 V ( $\pm 2.25$  V to  $\pm 20$  V); many specifications apply from  $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ .

### CAUTION

Supply voltages larger than 40 V can permanently damage the device; see the [Absolute Maximum Ratings](#) table.

Place 0.1- $\mu\text{F}$  bypass capacitors close to the power-supply pins to reduce errors coupling in from noisy or high-impedance power supplies. For more detailed information on bypass capacitor placement, refer to the [Layout](#) section.

## 10 Layout

### 10.1 Layout Guidelines

For best operational performance of the device, use good PCB layout practices, including:

- Noise can propagate into analog circuitry through the power pins of the circuit as a whole and op amp itself. Bypass capacitors are used to reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
  - Connect low-ESR, 0.1- $\mu\text{F}$  ceramic bypass capacitors between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable for single-supply applications.
- Separate grounding for analog and digital portions of circuitry is one of the simplest and most-effective methods of noise suppression. One or more layers on multilayer PCBs are usually devoted to ground planes. A ground plane helps distribute heat and reduces EMI noise pickup. Make sure to physically separate digital and analog grounds paying attention to the flow of the ground current.
- In order to reduce parasitic coupling, run the input traces as far away from the supply or output traces as possible. If these traces cannot be kept separate, crossing the sensitive trace perpendicular is much better as opposed to in parallel with the noisy trace.
- Place the external components as close to the device as possible. As illustrated in [Figure 10-2](#), keeping RF and RG close to the inverting input minimizes parasitic capacitance.
- Keep the length of input traces as short as possible. Always remember that the input traces are the most sensitive part of the circuit.
- Consider a driven, low-impedance guard ring around the critical traces. A guard ring can significantly reduce leakage currents from nearby traces that are at different potentials.
- Cleaning the PCB following board assembly is recommended for best performance.
- Any precision integrated circuit may experience performance shifts due to moisture ingress into the plastic package. Following any aqueous PCB cleaning process, baking the PCB assembly is recommended to remove moisture introduced into the device packaging during the cleaning process. A low temperature, post cleaning bake at  $85^{\circ}\text{C}$  for 30 minutes is sufficient for most circumstances.

## 10.2 Layout Example

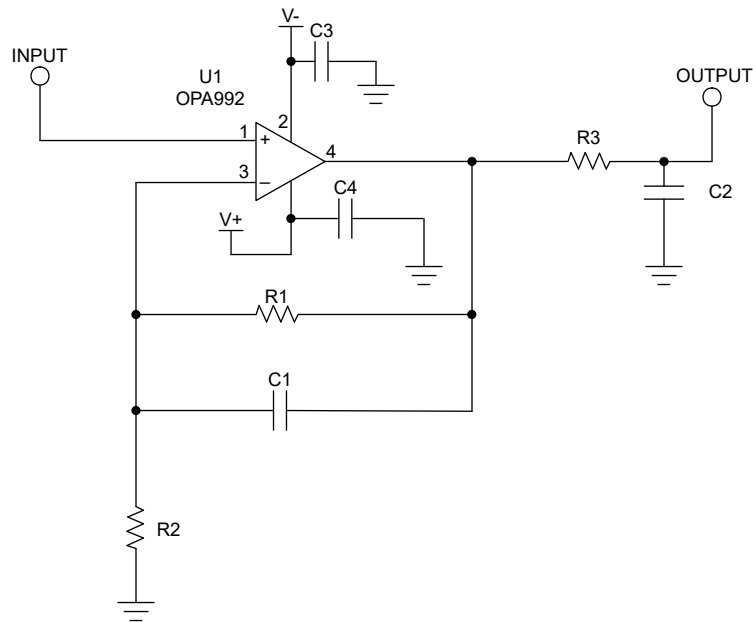


Figure 10-1. Schematic for Noninverting Configuration Layout Example

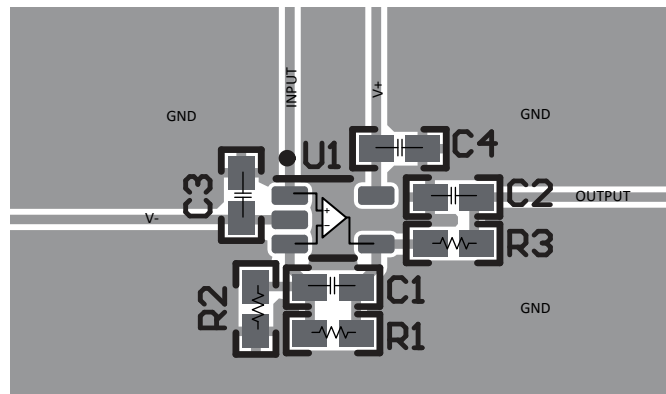


Figure 10-2. Operational Amplifier Board Layout for Noninverting Configuration - SC70 (DCK) Package

## 11 Device and Documentation Support

### 11.1 Device Support

#### 11.1.1 Development Support

##### 11.1.1.1 TINA-TI™ (Free Software Download)

TINA™ is a simple, powerful, and easy-to-use circuit simulation program based on a SPICE engine. TINA-TI is a free, fully-functional version of the TINA software, preloaded with a library of macro models in addition to a range of both passive and active models. TINA-TI provides all the conventional dc, transient, and frequency domain analysis of SPICE, as well as additional design capabilities.

Available as a [free download](#) from the Analog eLab Design Center, TINA-TI offers extensive post-processing capability that allows users to format results in a variety of ways. Virtual instruments offer the ability to select input waveforms and probe circuit nodes, voltages, and waveforms, creating a dynamic quick-start tool.

---

#### Note

These files require that either the TINA software (from DesignSoft™) or TINA-TI software be installed. Download the free TINA-TI software from the [TINA-TI folder](#).

---

##### 11.1.1.2 TI Precision Designs

The TLV936x is featured in several TI Precision Designs, available online at <http://www.ti.com/ww/en/analog/precision-designs/>. TI Precision Designs are analog solutions created by TI's precision analog applications experts and offer the theory of operation, component selection, simulation, complete PCB schematic and layout, bill of materials, and measured performance of many useful circuits.

### 11.2 Documentation Support

#### 11.2.1 Related Documentation

Texas Instruments, [Analog Engineer's Circuit Cookbook: Amplifiers](#)

Texas Instruments, [AN31 amplifier circuit collection](#) application report

Texas Instruments, [EMI Rejection Ratio of Operational Amplifiers](#) application report

Texas Instruments, [Capacitive Load Drive Solution using an Isolation Resistor](#) reference design

### 11.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com](http://ti.com). Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 11.4 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

### 11.5 Trademarks

TINA-TI™ is a trademark of Texas Instruments, Inc and DesignSoft, Inc.

TINA™ and DesignSoft™ are trademarks of DesignSoft, Inc.

TI E2E™ is a trademark of Texas Instruments.

Bluetooth® is a registered trademark of Bluetooth SIG, Inc.

All trademarks are the property of their respective owners.

## 11.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

## 11.7 Glossary

### [TI Glossary](#)

This glossary lists and explains terms, acronyms, and definitions.

## 12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

## PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TLV9361IDBVR	ACTIVE	SOT-23	DBV	5	3000	RoHS & Green	NIPDAU   SN	Level-1-260C-UNLIM	-40 to 125	T93DB	<a href="#">Samples</a>
TLV9361IDCKR	ACTIVE	SC70	DCK	5	3000	RoHS & Green	SN	Level-1-260C-UNLIM	-40 to 125	1JU	<a href="#">Samples</a>
TLV9362IDDFR	ACTIVE	SOT-23-THIN	DDF	8	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	2IDF	<a href="#">Samples</a>
TLV9362IDGKR	ACTIVE	VSSOP	DGK	8	2500	RoHS & Green	SN	Level-1-260C-UNLIM	-40 to 125	2JWT	<a href="#">Samples</a>
TLV9362IDR	ACTIVE	SOIC	D	8	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	T9362D	<a href="#">Samples</a>
TLV9362IPWR	ACTIVE	TSSOP	PW	8	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	T9362P	<a href="#">Samples</a>
TLV9364IDR	ACTIVE	SOIC	D	14	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	TLV9364D	<a href="#">Samples</a>
TLV9364IPWR	ACTIVE	TSSOP	PW	14	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	T9364PW	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

<sup>(6)</sup> Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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**OTHER QUALIFIED VERSIONS OF TLV9361, TLV9362, TLV9364 :**

- Automotive : [TLV9361-Q1](#), [TLV9362-Q1](#), [TLV9364-Q1](#)

NOTE: Qualified Version Definitions:

- Automotive - Q100 devices qualified for high-reliability automotive applications targeting zero defects

**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TLV9361IDBVR	SOT-23	DBV	5	3000	180.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
TLV9361IDCKR	SC70	DCK	5	3000	178.0	9.0	2.4	2.5	1.2	4.0	8.0	Q3
TLV9362IDDFR	SOT-23-THIN	DDF	8	3000	180.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
TLV9362IDGKR	VSSOP	DGK	8	2500	330.0	12.4	5.25	3.35	1.25	8.0	12.0	Q1
TLV9362IDR	SOIC	D	8	3000	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TLV9362IPWR	TSSOP	PW	8	3000	330.0	12.4	7.0	3.6	1.6	8.0	12.0	Q1
TLV9364IDR	SOIC	D	14	3000	330.0	16.4	6.5	9.0	2.1	8.0	16.0	Q1
TLV9364IPWR	TSSOP	PW	14	3000	330.0	12.4	6.9	5.6	1.6	8.0	12.0	Q1



## TAPE AND REEL BOX DIMENSIONS



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TLV9361IDBVR	SOT-23	DBV	5	3000	210.0	185.0	35.0
TLV9361IDCKR	SC70	DCK	5	3000	180.0	180.0	18.0
TLV9362IDDFR	SOT-23-THIN	DDF	8	3000	210.0	185.0	35.0
TLV9362IDGKR	VSSOP	DGK	8	2500	366.0	364.0	50.0
TLV9362IDR	SOIC	D	8	3000	356.0	356.0	35.0
TLV9362IPWR	TSSOP	PW	8	3000	356.0	356.0	35.0
TLV9364IDR	SOIC	D	14	3000	356.0	356.0	35.0
TLV9364IPWR	TSSOP	PW	14	3000	356.0	356.0	35.0

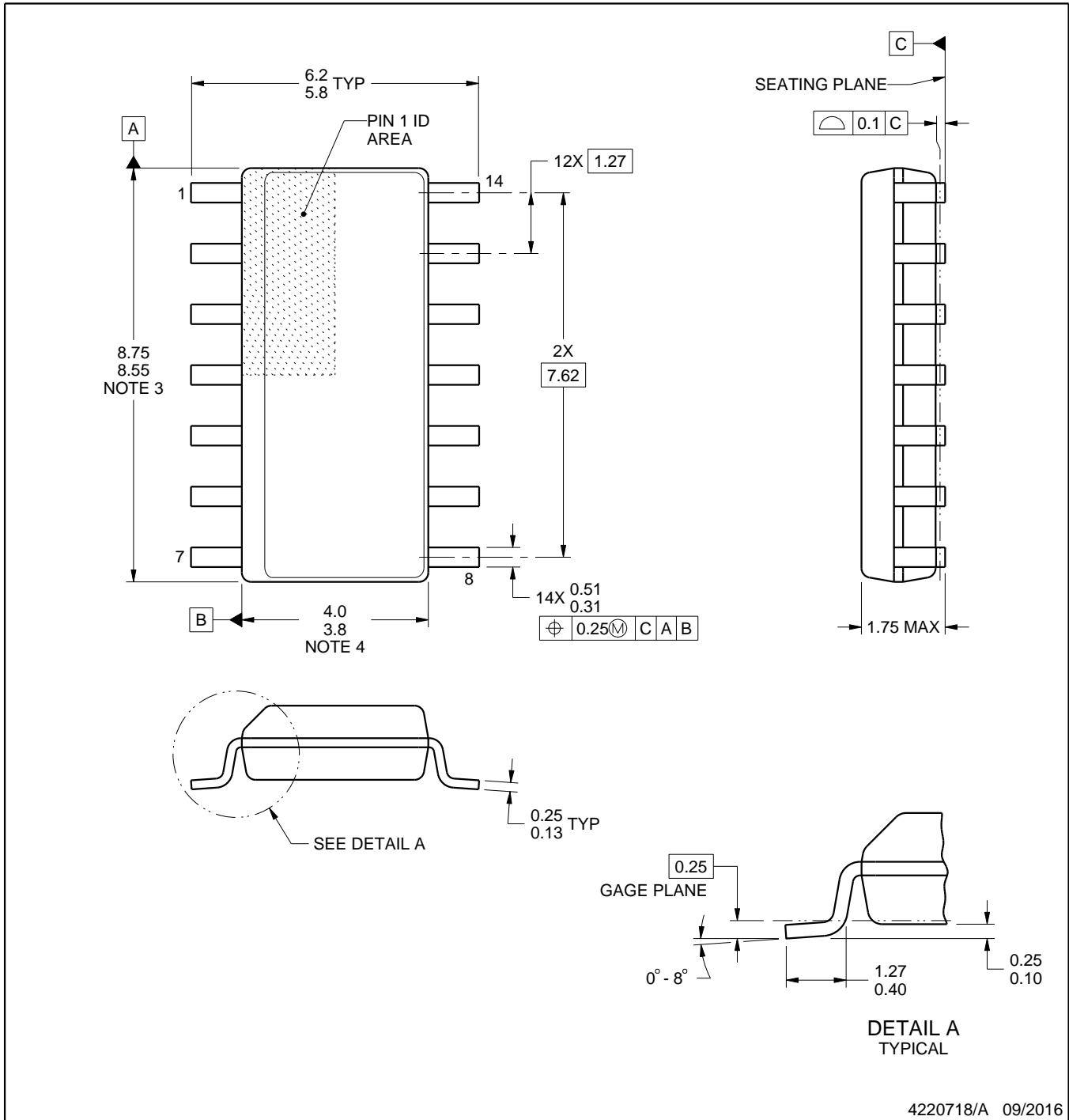
D0014A



# PACKAGE OUTLINE

## SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



4220718/A 09/2016

# EXAMPLE BOARD LAYOUT

D0014A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



LAND PATTERN EXAMPLE  
SCALE:8X



SOLDER MASK DETAILS

4220718/A 09/2016

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

D0014A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:8X

4220718/A 09/2016

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

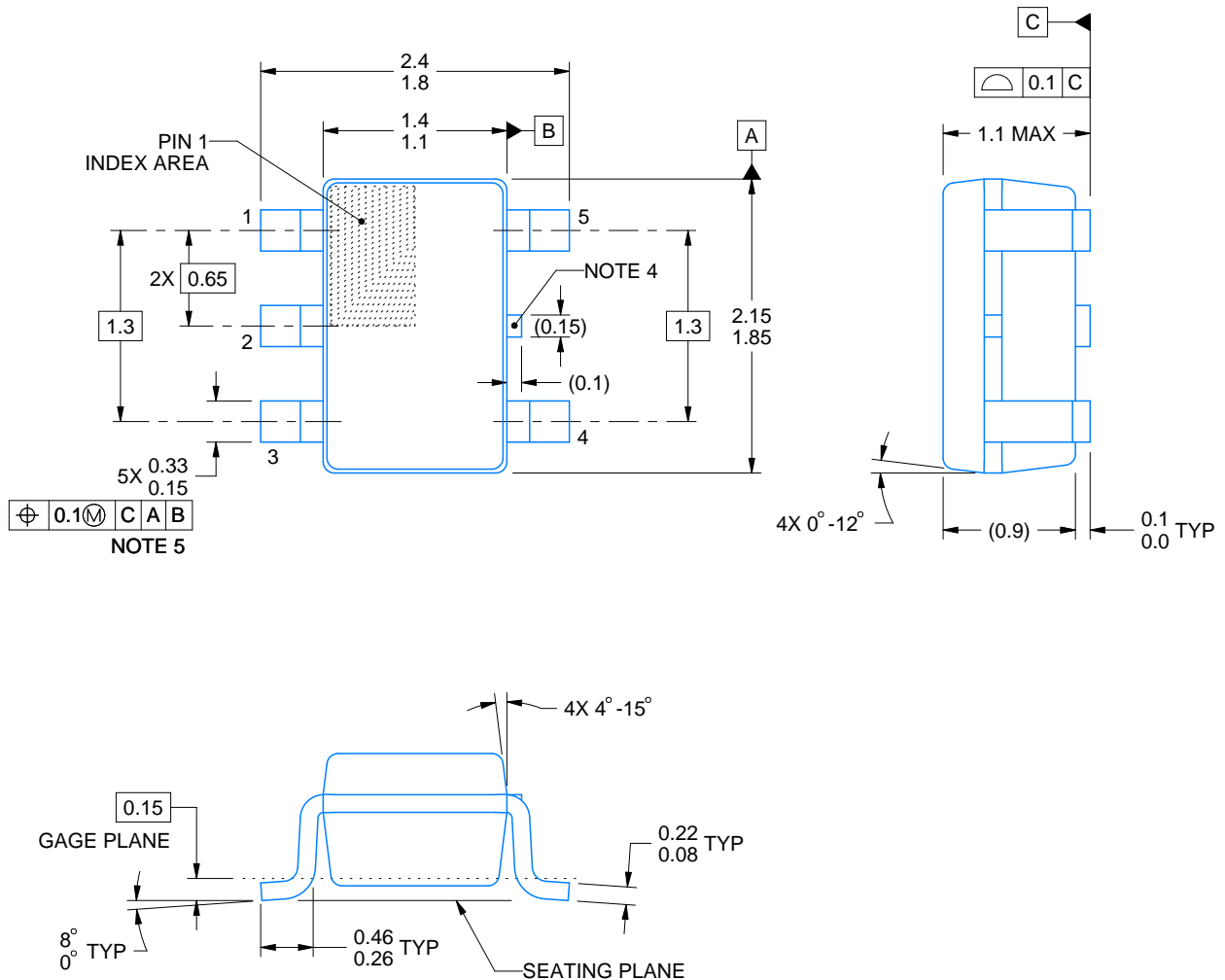


# PACKAGE OUTLINE

## DCK0005A

### SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



4214834/G 11/2024

#### NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Reference JEDEC MO-203.
4. Support pin may differ or may not be present.
5. Lead width does not comply with JEDEC.
6. Body dimensions do not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.25mm per side

# EXAMPLE BOARD LAYOUT

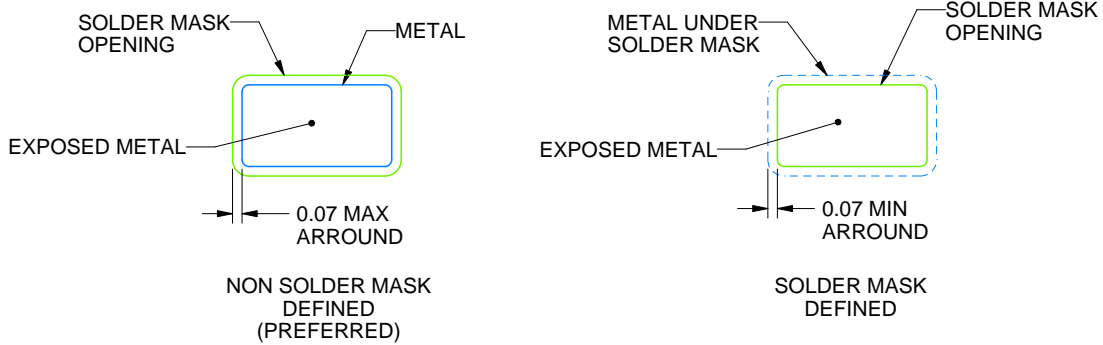
DCK0005A

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:18X



SOLDER MASK DETAILS

4214834/G 11/2024

NOTES: (continued)

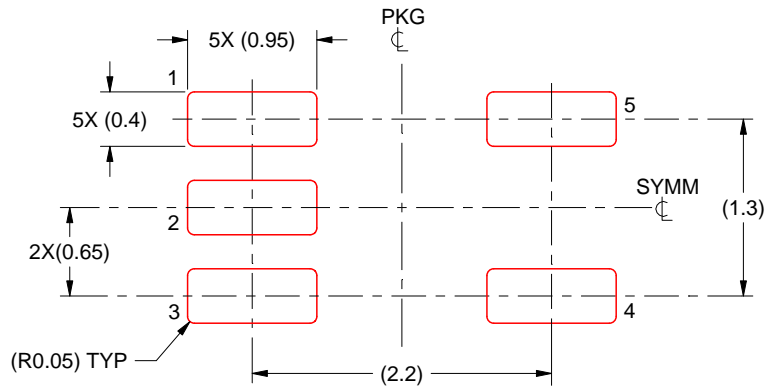
- 7. Publication IPC-7351 may have alternate designs.
- 8. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DCK0005A

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 THICK STENCIL  
SCALE: 18X

4214834/G 11/2024

NOTES: (continued)

9. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
10. Board assembly site may have different recommendations for stencil design.

# DDF0008A



# PACKAGE OUTLINE

## SOT-23-THIN - 1.1 mm max height

PLASTIC SMALL OUTLINE



4222047/E 07/2024

### NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.

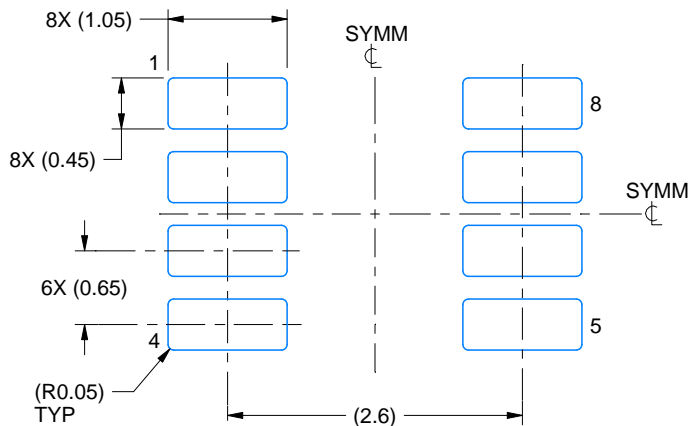


# EXAMPLE BOARD LAYOUT

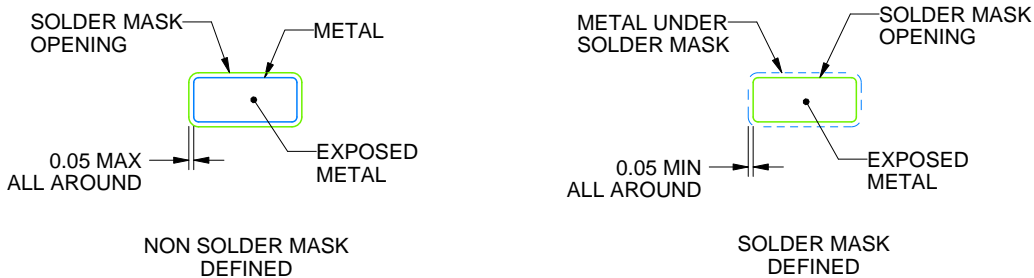
DDF0008A

SOT-23-THIN - 1.1 mm max height

PLASTIC SMALL OUTLINE



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

4222047/E 07/2024

NOTES: (continued)

4. Publication IPC-7351 may have alternate designs.
5. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DDF0008A

SOT-23-THIN - 1.1 mm max height

PLASTIC SMALL OUTLINE



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

4222047/E 07/2024

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
7. Board assembly site may have different recommendations for stencil design.



D0008A

# PACKAGE OUTLINE

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



4214825/C 02/2019

NOTES:

- Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- This drawing is subject to change without notice.
- This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed  $.006$  [0.15] per side.
- This dimension does not include interlead flash.
- Reference JEDEC registration MS-012, variation AA.

# EXAMPLE BOARD LAYOUT

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



LAND PATTERN EXAMPLE  
 EXPOSED METAL SHOWN  
 SCALE:8X



SOLDER MASK DETAILS

4214825/C 02/2019

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



SOLDER PASTE EXAMPLE  
BASED ON .005 INCH [0.125 MM] THICK STENCIL  
SCALE:8X

4214825/C 02/2019

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

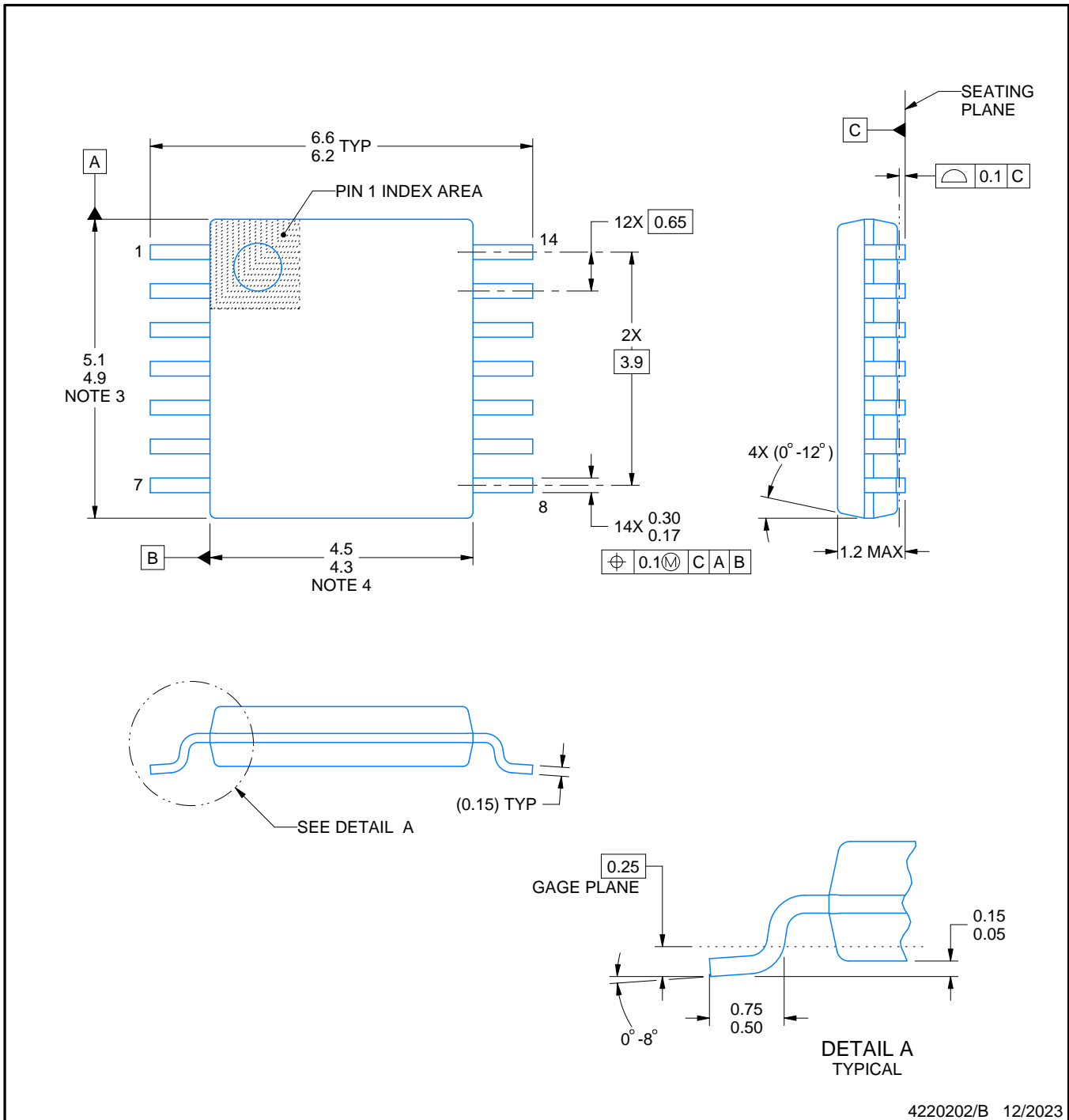
PW0014A



PACKAGE OUTLINE

TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



4220202/B 12/2023

NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
5. Reference JEDEC registration MO-153.

# EXAMPLE BOARD LAYOUT

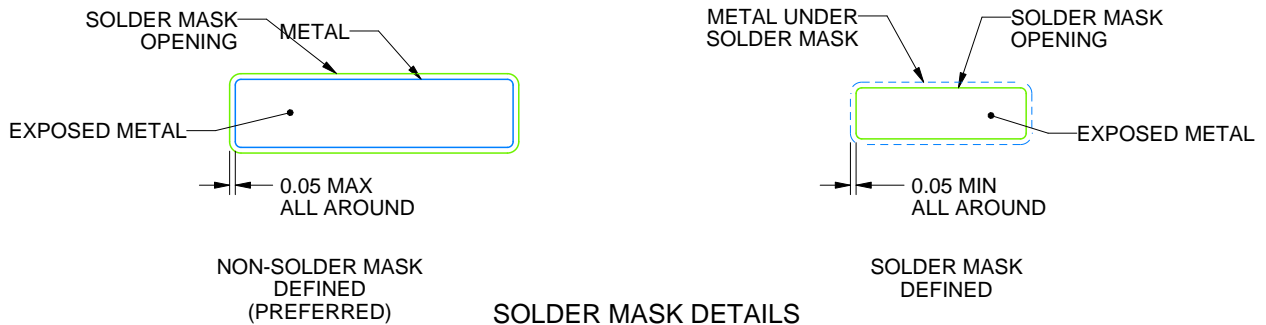
PW0014A

TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE: 10X



4220202/B 12/2023

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

PW0014A

TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE: 10X

4220202/B 12/2023

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.



PW0008A



# PACKAGE OUTLINE

## TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



4221848/A 02/2015

### NOTES:

- All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- This drawing is subject to change without notice.
- This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
- This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- Reference JEDEC registration MO-153, variation AA.

# EXAMPLE BOARD LAYOUT

PW0008A

TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE  
SCALE:10X



SOLDER MASK DETAILS  
NOT TO SCALE

4221848/A 02/2015

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

PW0008A

TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:10X

4221848/A 02/2015

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.



# EXAMPLE BOARD LAYOUT

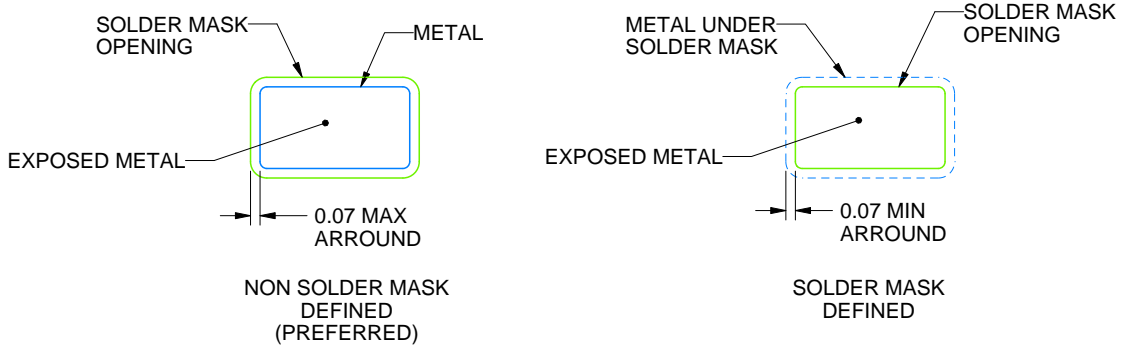
DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

4214839/K 08/2024

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

4214839/K 08/2024

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

# DGK0008A



# PACKAGE OUTLINE

VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



**NOTES:**

PowerPAD is a trademark of Texas Instruments.

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
5. Reference JEDEC registration MO-187.

# EXAMPLE BOARD LAYOUT

DGK0008A

™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE: 15X



SOLDER MASK DETAILS

4214862/A 04/2023

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
9. Size of metal pad may vary due to creepage requirement.



# EXAMPLE STENCIL DESIGN

DGK0008A

™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



SOLDER PASTE EXAMPLE  
SCALE: 15X

4214862/A 04/2023

NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
12. Board assembly site may have different recommendations for stencil design.

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